

High Strength Reduced Modulus Concrete for Railroad Crossties

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Director of Advanced Railroad Technology Group

*Department of Civil and Environmental Engineering University
of South Carolina*

William W. Hay Railroad Engineering Seminar



January 27, 2017

- ❑ **8 Campuses** more than 45,000 students
- ❑ **Location:** Columbia, S.C.
- ❑ **Organization:** 14 colleges and schools
- ❑ **Degree Programs:** more than 324
- ❑ **Enrollment:** more than 30,000 (Columbia)
- ❑ **Faculty:** approximately 1,560



Environmental Engineering

Transportation Engineering

Geotechnical Engineering

Water Resources Engineering

Structural Engineering & Mechanics

Railroad Engineering





Environmental Engineering

Transportation Engineering

Geotechnical Engineering

Water Resources Engineering

Structural Engineering & Mechanics

Railroad Engineering & the Advanced Railroad Technology Group

OBJECTIVES:

Nationally Recognized Research and Education Program

Nucleus of Excellence within CEE and USC to support industry

Promote Railroads in SC and the USA



Dimitris C. Rizos
Director
Infrastructure



Roger Dougal
Power & Controls



Michael Sutton
Experimental
Mechanics



Inthuorn Sasanakul
Geotechnical
Engineering



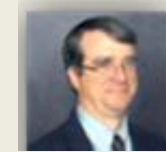
Michael Meadows
Hydraulics &
Education



Juan Caicedo
System Prognosis



Robert Mullen
Reliability & Risk



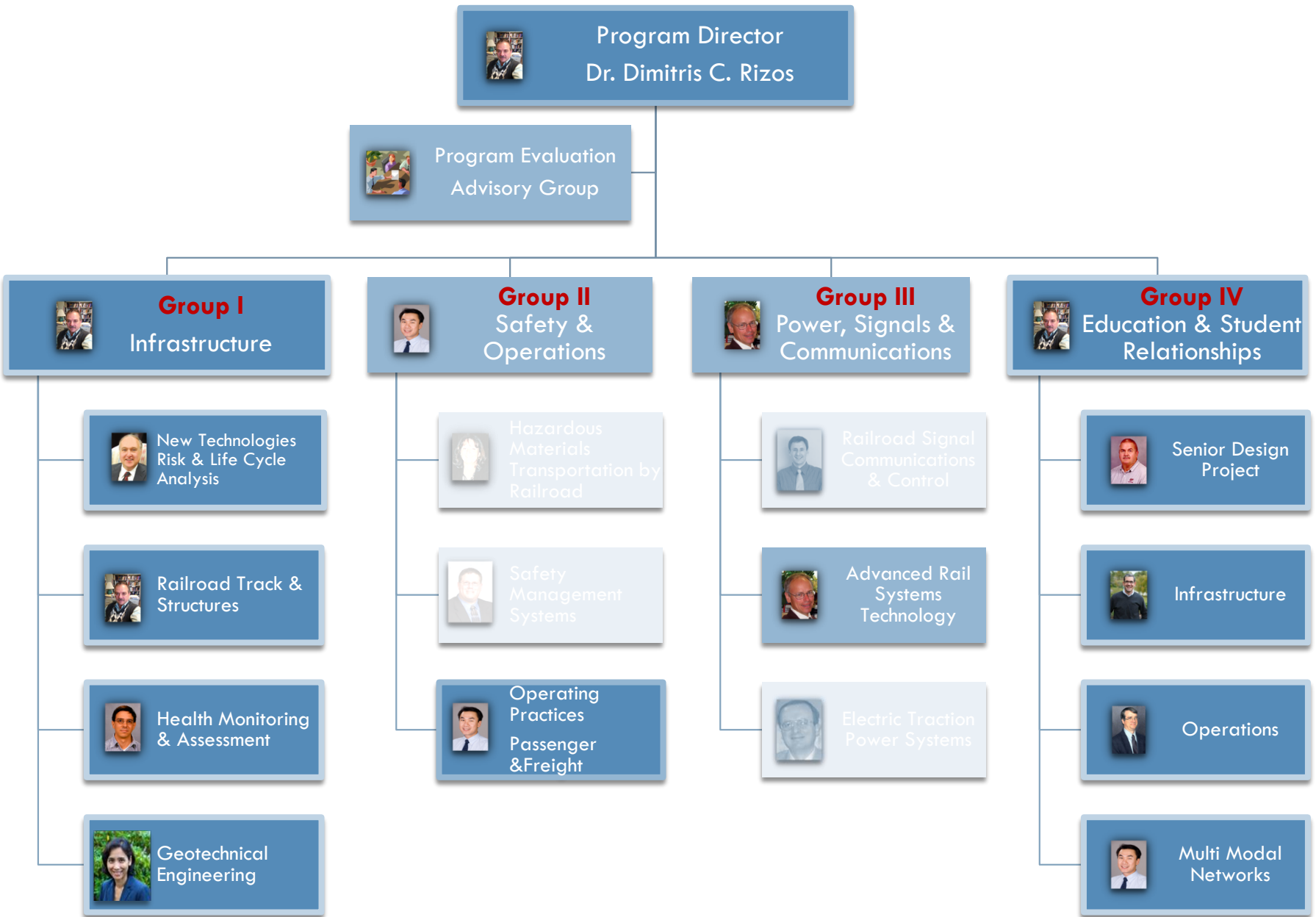
Dave Clarke
Rail Transportation

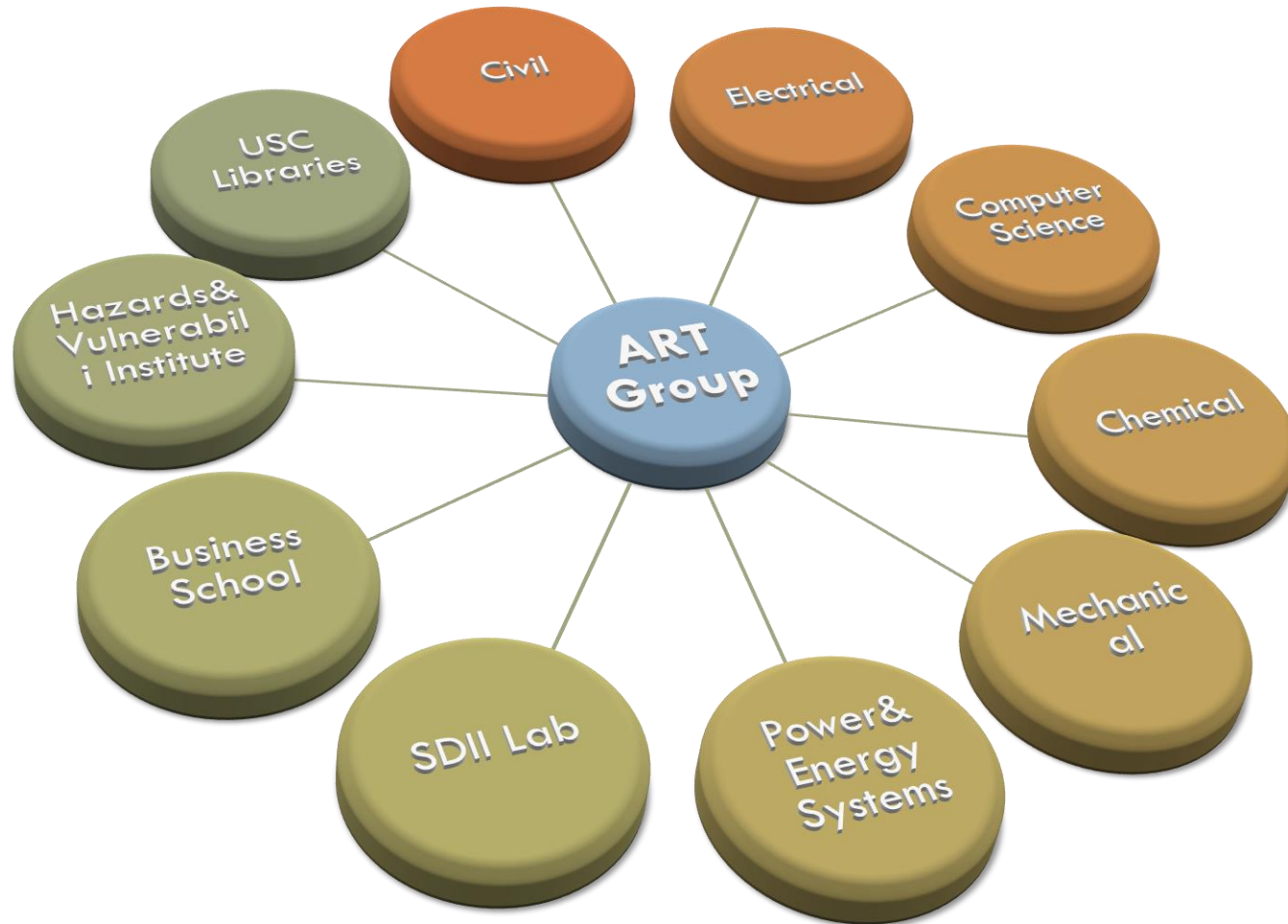


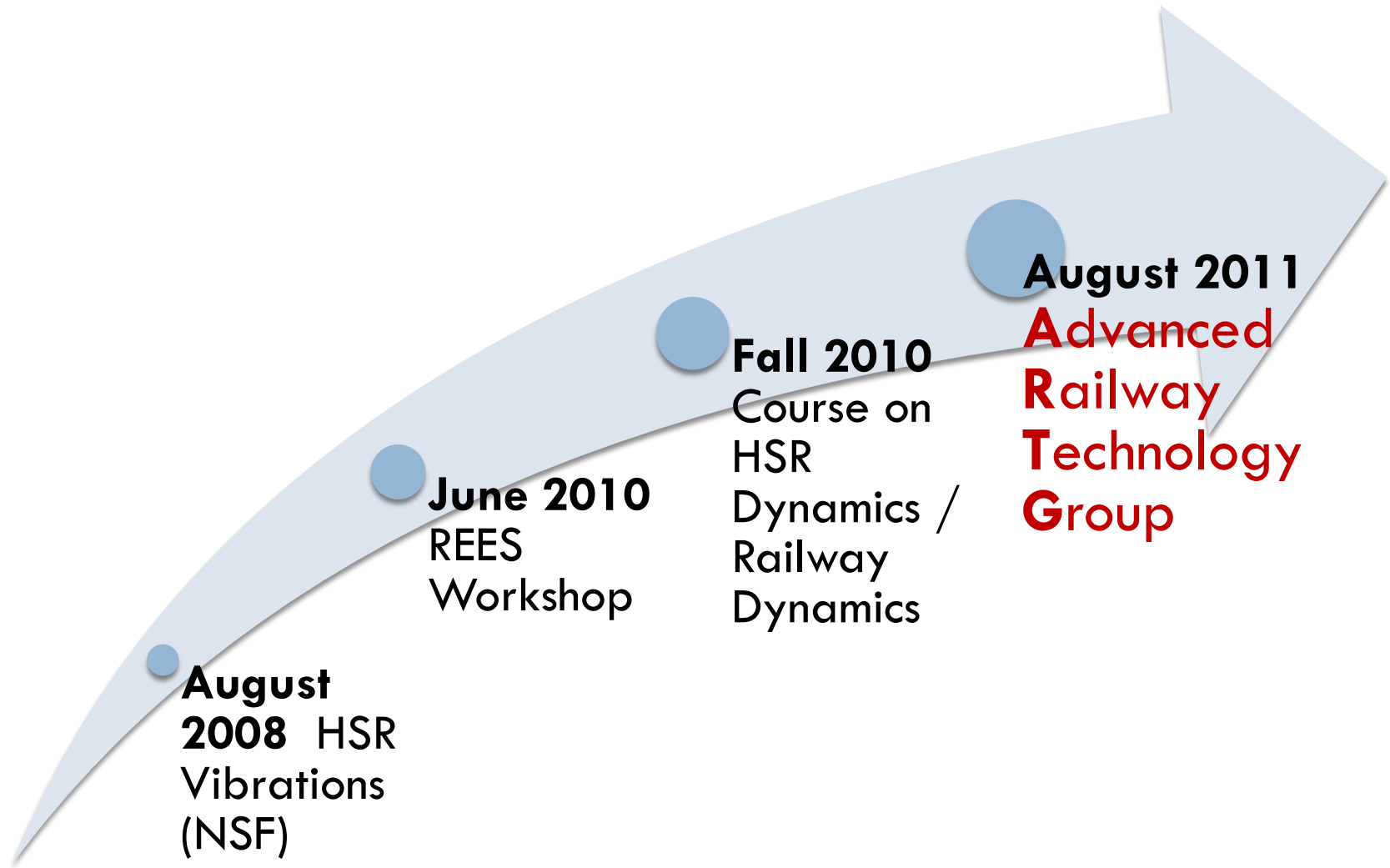
Nathan Huynh
Operations &
Logistics

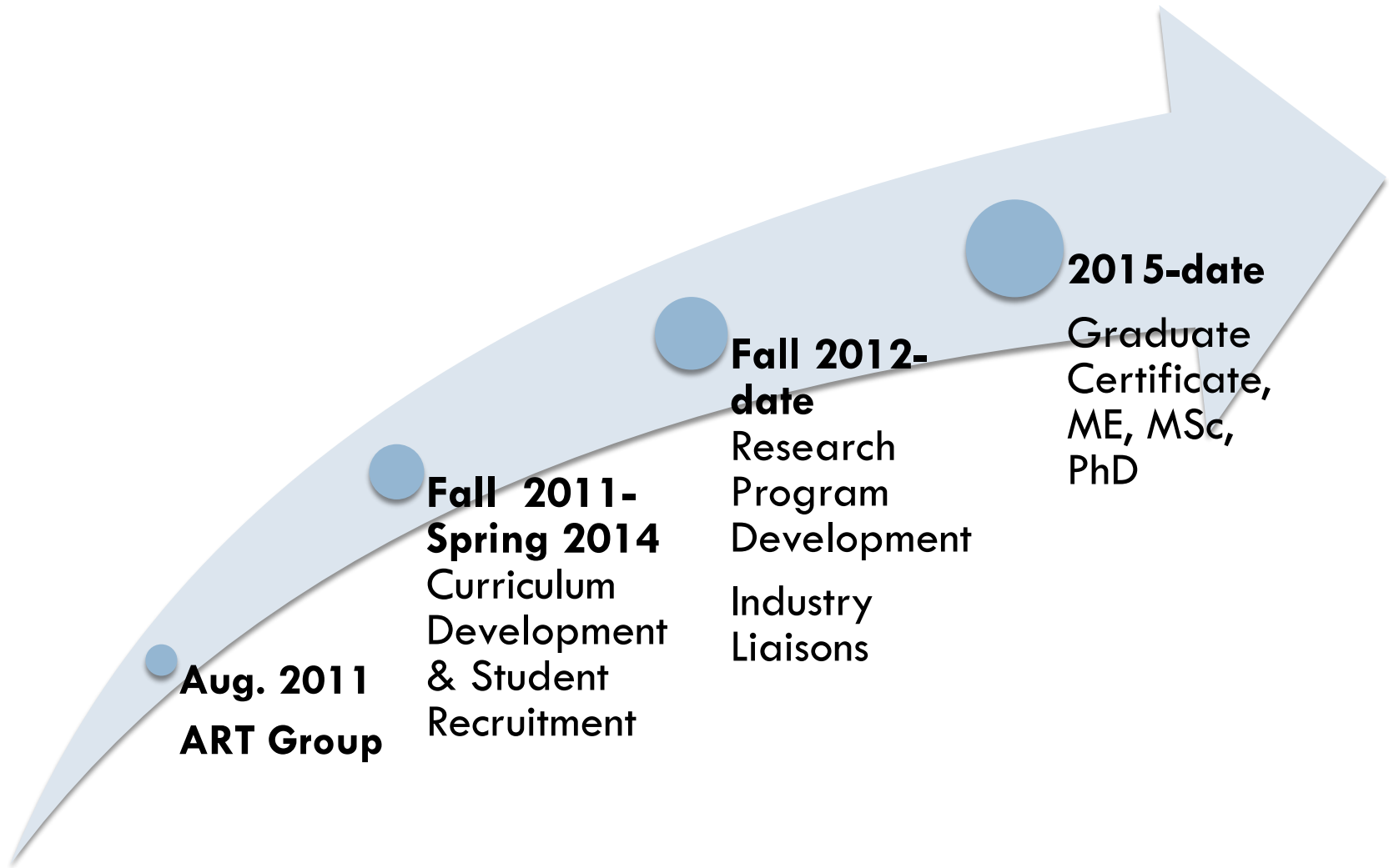


Dallas Richards
Education,
Industry Liaison









Course	Fall	Spr	Smr
ECIV 789: Design Project-Railroad Engineering		●	
ECIV 580: Infrastructure Planning and Design	●		
ECIV 581: Infrastructure Maintenance and Inspections	○		
ECIV 582: Operations and Logistics		●	
ECIV 588: Analysis & Design of Railroad Bridges	●		
ECIV 784: Dynamics of Railway Systems		●	
ECIV 797: Multimodal Transportation Systems	●		
ECIV 707: Management of Engineering Projects			●
ECIV 708: Risk Analysis of Engineering Applications			●
MGMT 718: Management of Human Resources		●	

