

Finite Element Modeling Crosstie and Fastening System at UIUC



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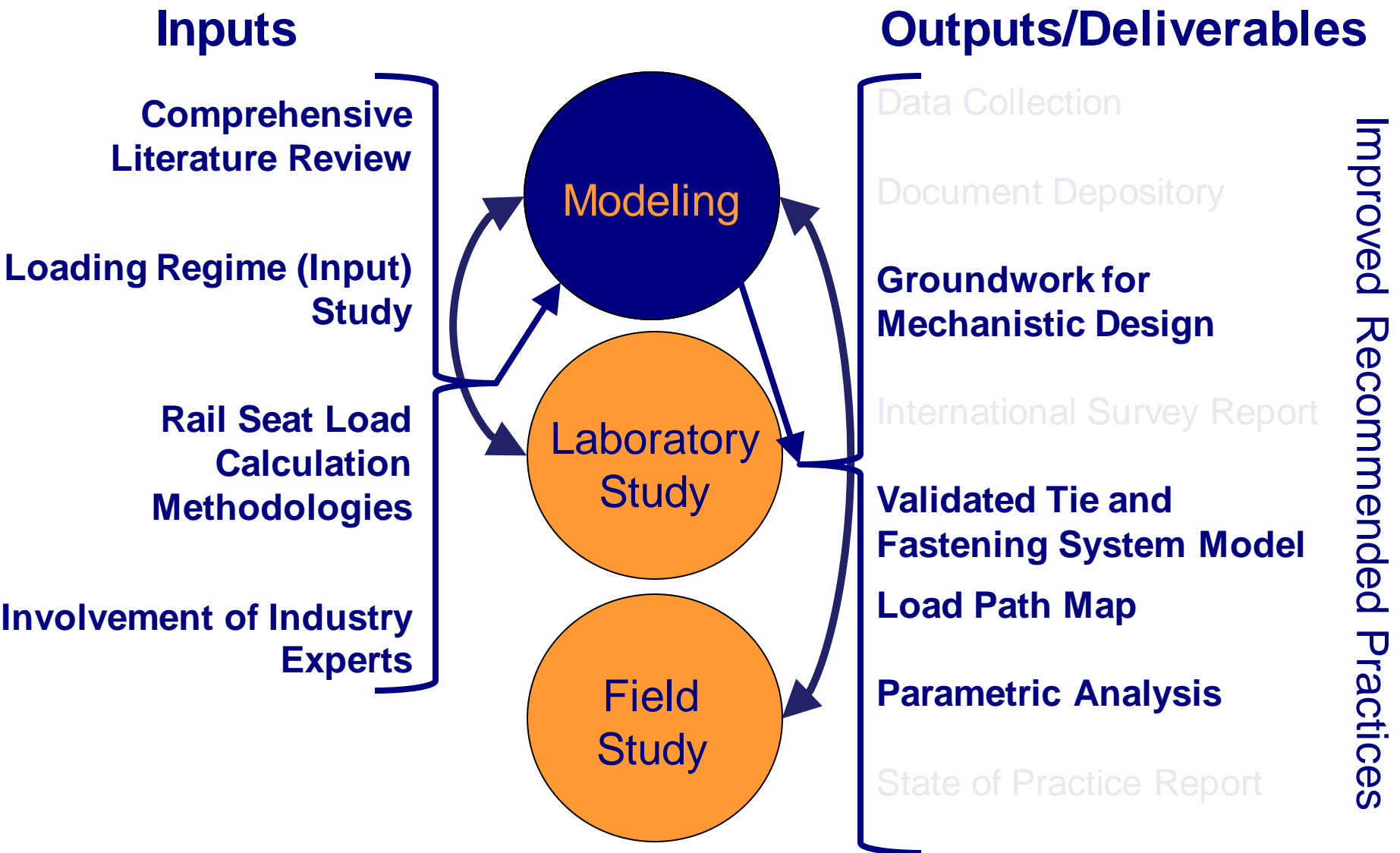
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Outline

- Research Objective and the Role of Modeling
- State of the Art
- Component Modeling
- System Modeling
 - Fastening System (2D and 3D)
 - Single-Tie System Modeling
 - Multiple-Tie System Modeling
- Conclusions
- Future Work

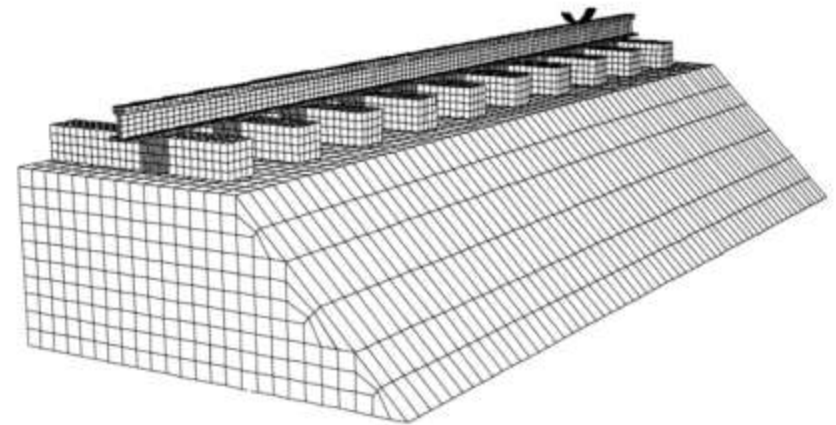
FRA Tie and Fastener Project Structure



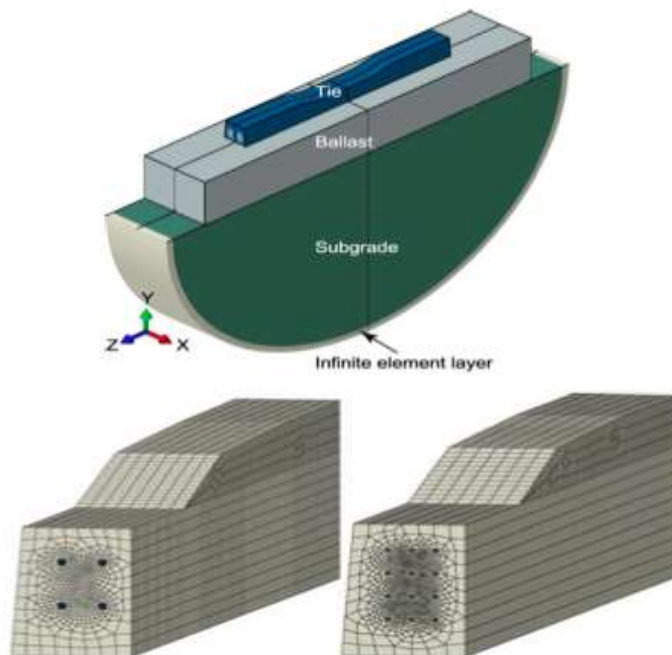
State of the Art

Track System Modeling

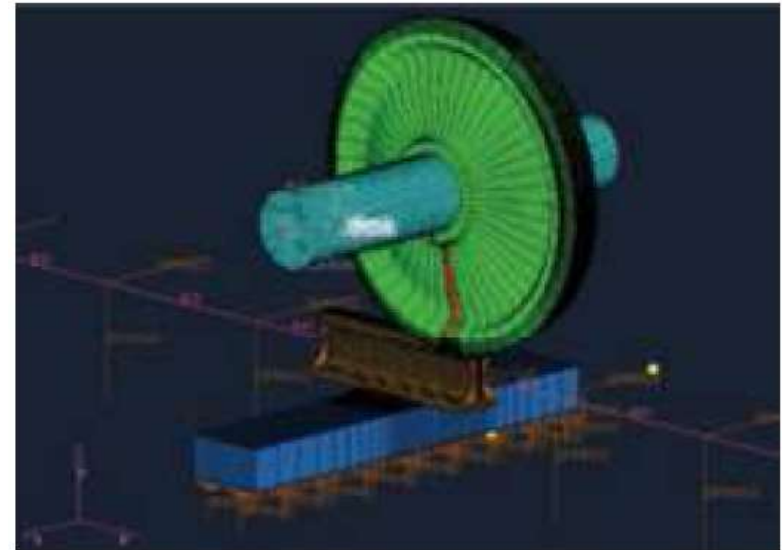
- Simplified fastening systems
- Focused on vertical loading
- Simplified support conditions



(Lundqvist and Dahlberg, 2005 - Sweden)

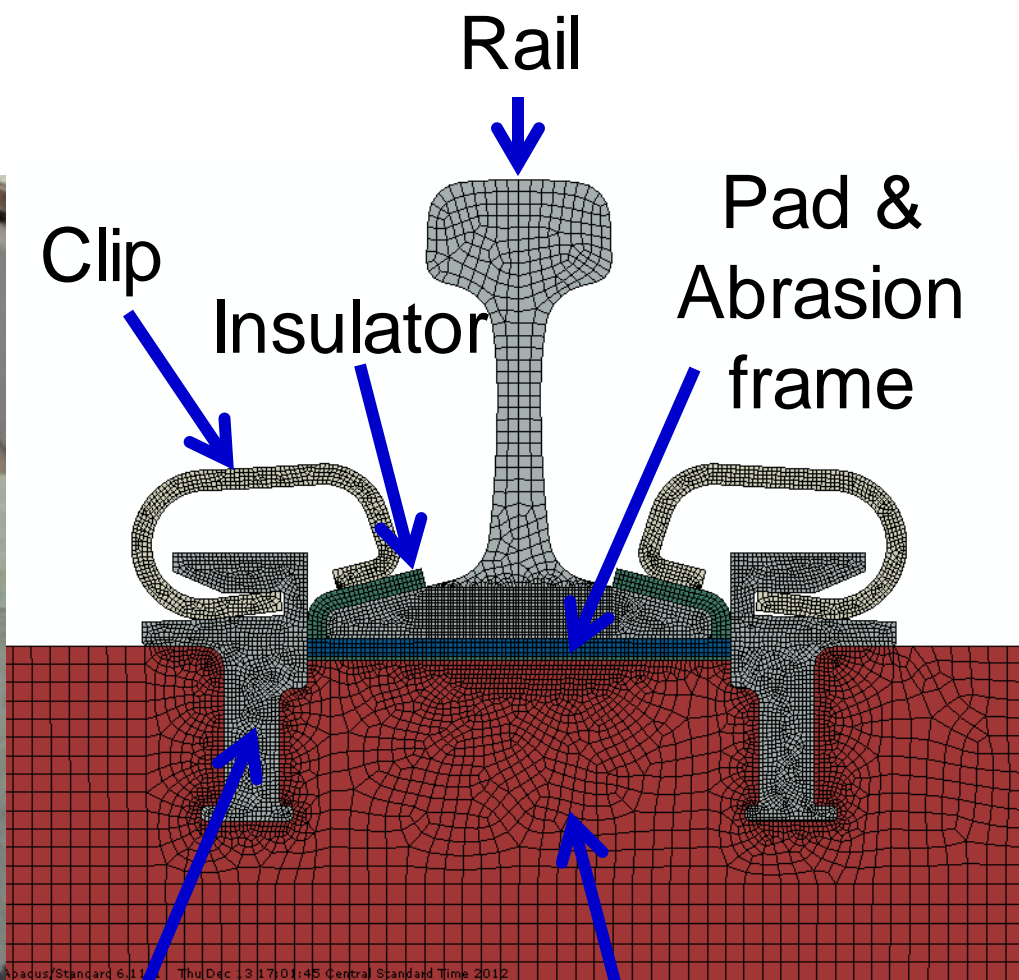


(Yu and Jeong, 2011)