Over 250 students attended classes in the last 3 years

APOGEE

A Program of Graduate Engineering Education

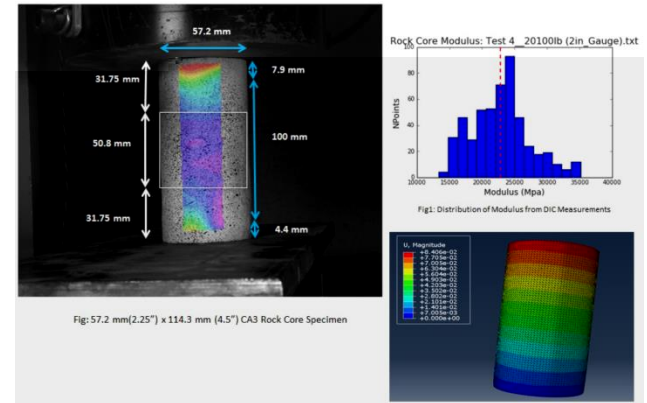
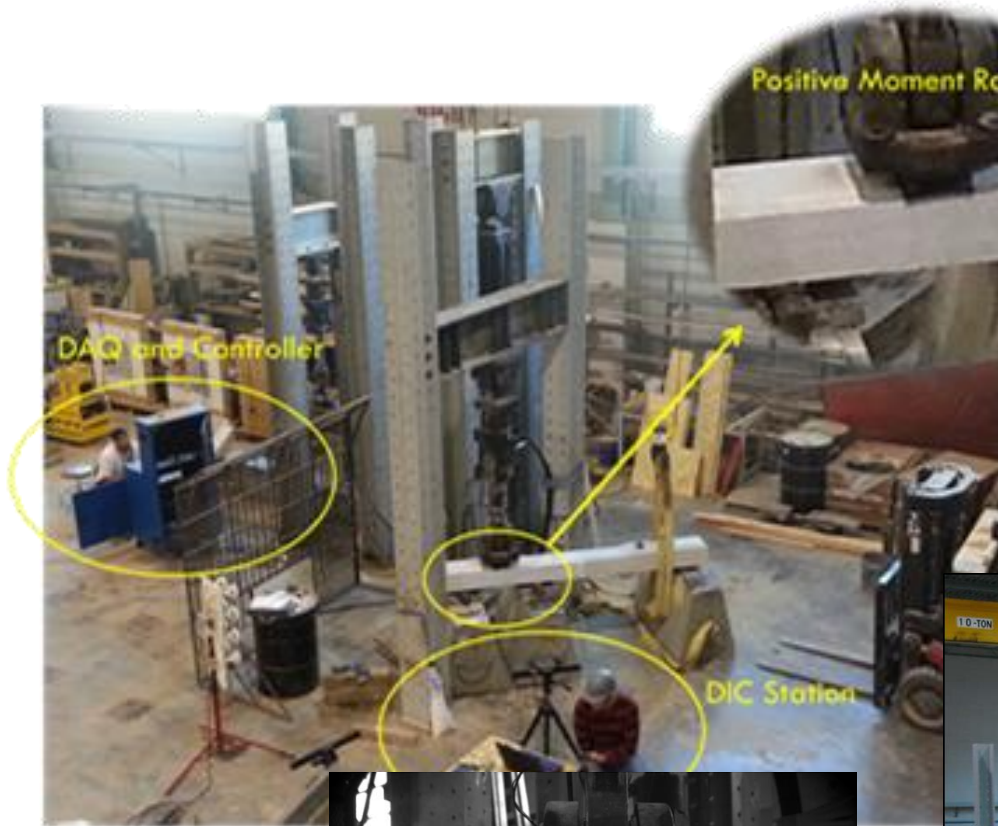
Help engineering professionals earn graduate credit/degree while maintaining full-time employment and without the constraints of on-campus attendance.

Allows instructors to deliver lectures from anywhere in the world

Facilitates the development of shared curricula

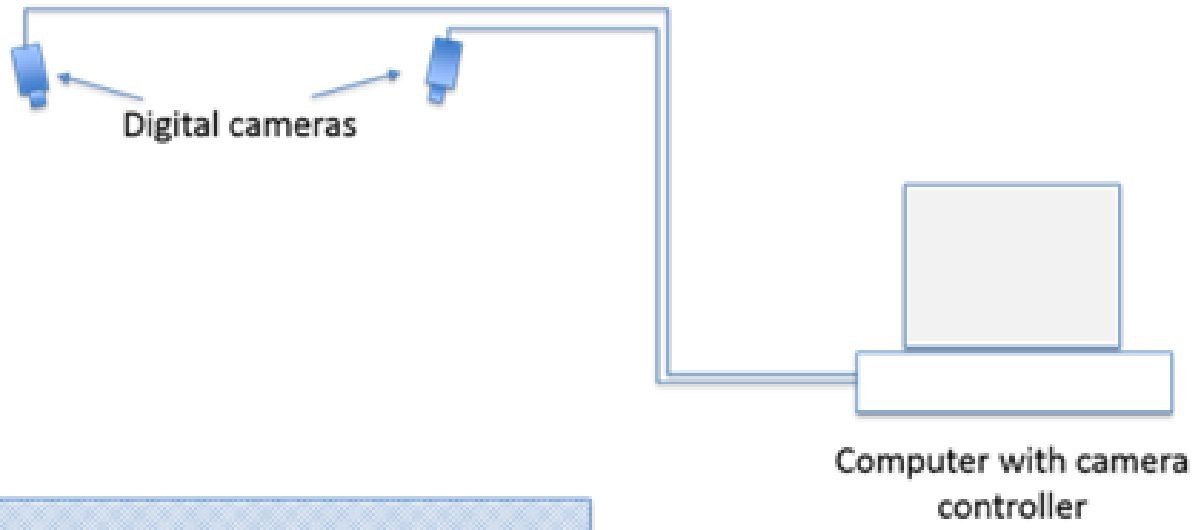


US News & World Report has awarded our APOGEE program “Best Online Programs Graduate Education 2013” with a rank of 28 in the nation.

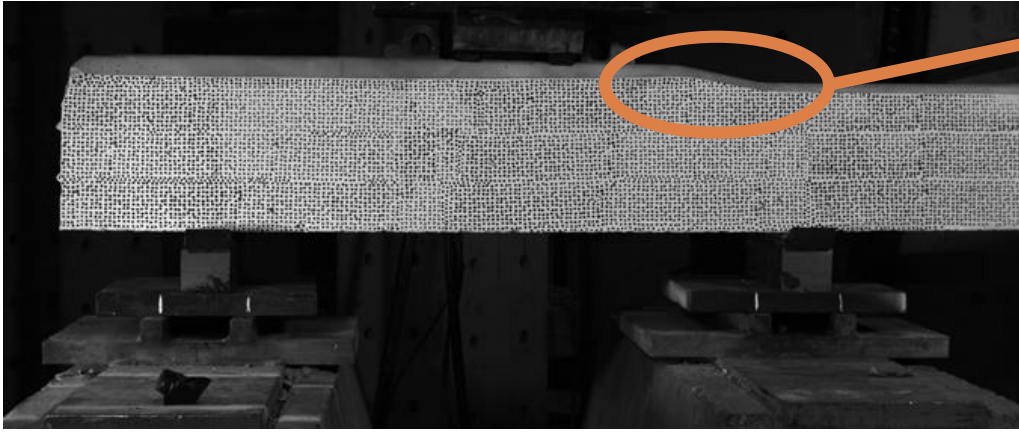




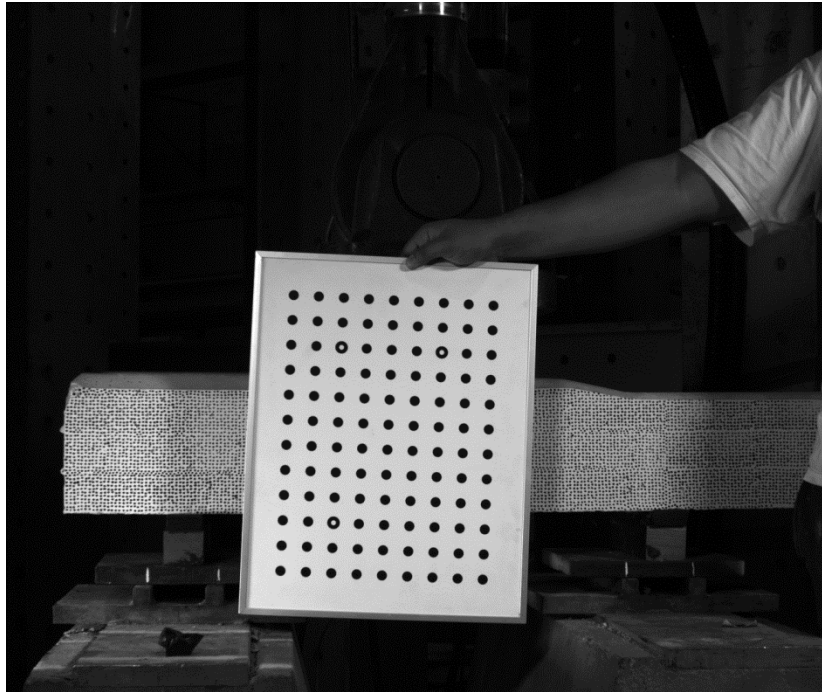
- 2D and 3D Systems Developed at the University of South Carolina over the last 30+ years
- Proven technology successfully applied to other industries
- Typical 3D System: 2 cameras and a computer setup
 - ▣ VIC-3D software by Correlated Solutions is used



Pre-stressed concrete with speckle pattern



System Calibration (50-100) images



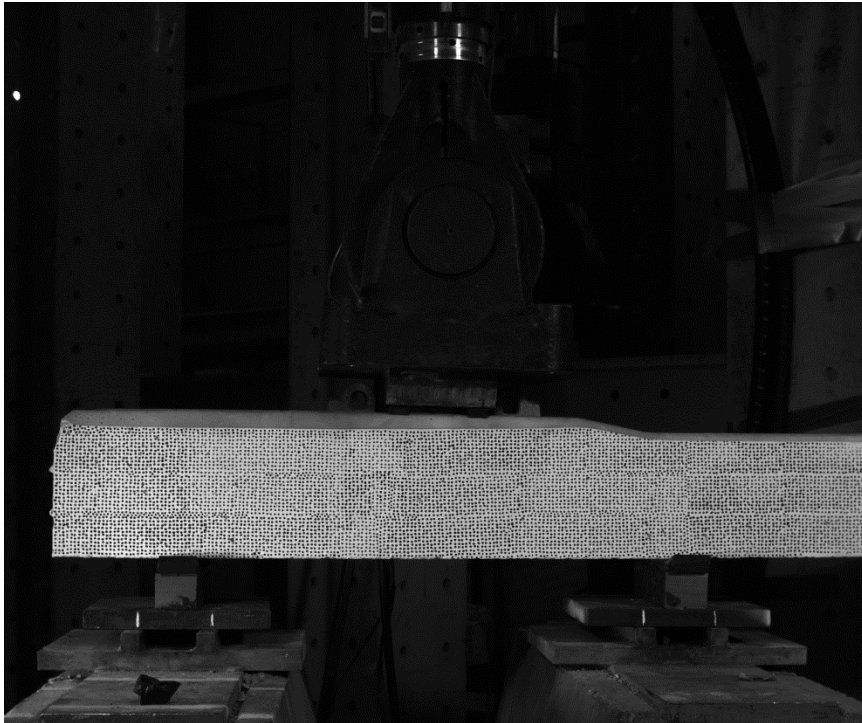
Project

Images Data Calibration

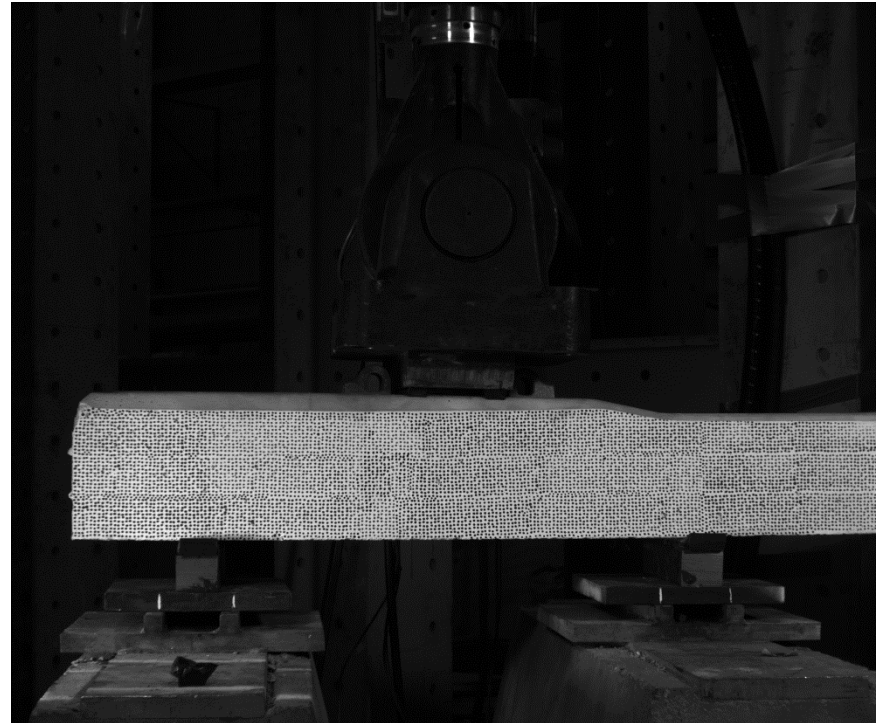
- ▲ Camera 1
 - Center x: 1686.41 pixel
 - Center y: 1331.03 pixel
 - Focal length x: 4795.94 pixel
 - Focal length y: 4799.28 pixel
 - Skew: -2.19237
 - Kappa 1: -0.16001
 - Kappa 2: 0
 - Kappa 3: 0
- ▲ Camera 2
 - Center x: 1682.76 pixel
 - Center y: 1296.27 pixel
 - Focal length x: 4761.49 pixel
 - Focal length y: 4764.16 pixel
 - Skew: -1.57112
 - Kappa 1: -0.16609
 - Kappa 2: 0
 - Kappa 3: 0
- ▲ Transformation
 - Alpha: 0.520279 deg
 - Beta: -3.09018 deg
 - Gamma: 0.764269 deg
 - Tx: 110.27 mm
 - Ty: 1.25525 mm
 - Tz: 2.64961 mm
 - Baseline: 110.309 mm