(Tangtragulwong 2009)

Concrete Crosstie and Fastening System



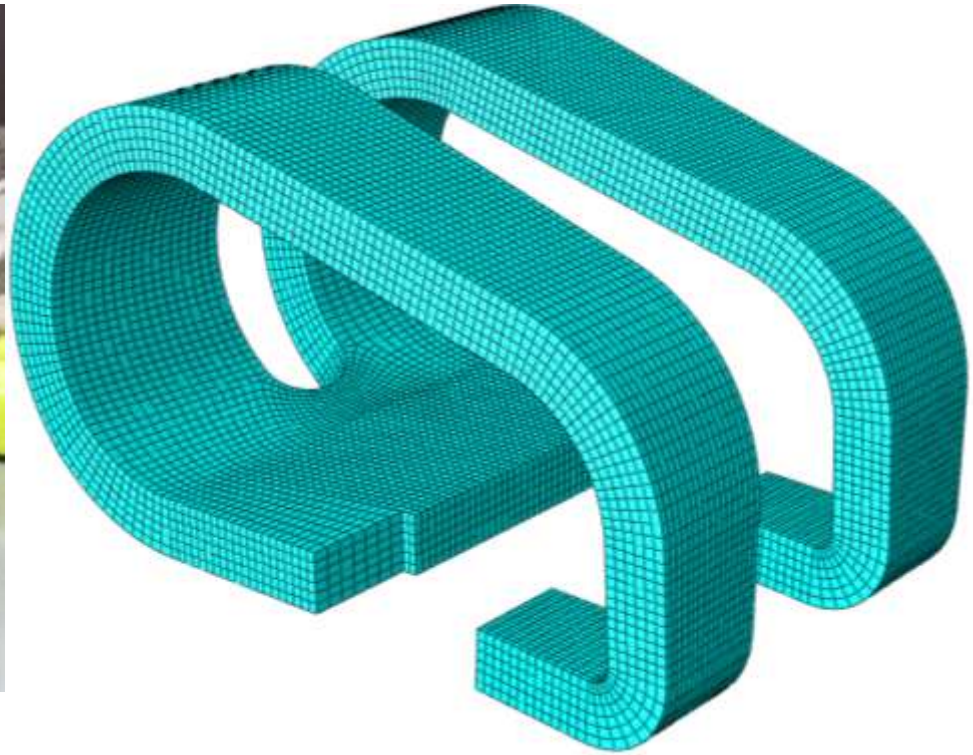
Shoulder Concrete crosstie

Apacus/Standard 6.11 Thu Dec 3 17:01:45 Central Standard Time 2012

Component Modeling



Rail Clip

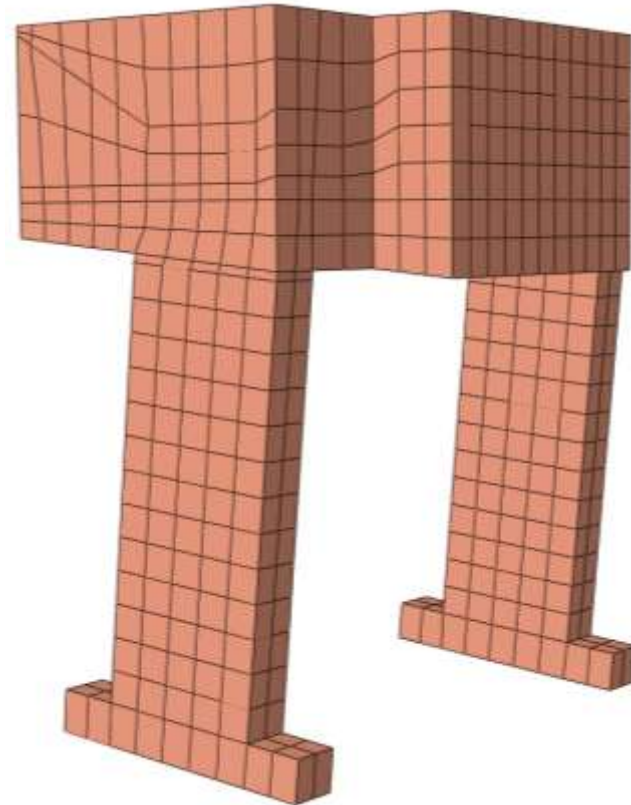


Rail Clip model

Component Modeling



Rail Shoulder

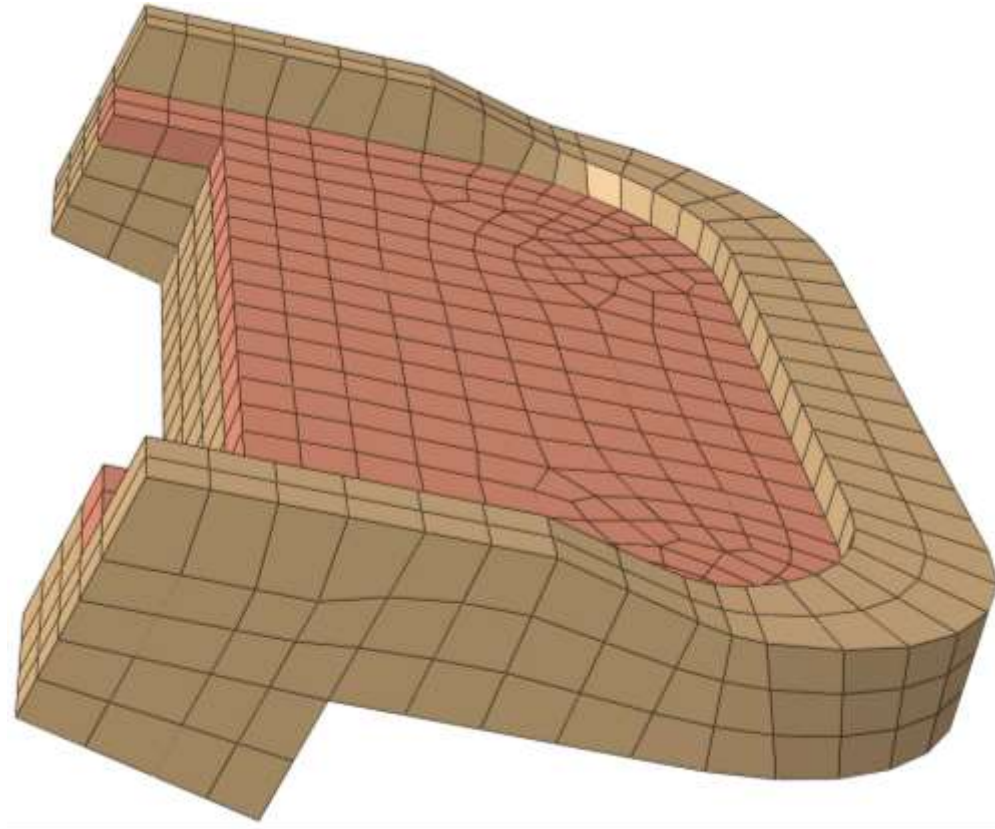


Rail Shoulder model

Component Modeling



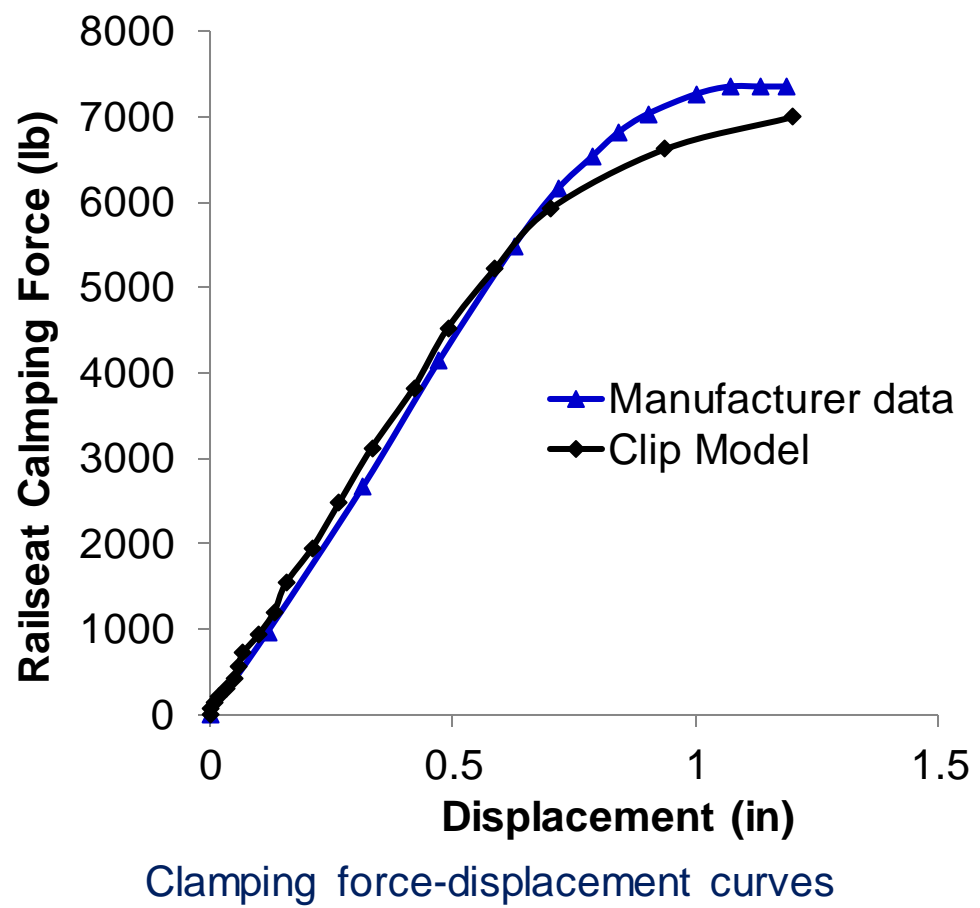
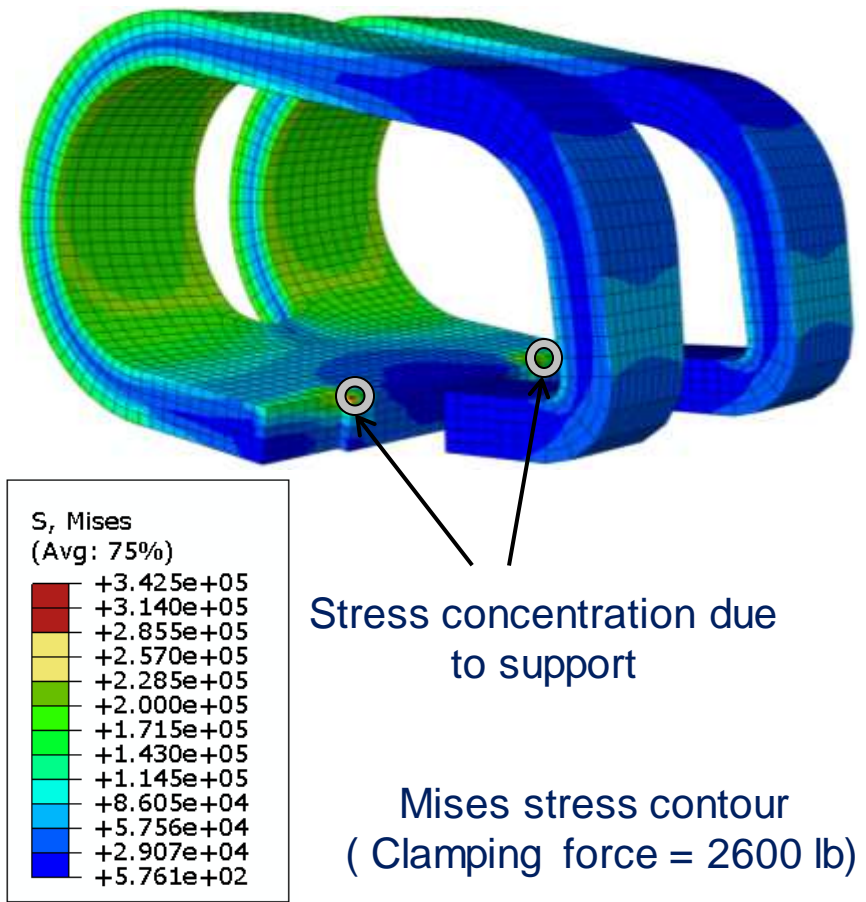
Rail Insulator



Rail Insulator model

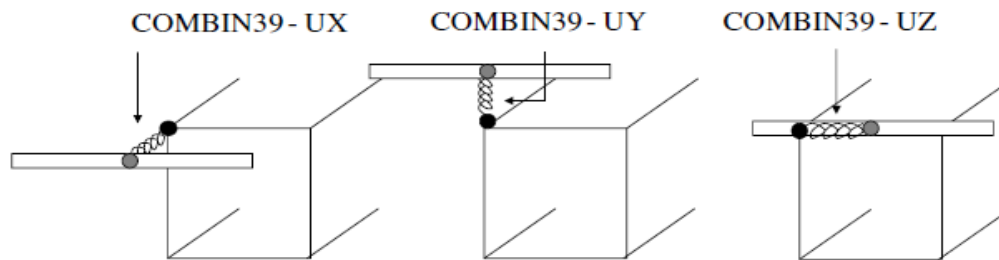
Component Modeling: Validation

- Clip Model



Component Modeling: Concrete Tie

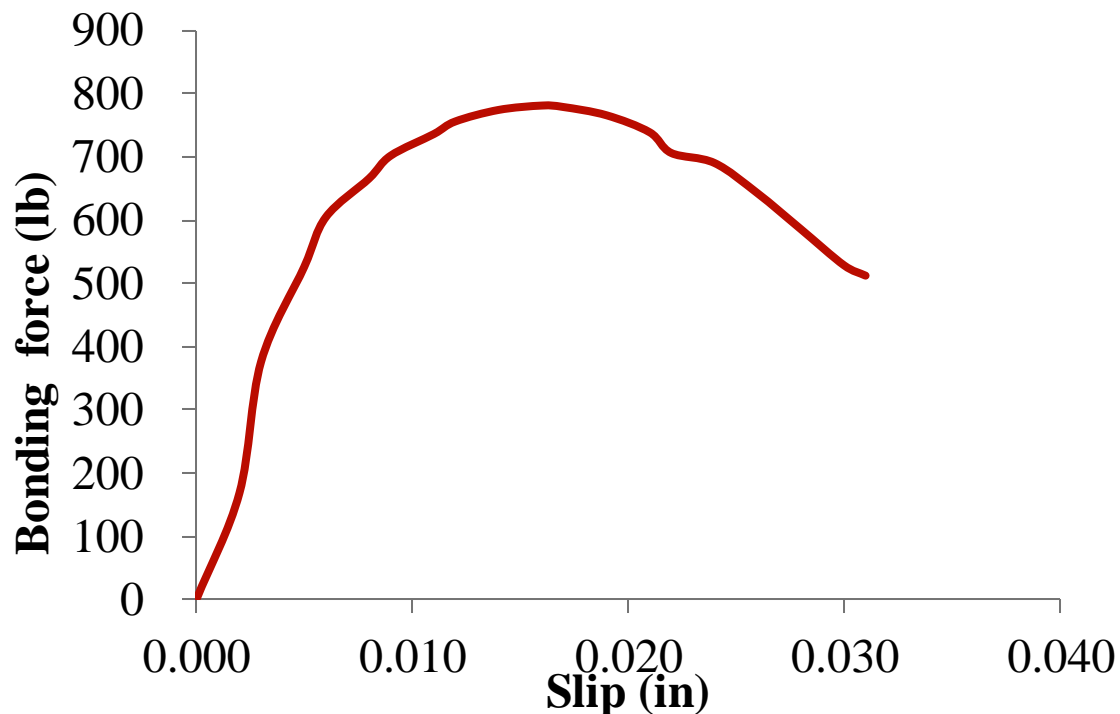