Take initial set of images before load is introduced SET 0

Left Camera – Set 0

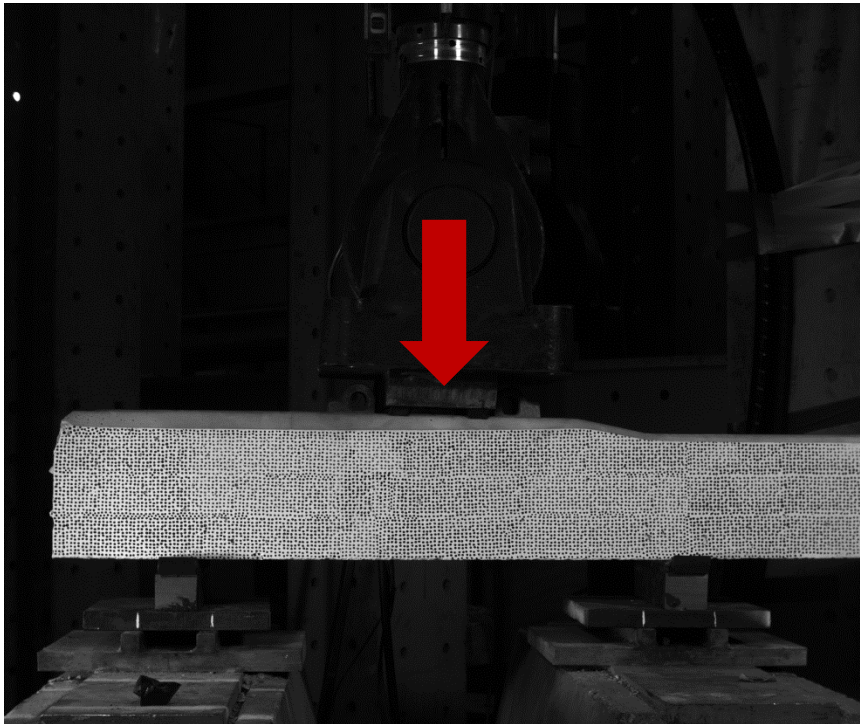


Right Camera – Set 0

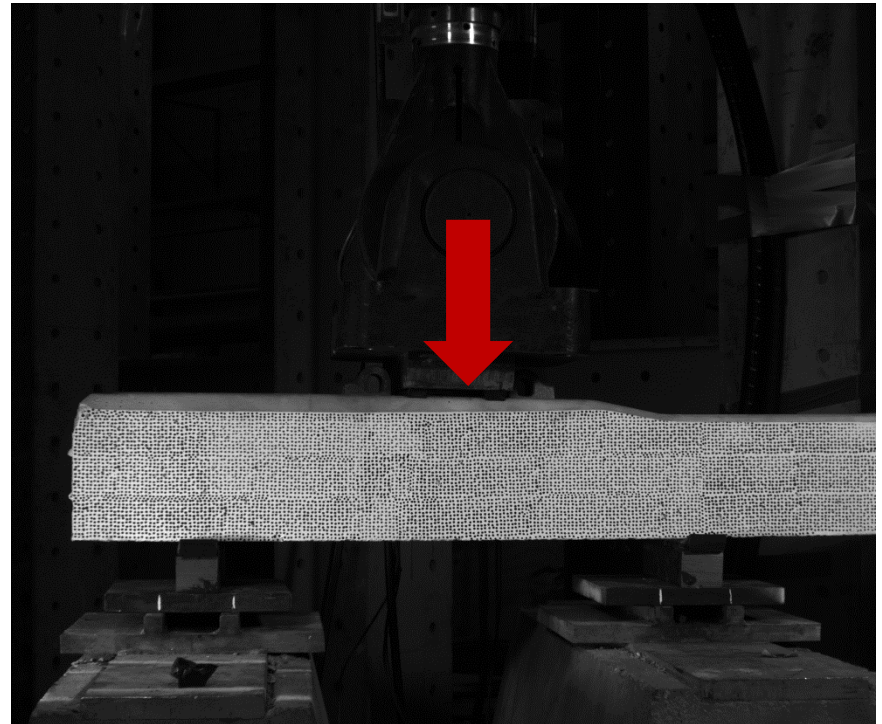


Load specimen

Left Camera

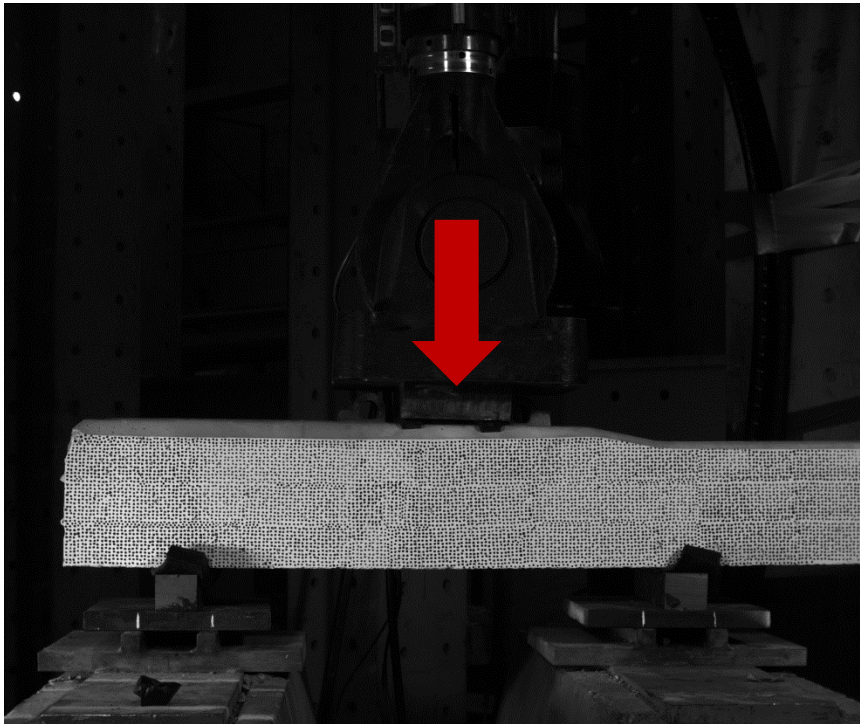