- Model Features:
 - Concrete material property: damage plasticity model
 - Connector element is used to simulate the bond relationship between concrete and strand
 - Prestress and vertical static loading is applied in the model
 - The effect of confining pressure on material property is considered in ballast modeling



3-D elastic spring connection between concrete and strand
(Pozolo and Andrawes 2011)

Component Modeling: Concrete Tie

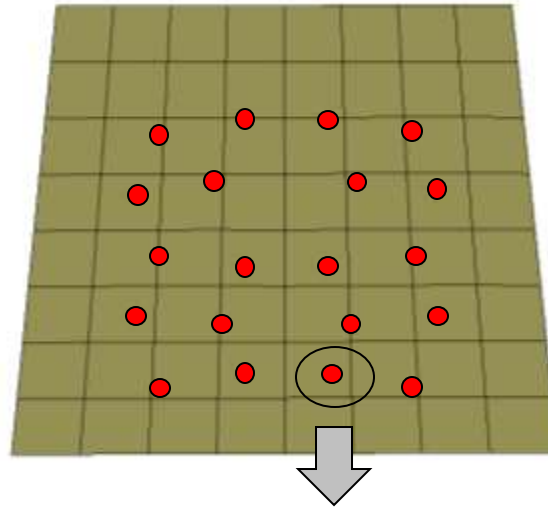
- A bonding force-slip relationship is defined in the model



Bonding force-slip Relationships

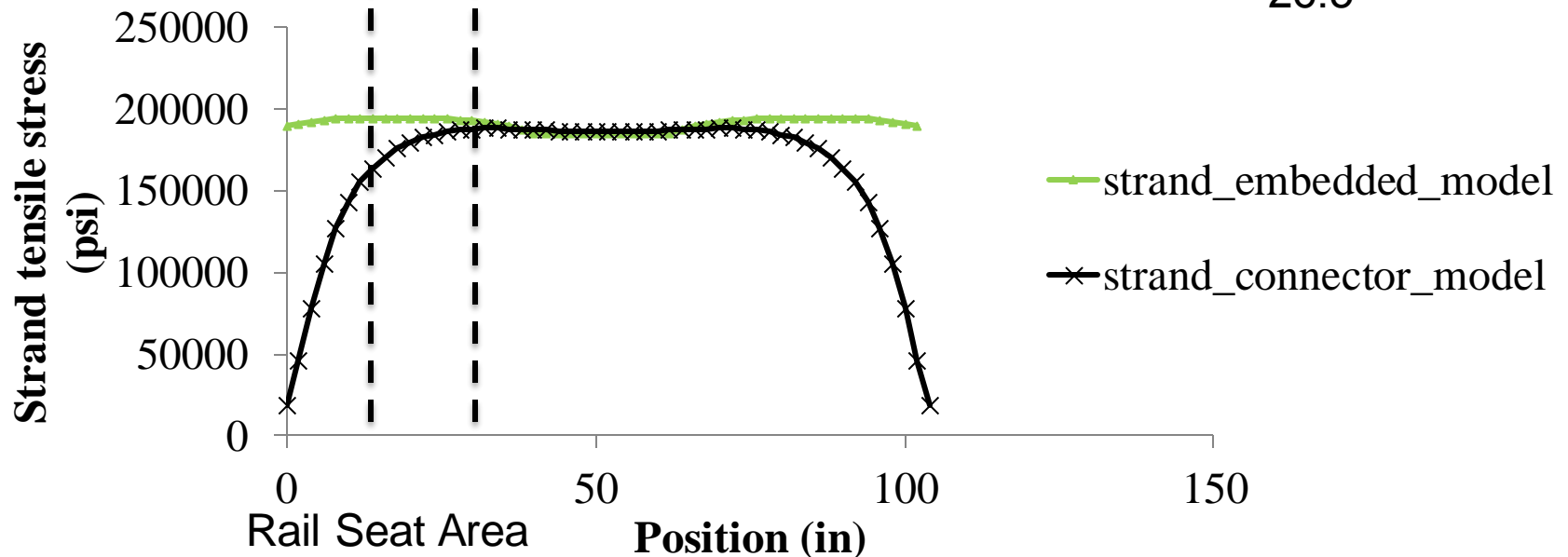
(Testing Data from the Kansas State University)

Component Modeling: Concrete Tie



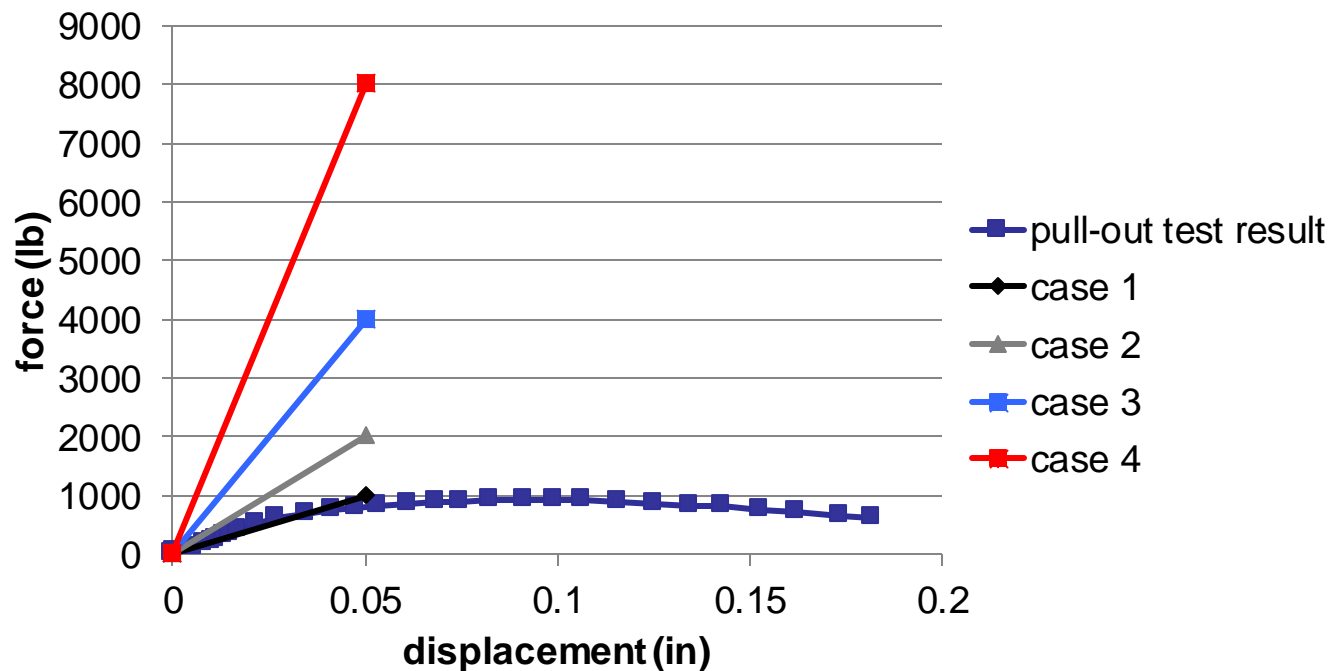
Positions of strands

Rail seat area is between 15.2" to 26.5"



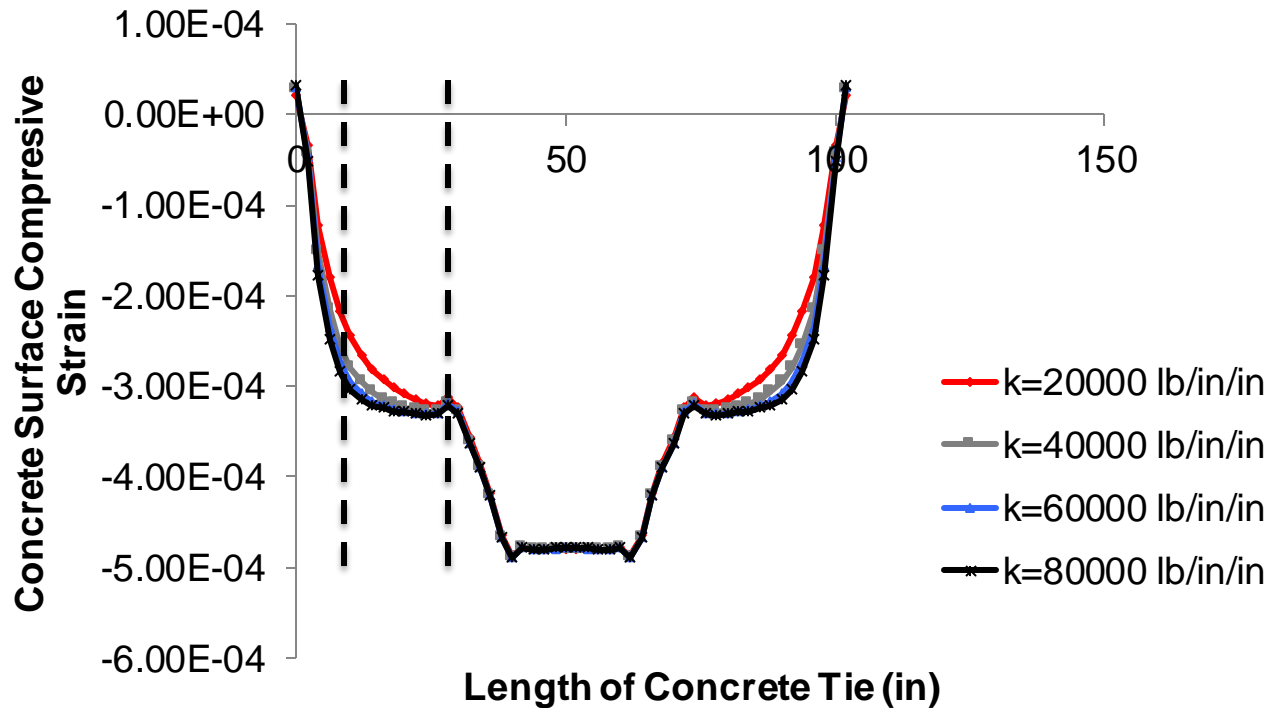
Component Modeling: Concrete Tie

- Different bond-slip behavior are defined for parametric study.
- The force-displacement relationship of connectors was simplified as elastic.
- Range of parameter is justified by pull-out tests of similar material in literature.



Component Modeling: Concrete Tie

- Transfer length gradually reduced with higher bond-slip stiffness.
- The rail-seat region is within transfer length with in case 1 and case 2.

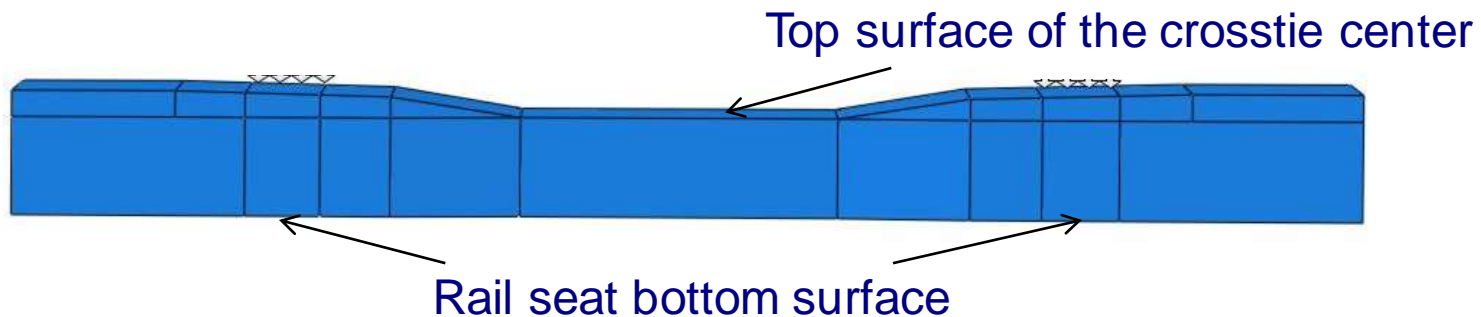


Rail seat area is between 15.2" to 26.5"

bond-slip stiffness	k= 20000 lb/in/in	k=40000 lb/in/in	k=60000 lb/in/in	k=80000 lb/in/in
transfer length (in)	22	16	14	12

Component Modeling: Concrete Tie

- The bond slip stiffness had little effect on the concrete prestress at the top surface of tie center.
- The concrete prestress at the bottom surface of rail seat region gradually increased with higher bond-slip stiffness.