Right Camera

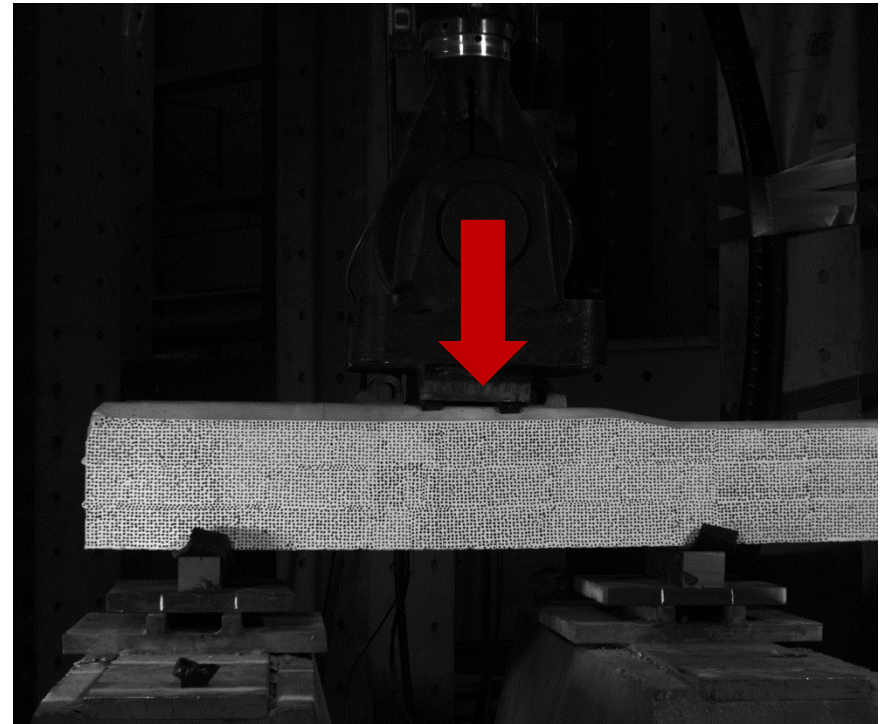


Take another set of images after load is applied SET 1

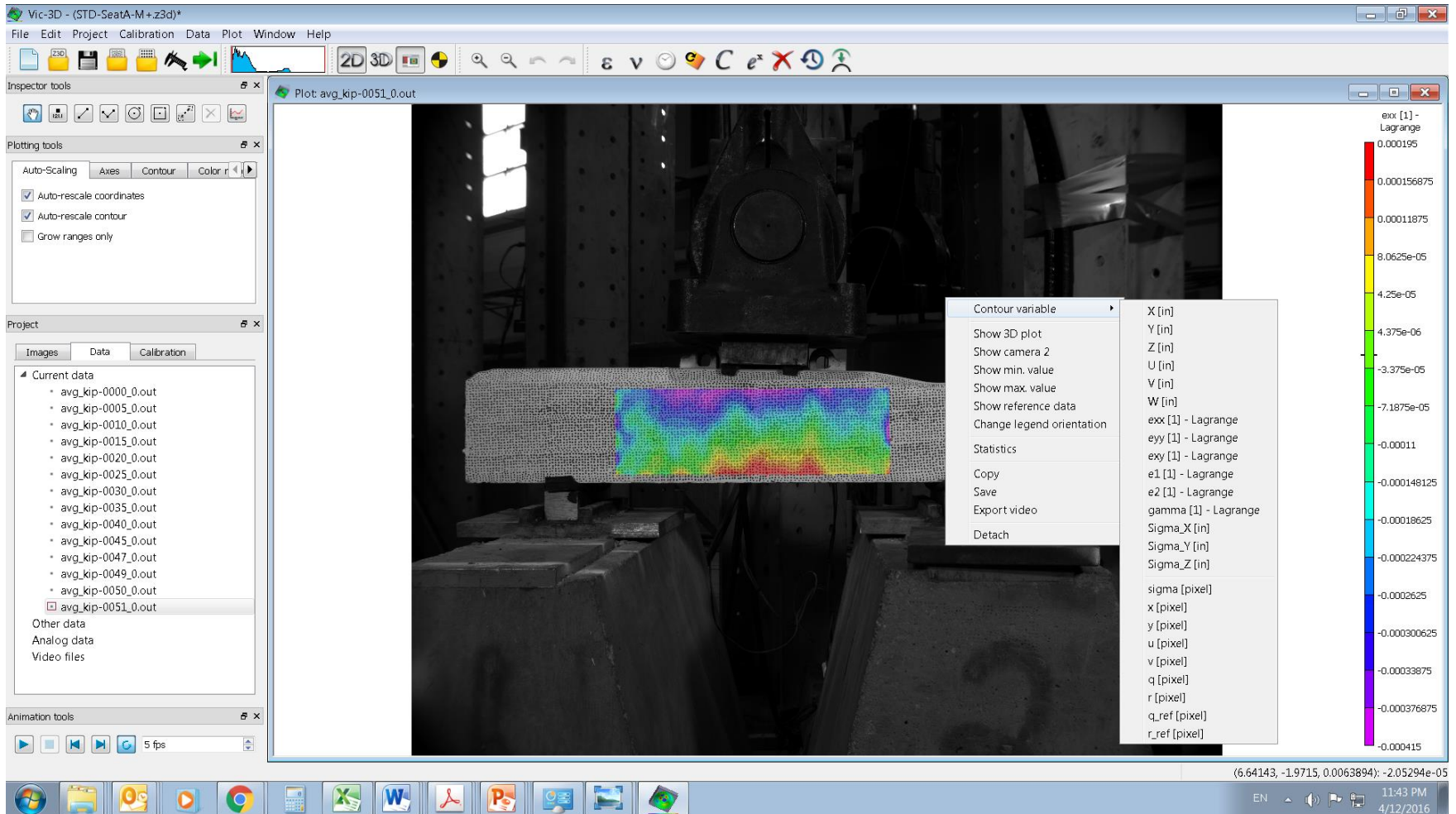
Left Camera – Set 1

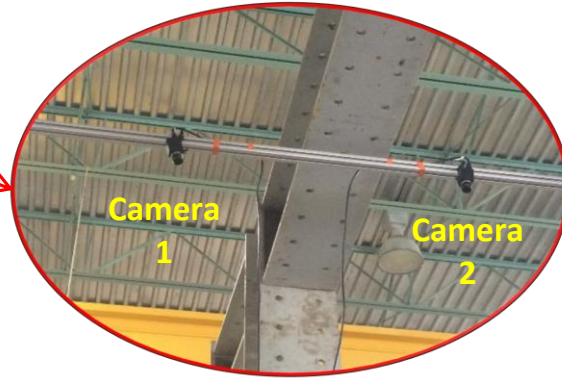
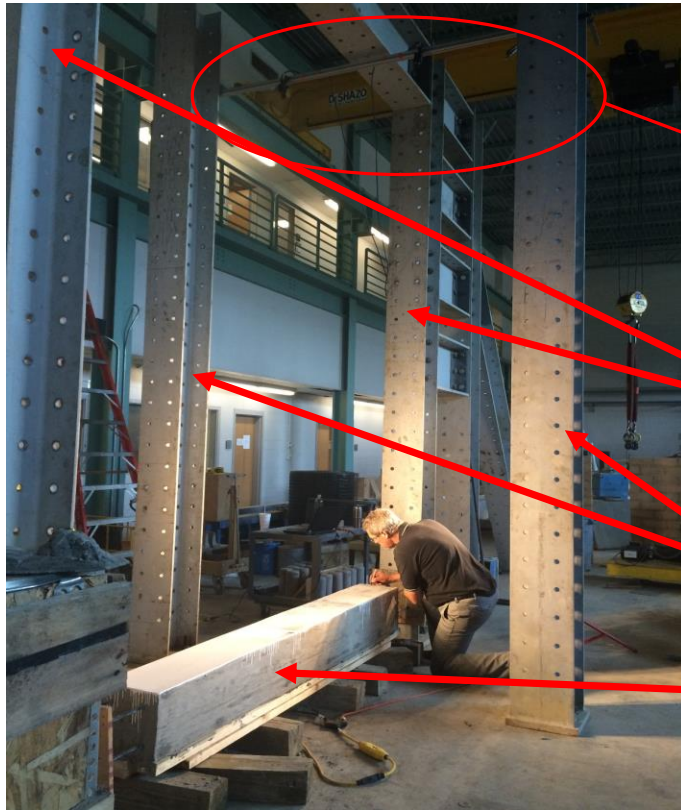