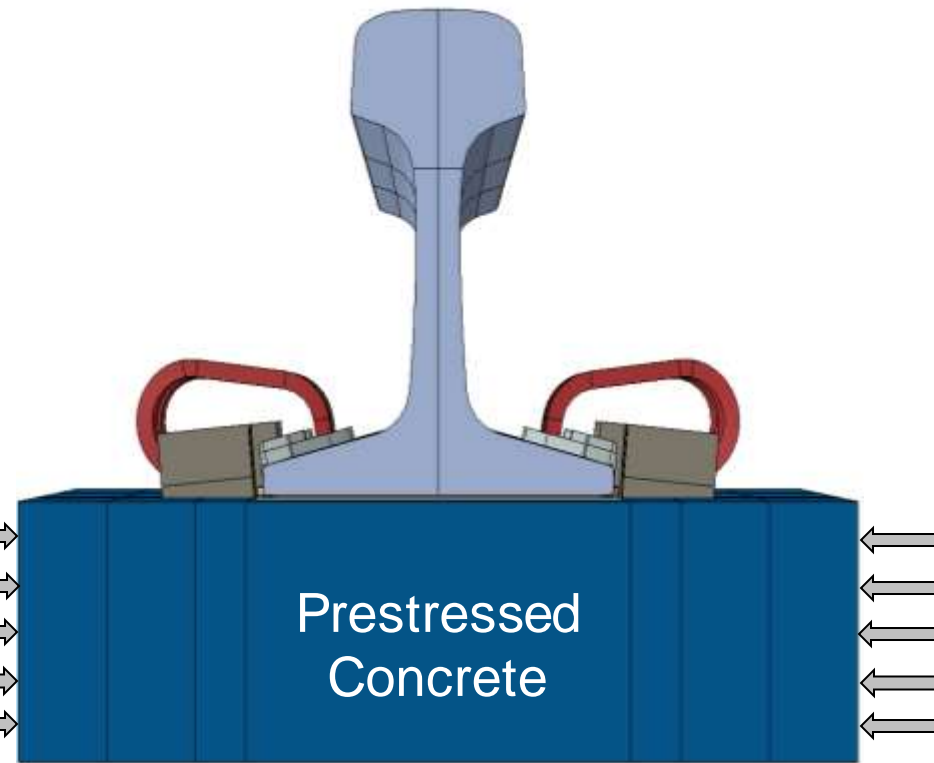
Bond slip stiffness	k= 20000 lb/in/in		k=40000 lb/in/in	
Surface position	Rail seat bottom surface	Tie center top surface	Rail seat bottom surface	Tie center top surface
Concrete surface stress after prestress release (psi)	-1793	-2416	-1863	-2414
Bond slip stiffness	k=60000 lb/in/in		k=80000 lb/in/in	
Surface position	Rail seat bottom surface	Tie center top surface	Rail seat bottom surface	Tie center top surface
Concrete surface stress after prestress release (psi)	-1880	-2412	-1886	-2411

System Modeling: 2D and 3D Modeling

2D Modeling



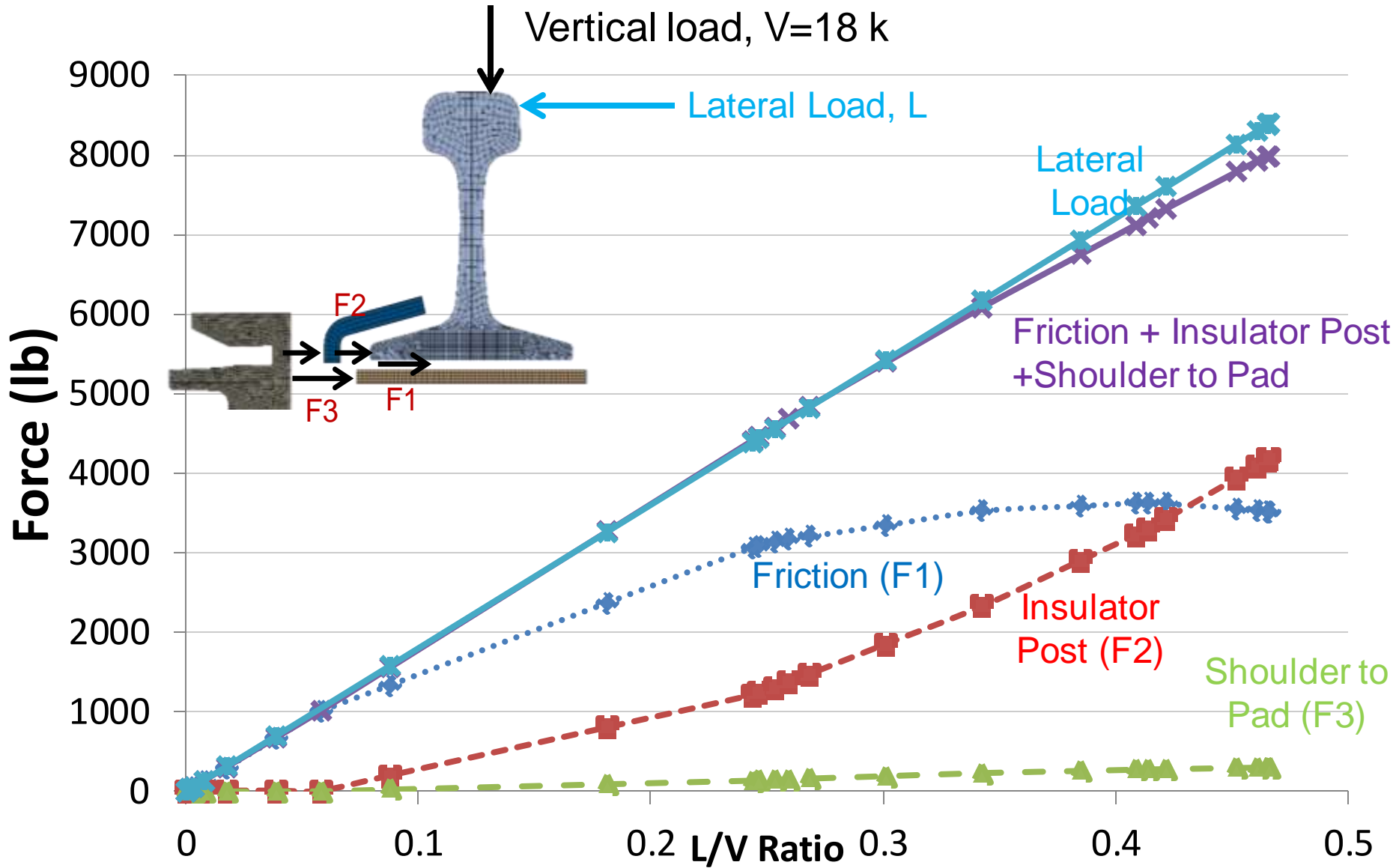
3D Modeling



Pin Support

System Modeling: Fastening Systems

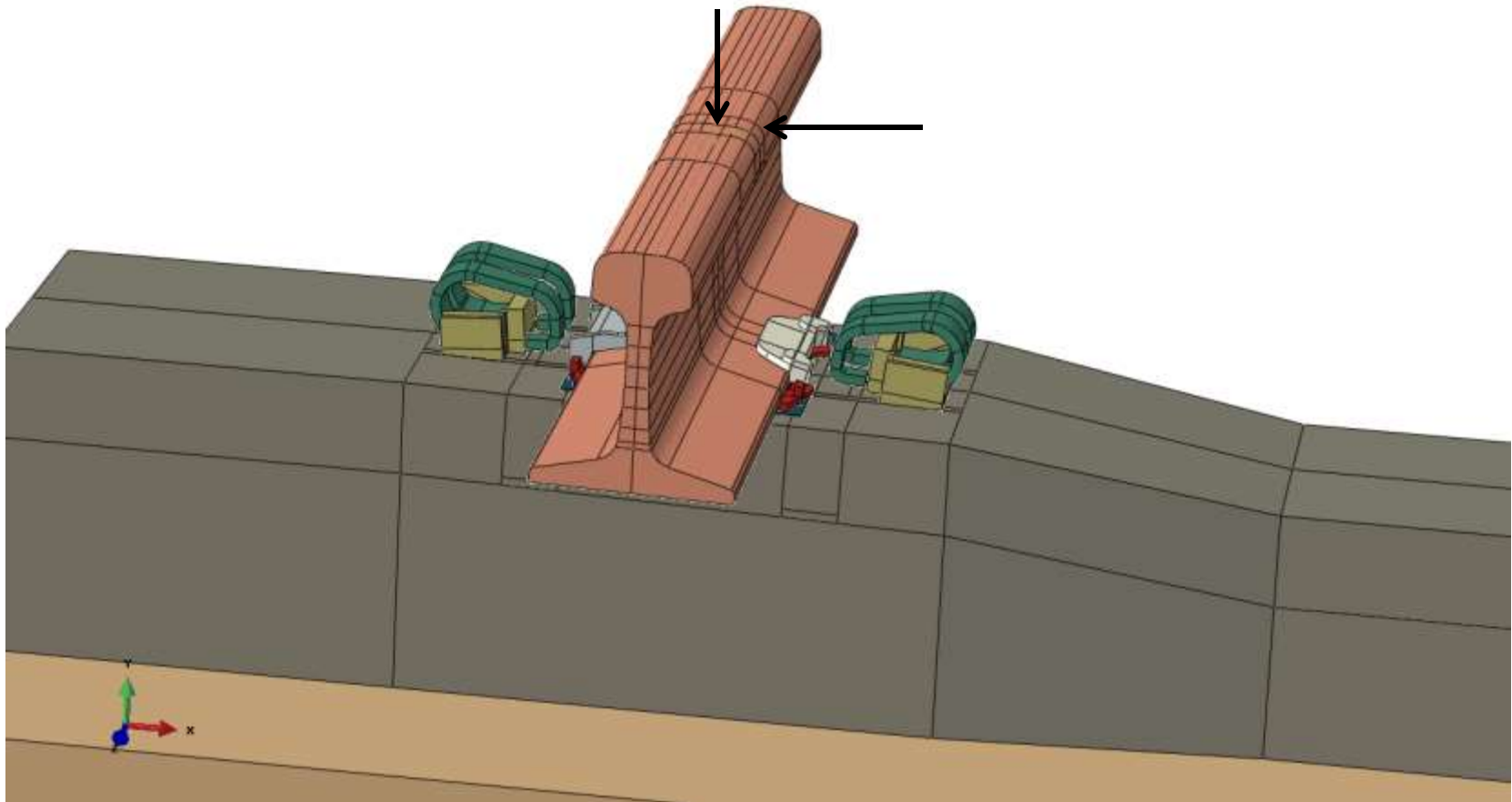
Lateral Loading Path



Lateral Force to a Shoulder

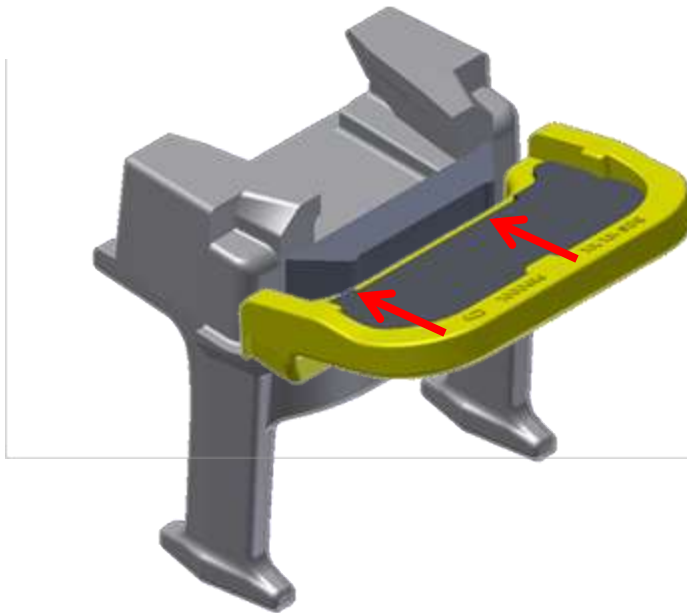
Vertical Force:

1. Magnitude: 32.5 kips

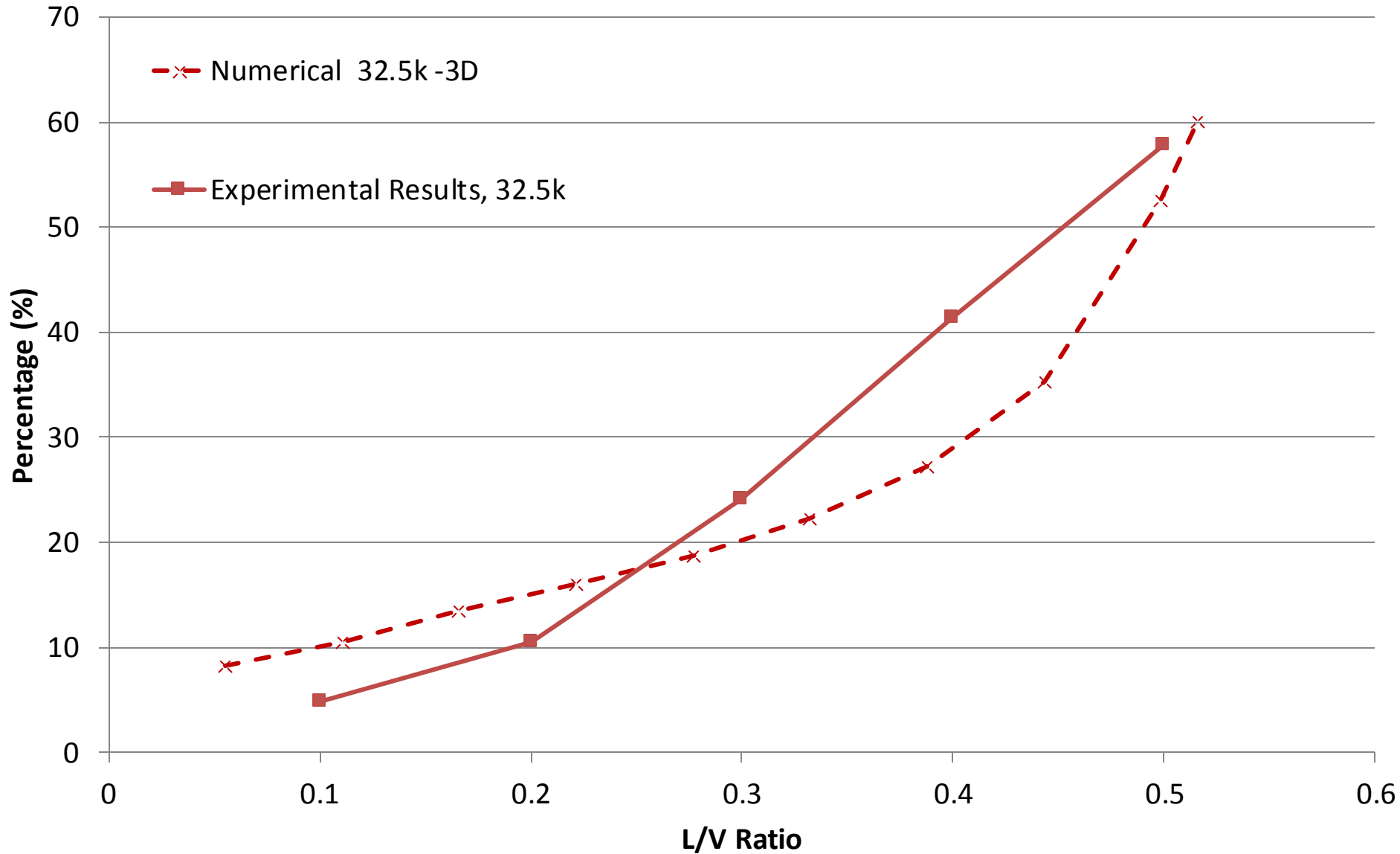


Quantifying lateral load on the insulator post (F2)