Right Camera – Set 1



Compute 3-D displacement and strain fields through image correlation of two sets





Strong-back for pretensioning of cables

Columns of Camera Frame

**Prestressed Prismatic Beams
2.4m X .3m X .3m**

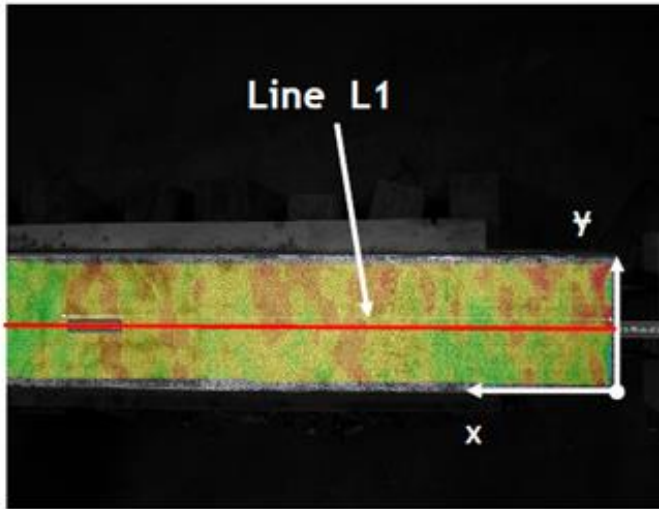
Laboratory Specimens



*Flame
cut*

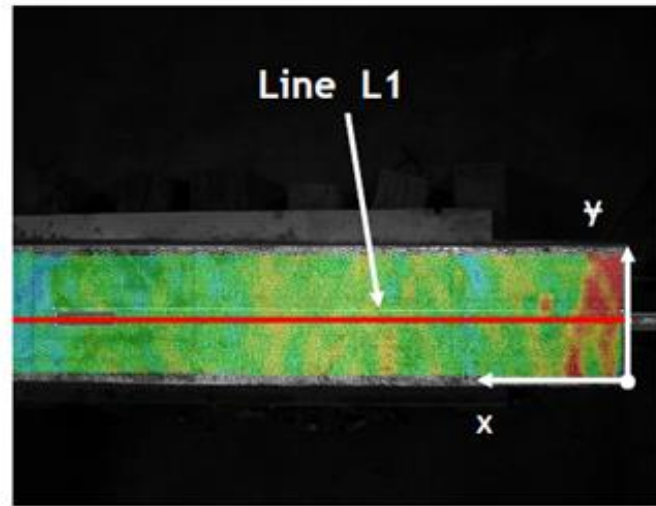


Flame Cut - Axial Strain Results



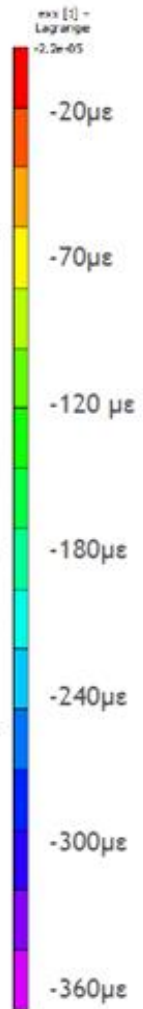
Top Two Cut

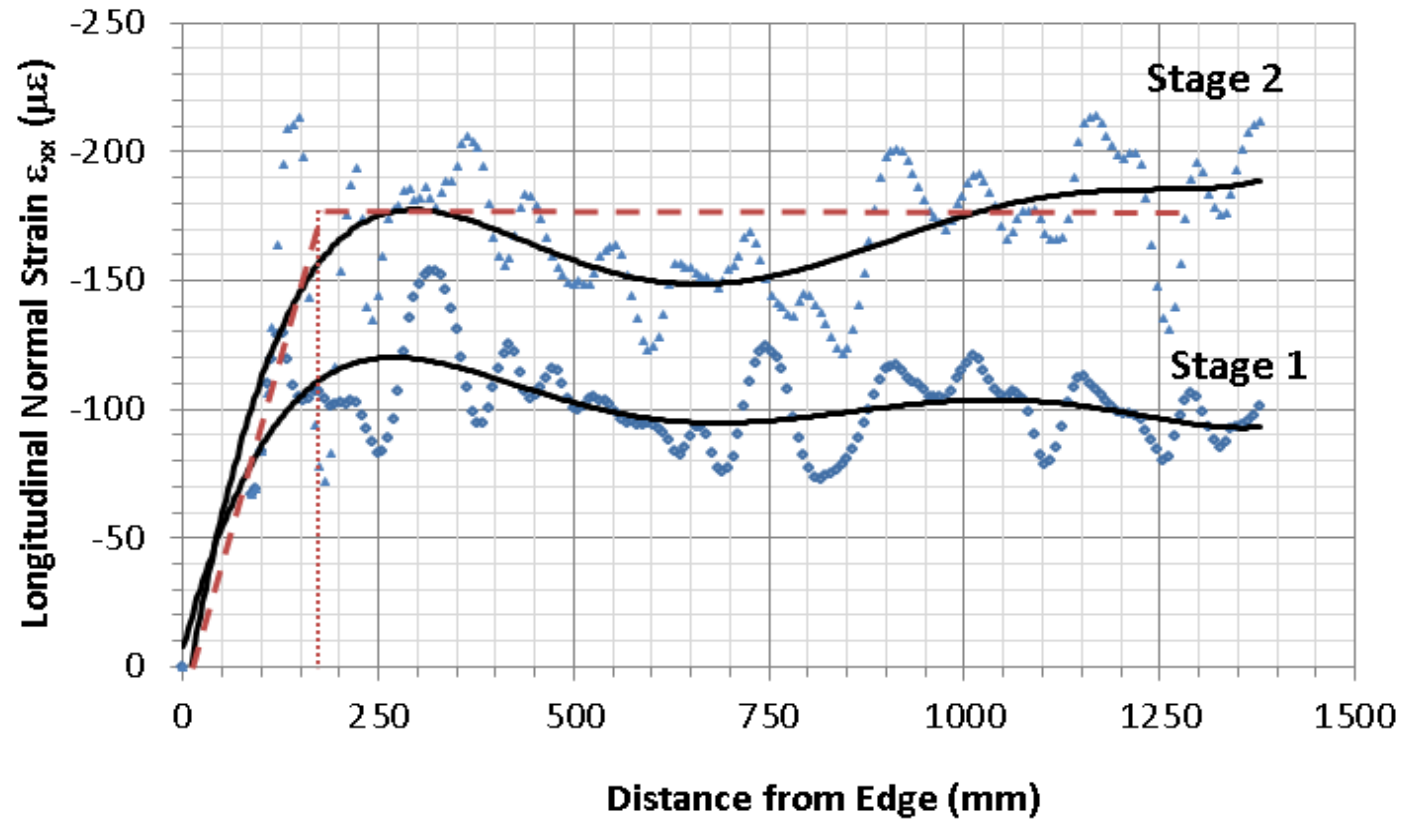
Avg strain: -110 $\mu\epsilon$



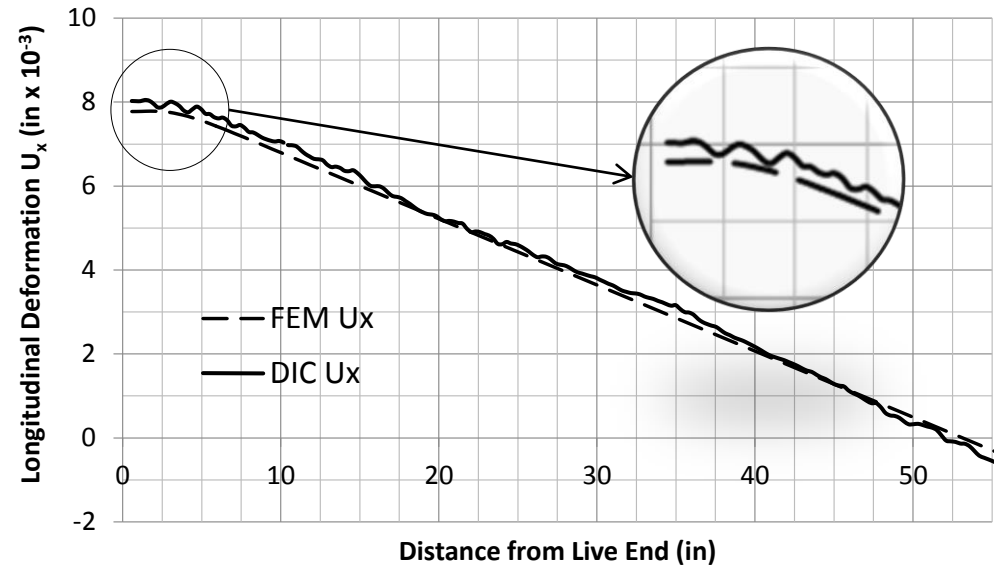
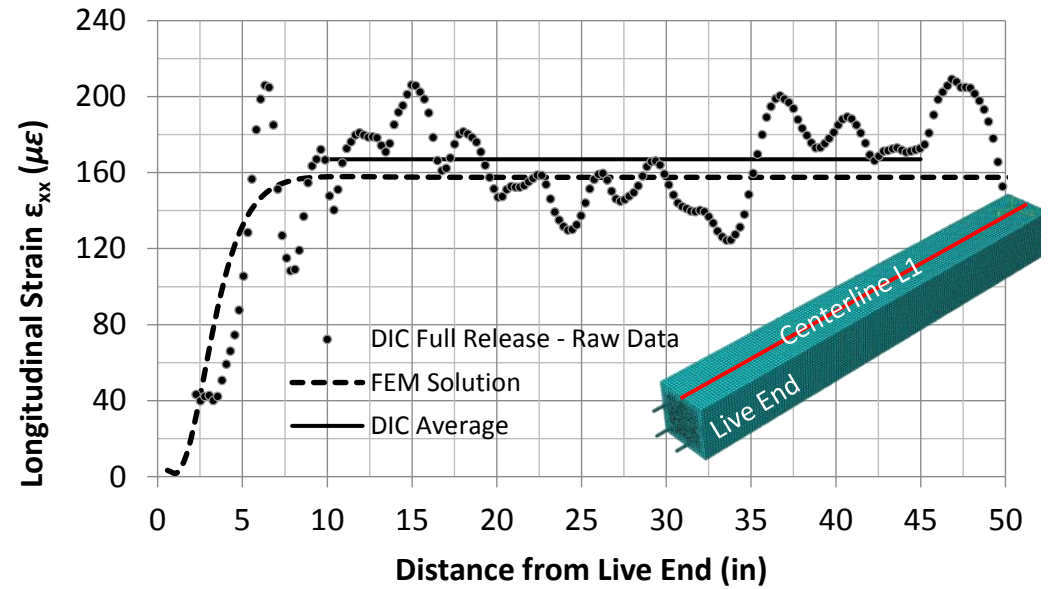
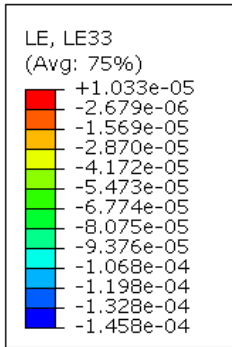
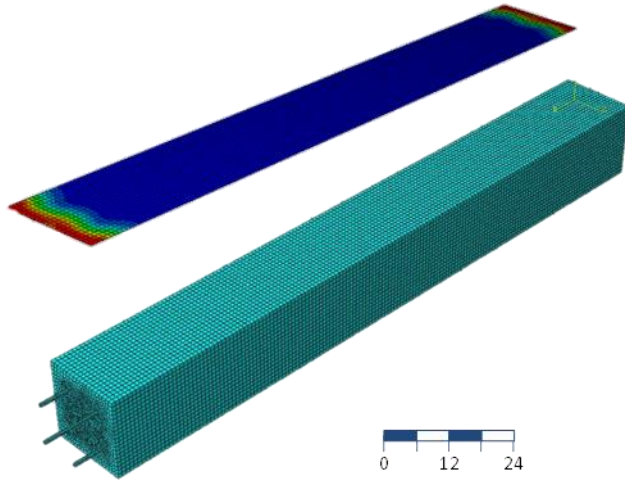
All Four Cut