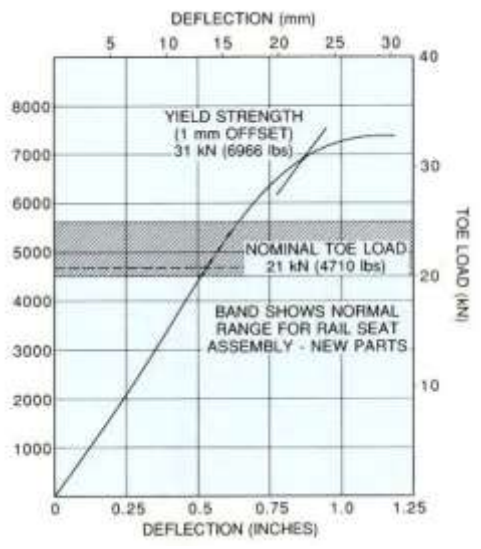
- Instrumented shoulder face insert



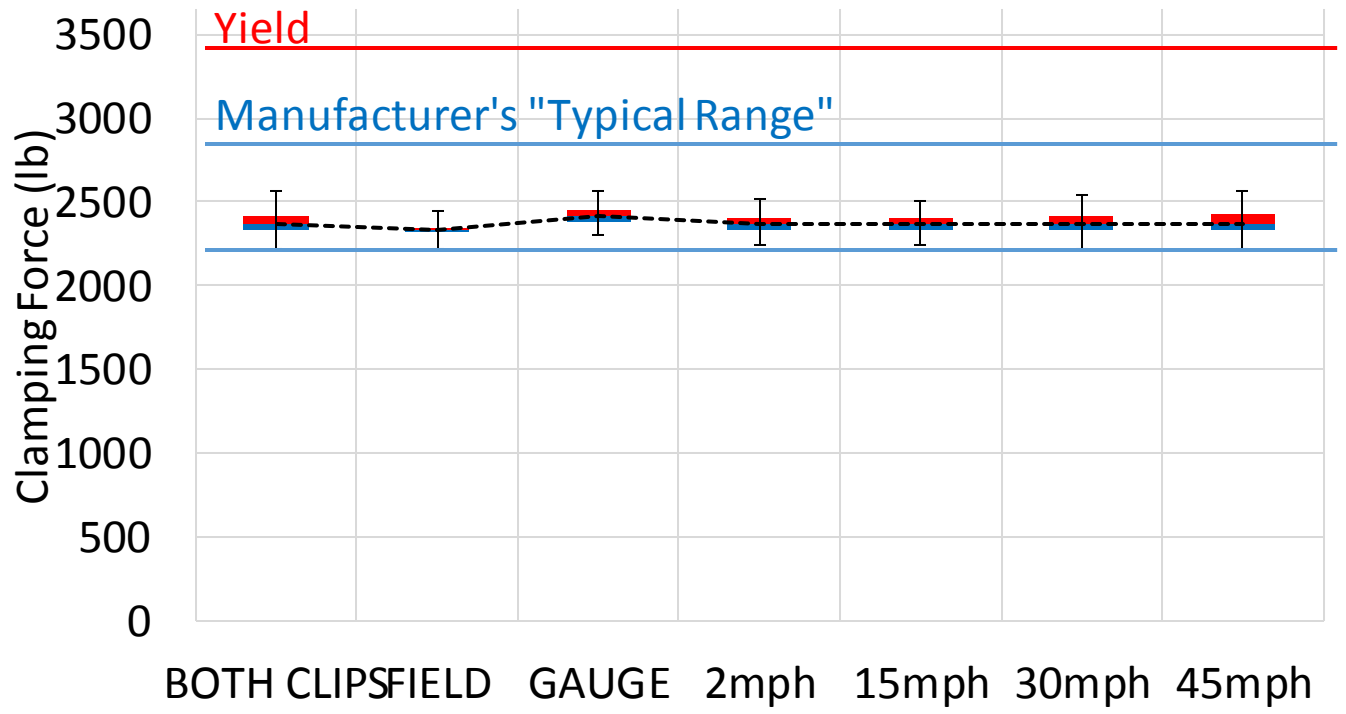
Lateral Force to a Shoulder



Changes of the Clamping Force



Range of the clamping force: ± 300 lb

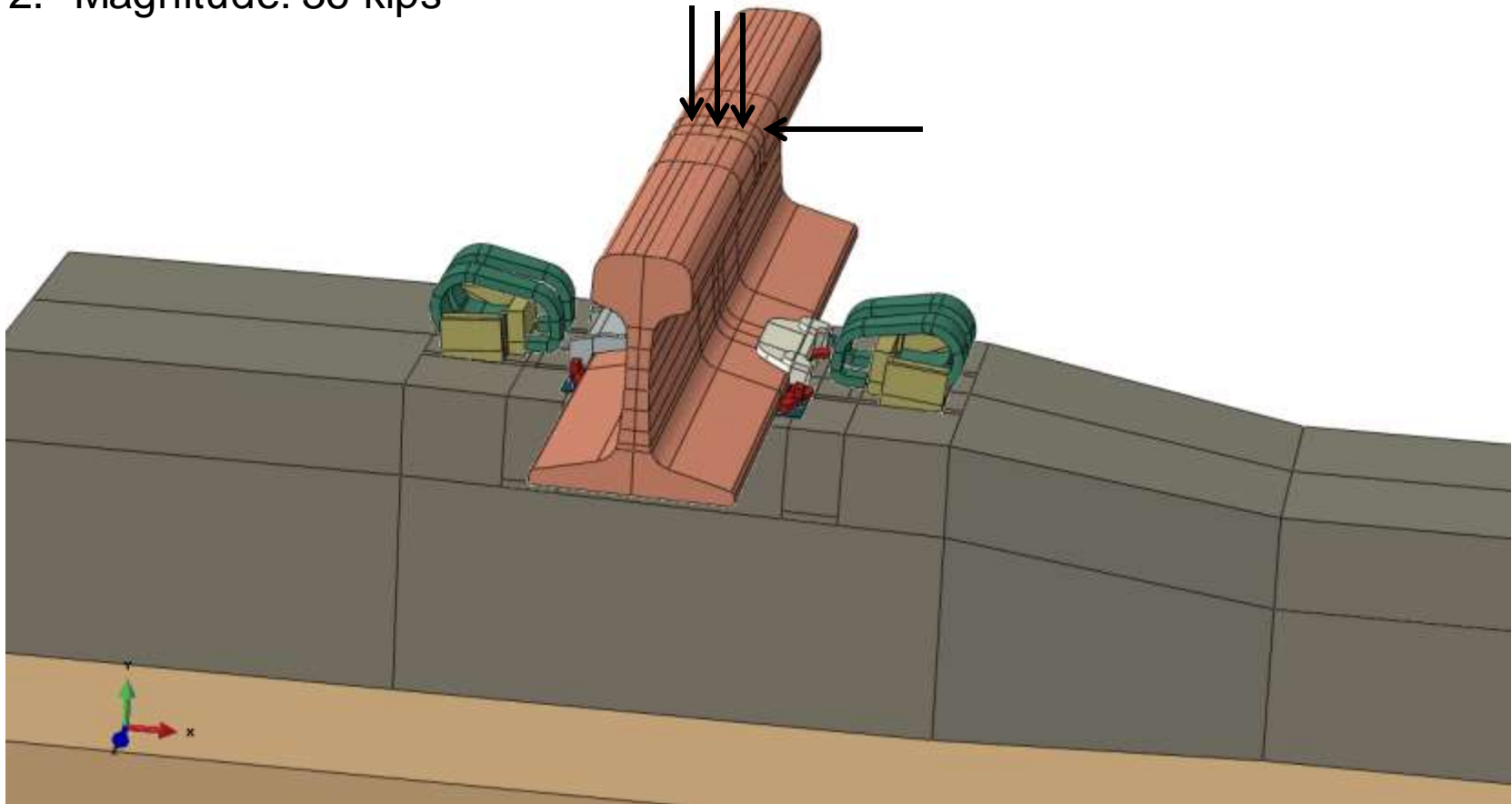


(Grasse JRC Presentation, 2013)

Changes of the Clamping Force

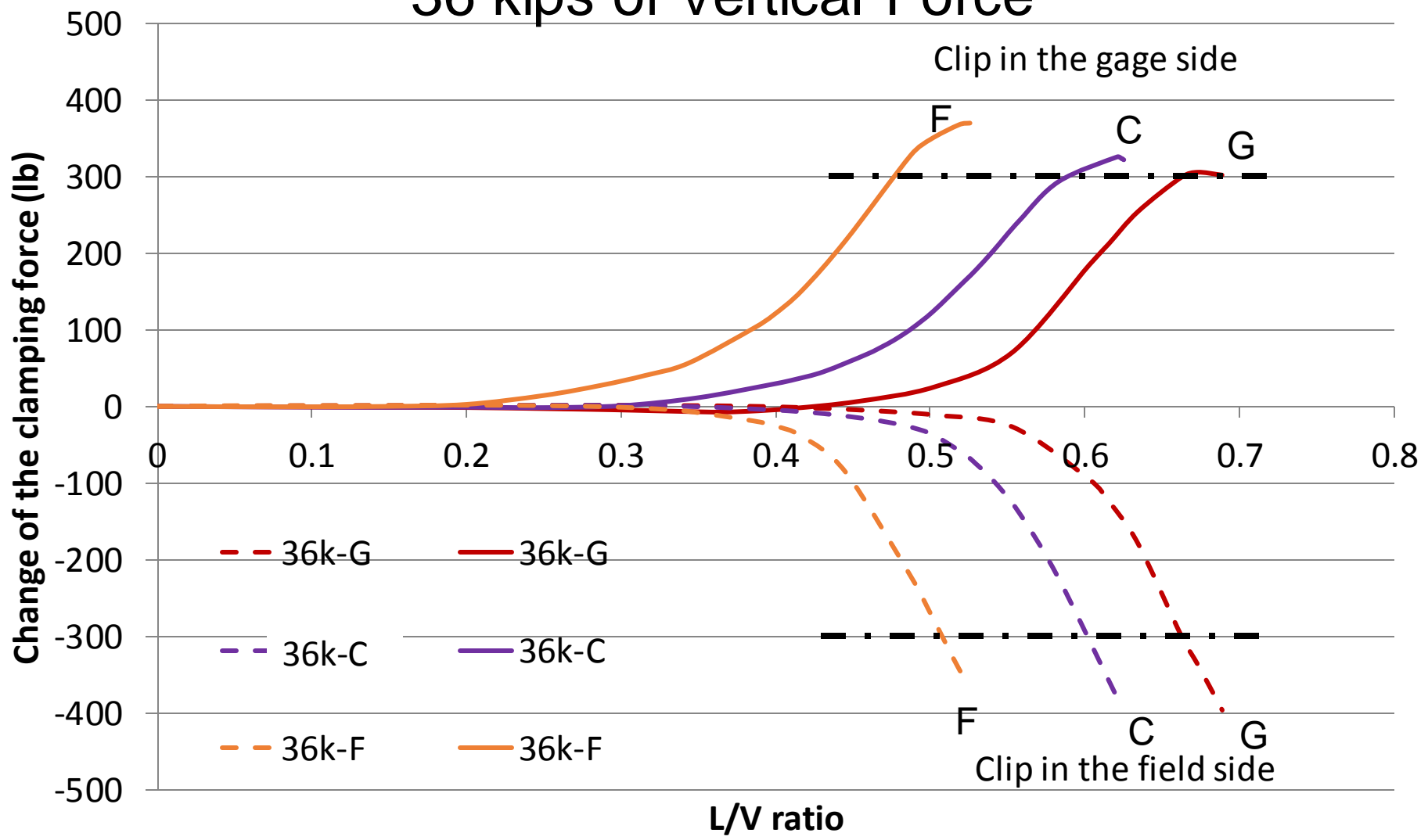
Vertical Force:

1. Location: Gage, Center, Field
2. Magnitude: 36 kips



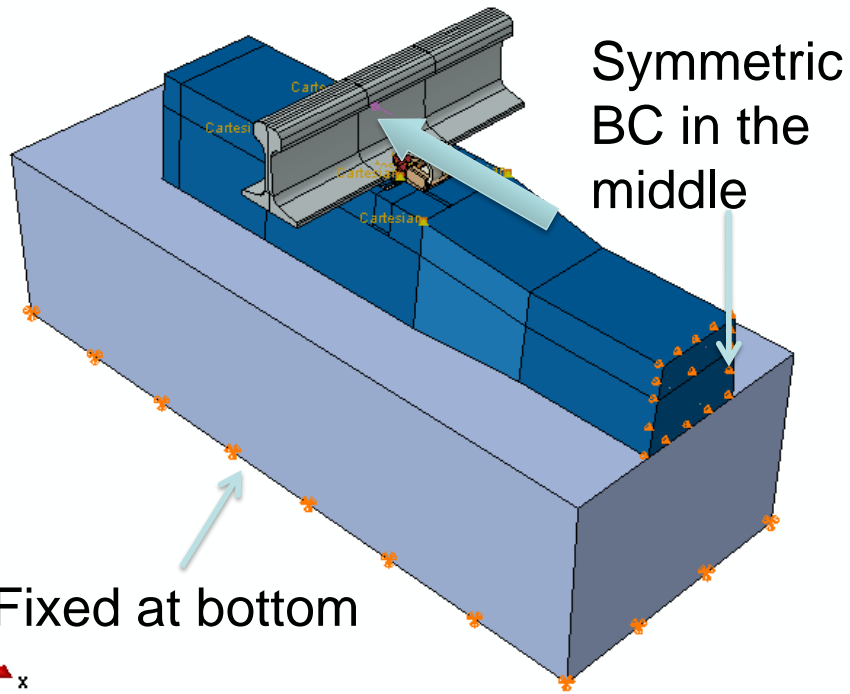
Change of the Clamping Force

36 kips of Vertical Force



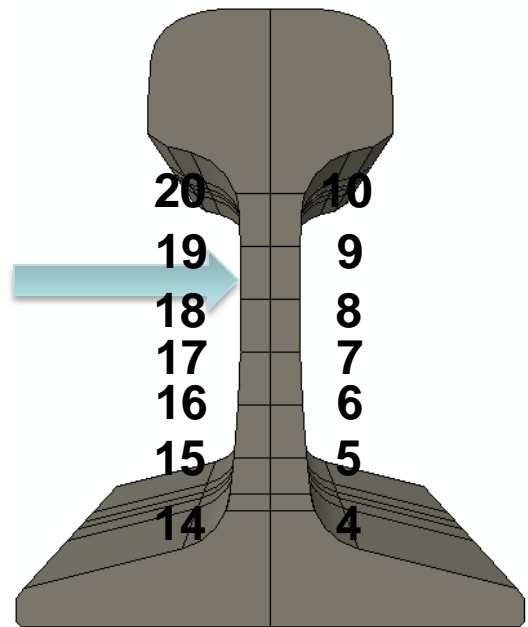
System Modeling: Single-Tie Modeling

Laboratory Test Validation



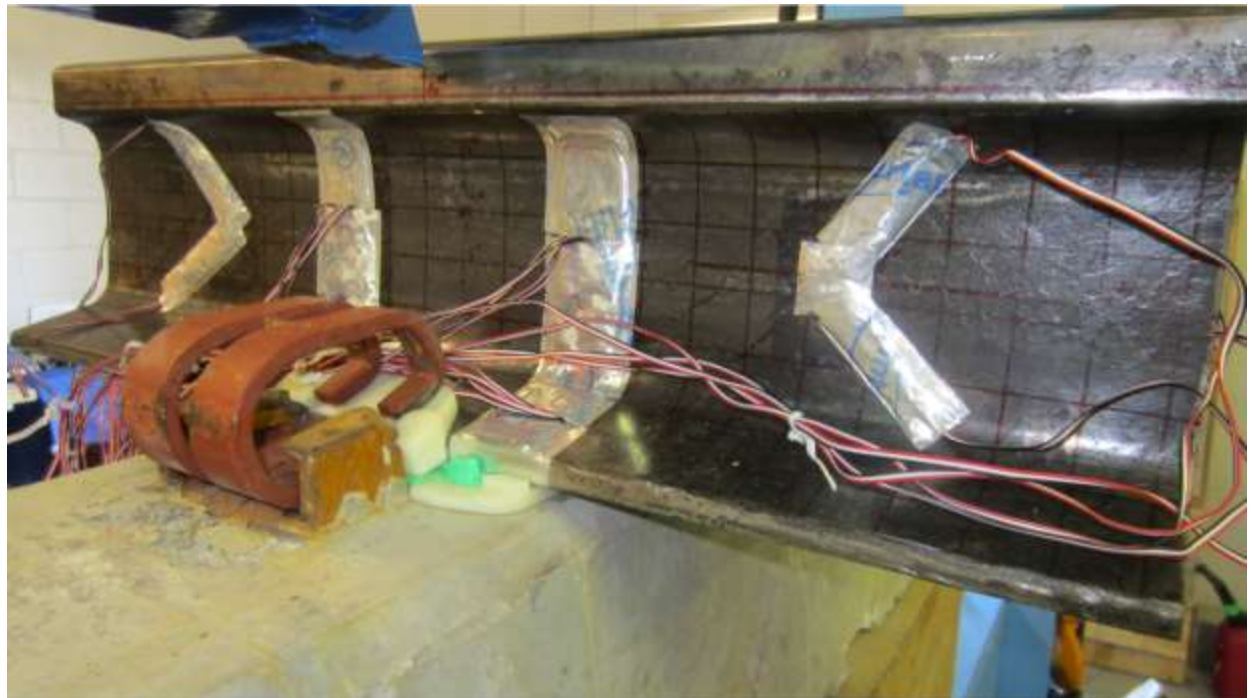
System Modeling: Single-Tie Modeling

- Strain gauges are attached to the rail to measure vertical web strain
- Lateral loading is applied on rail web.



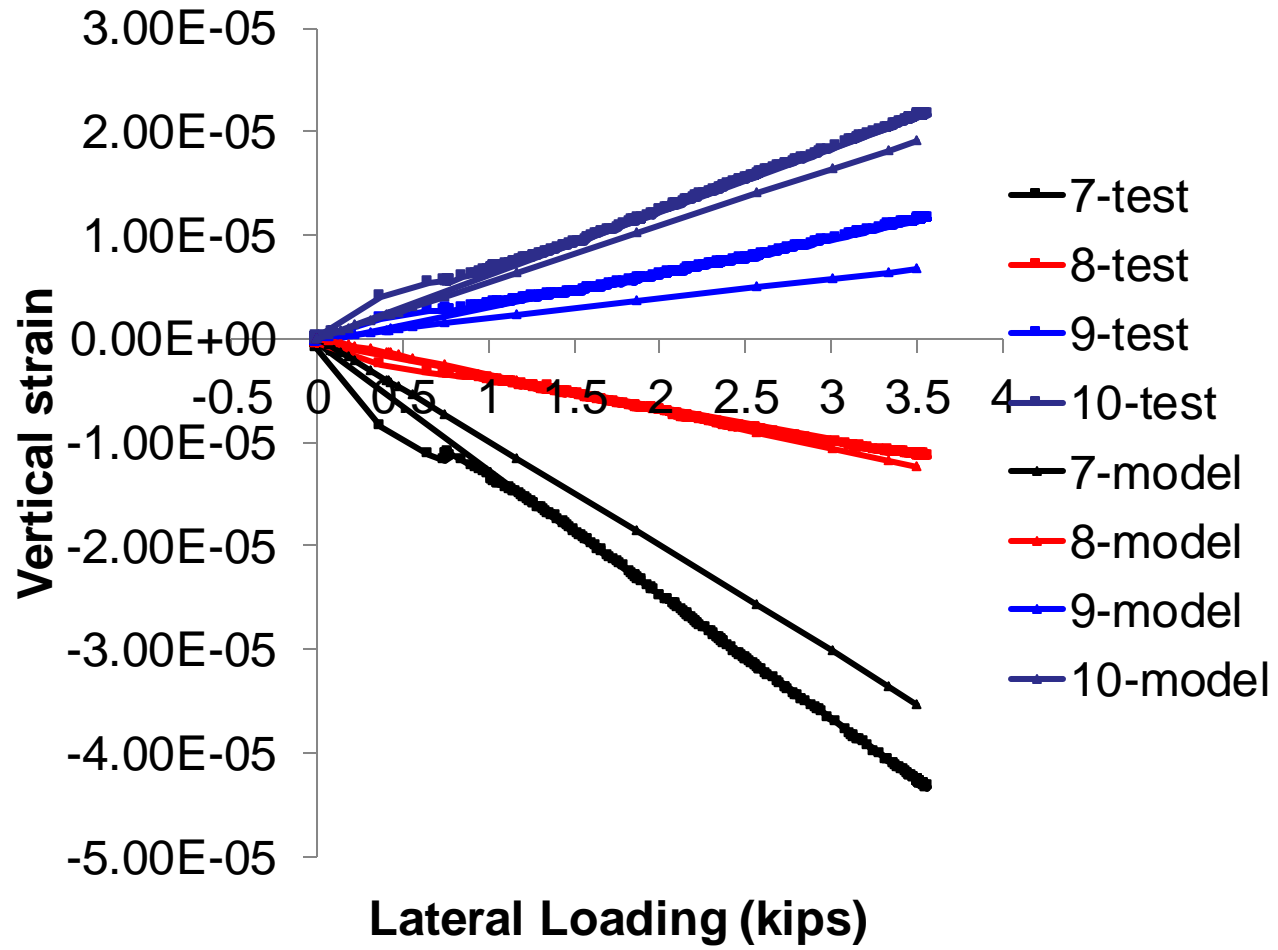
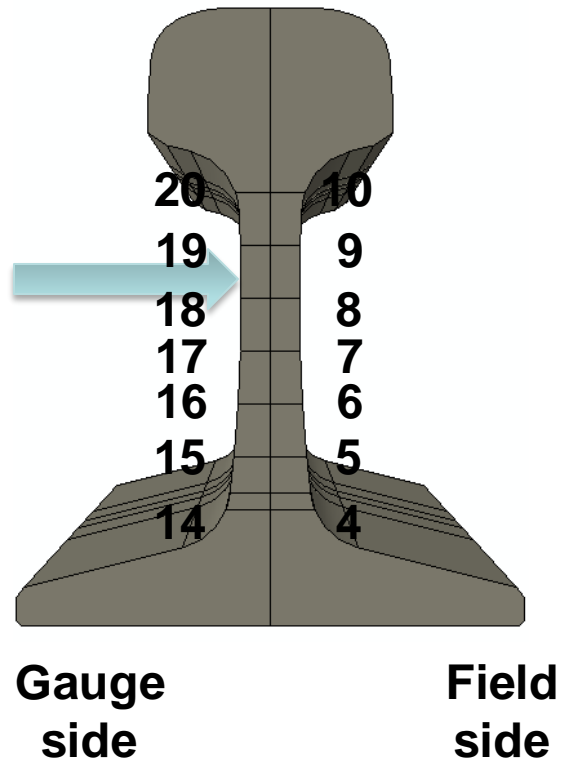
Gauge
side

Field
side



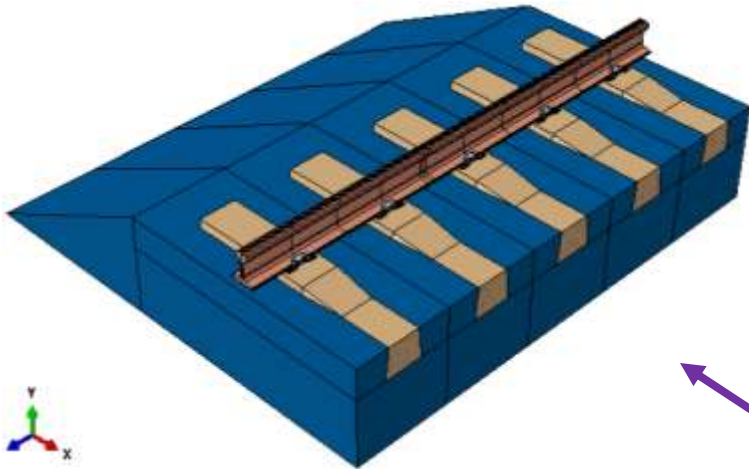
System Modeling: Single-Tie Modeling

Comparisons of strains

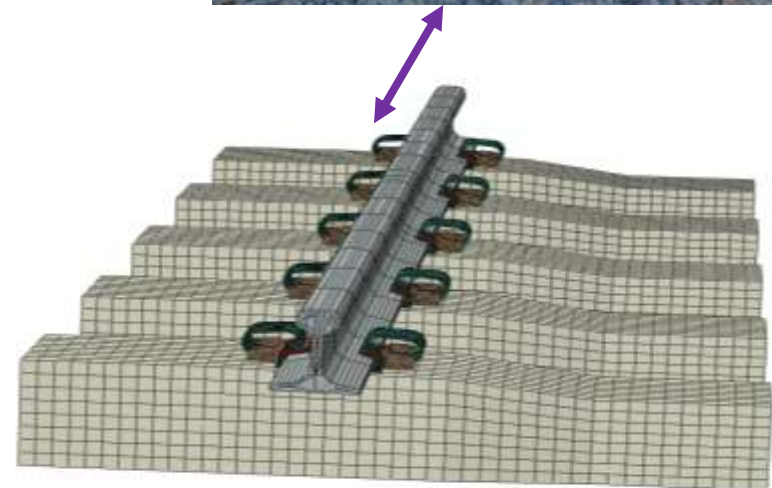


System Model: Multiple-Tie Modeling

- Track loading vehicle (TLV) applying vertical and lateral loads to the track structure in field
- The symmetric model including 5 ties



Simplified model:
Fastening system were replaced
by bcs and pressure



Detailed model with the fastening system

Conclusions

- Some component models were validated with manufacturer data
- Single tie model was used to study bond-slip behavior of strands
- With the fastening system model, the loading path (vertical and lateral) can be identified
- Current laboratory tests were validated, and good agreement was observed
- Multiple tie models have been developed and ready to validate the track system models in field

Future Work

- **Further comparisons:** More measurements on the lab testing set-ups will be deployed and compared with the models
- **Validation of FE models in field:** Comparisons with data collected with the field instrumentations at Transportation Technology Center, Pueblo, CO
- **Realistic loading:** More load types (vertical, lateral, and longitudinal loads) and load forms (static and dynamic load) will be applied to the track system to better simulate the actual loading environment
- **Parametric studies:** Parametric studies about material properties and geometric dimensions will be conducted using the model
- **Simplified analytical tool**



U.S. Department of Transportation

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Questions?



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