Avg strain: -180 $\mu\epsilon$





Verification of results with strain gage measurements



Design of High Strength Low Modulus Concrete Crossties



UNIVERSITY OF
SOUTH CAROLINA

College of Engineering
and Computing



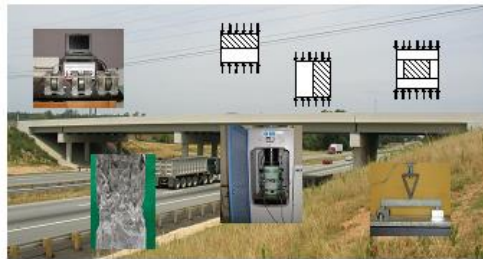
- ❑ Historical Background
- ❑ Hypothesis
- ❑ Material Development and Characterization
- ❑ Prototype Tie Design and Fabrication
- ❑ Product Qualification
- ❑ Benefits
- ❑ Conclusions

- ❑ **Historical Background**
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Permeability of Portland Cement Concrete (PCC) Structures in South Carolina –Volume II

Dr. Michael F. Petrou
 Dr. Dimitris C. Rizos
 Dr. Kent A. Harries
 Jean Hanson



submitted to
 The South Carolina Department of Transportation
 and
 The Federal Highway Administration
 March, 2004

This research was sponsored by the South Carolina Department of Transportation and the Federal Highway Administration. The opinions, findings and conclusions expressed in this report are those of the authors and not necessarily those of the SCDOT or FHWA. This report does not comprise a standard, specification or regulation.

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Report No. ST04-02
 FHWA-SC-04-04

SCDOT Research Project

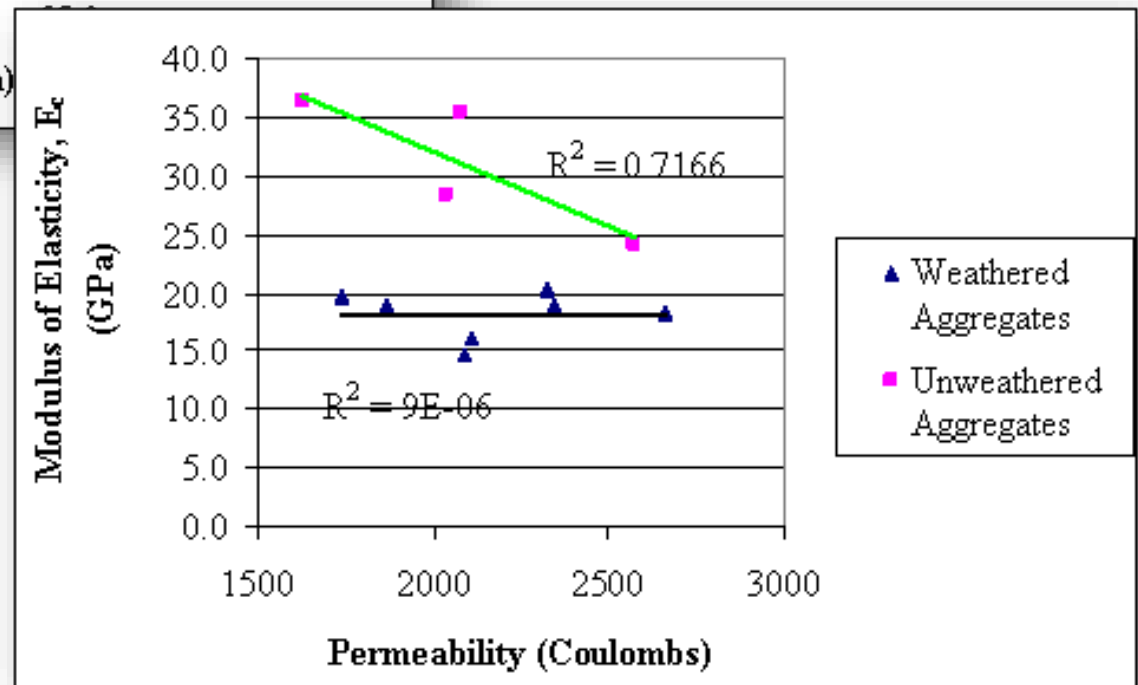
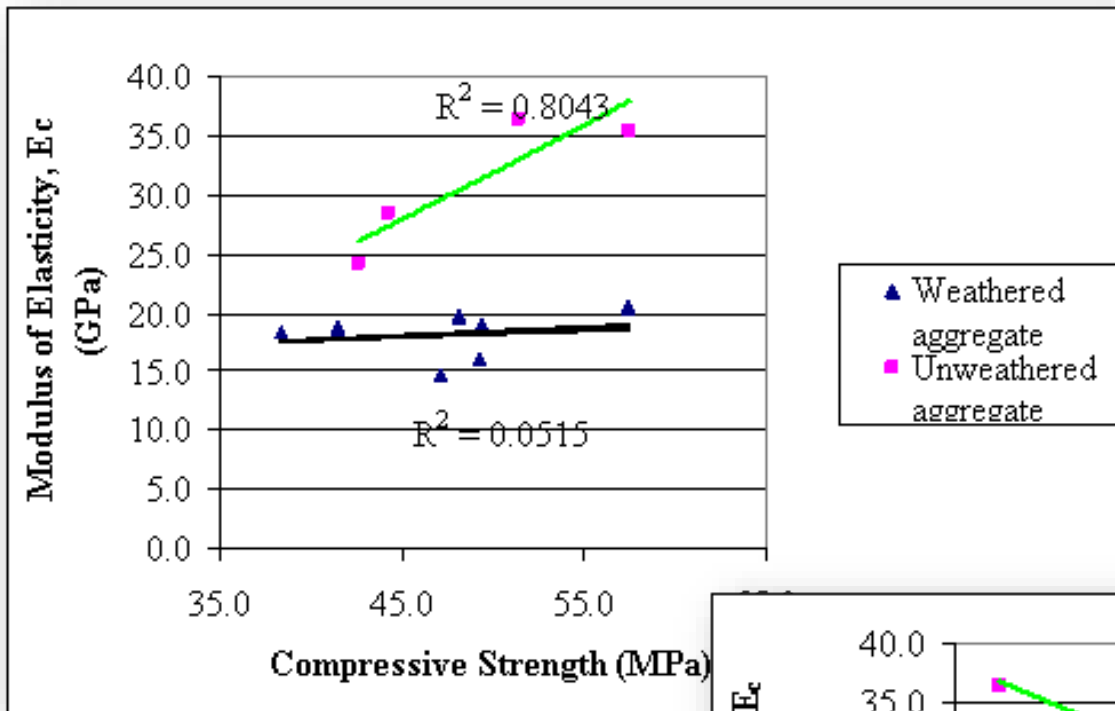
- ❑ HPC for Highway Bridges
- ❑ Local Aggregates
- ❑ SCDOT Mixture Designs

Table 2.1 Grades of Performance Characteristics for High Performance Structural Concrete (Goodspeed et al., 1996)

Performance Characteristic	Standard Test Method	FHWA HPC Performance Grade			
		1	2	3	4
Strength (x=compressive strength)	AASHTO T22 ASTM C39	$41 \leq x < 55$ MPa ($6 \leq x < 8$ ksi)	$55 \leq x < 69$ MPa ($8 \leq x < 10$ ksi)	$69 \leq x < 97$ MPa ($10 \leq x < 14$ ksi)	$x \geq 97$ MPa ($x \geq 14$ ksi)
Elasticity (x=modulus of elasticity)	ASTM C469	$28 \leq x < 40$ GPa ($4 \leq x < 6 \cdot 10^6$ psi)	$40 \leq x < 50$ GPa ($6 \leq x < 7.5 \cdot 10^6$ psi)	$x \geq 50$ GPa ($x \geq 7.5 \cdot 10^6$ psi)	
Shrinkage (x=microstrain)	ASTM C157	$800 > x \geq 600$	$600 > x \geq 400$	$400 > x$	
Creep (x=microstrain/pressure unit)	ASTM C512	$75 \geq x \geq 60$ /MPa ($0.52 \geq x \geq 0.41$ /psi)	$60 \geq x > 45$ /MPa ($0.41 \geq x > 0.31$ /psi)	$45 \geq x > 30$ /MPa ($0.31 \geq x > 0.21$ /psi)	$30/\text{MPa} \leq x$ ($0.21/\text{psi} \leq x$)
Freeze-thaw durability (x=relative dynamic modulus of elasticity at 300 cycles)	AASHTO T161 ASTM C666 (Procedure A)	$60\% \leq x < 80\%$	$80\% \leq x$		
Scaling (x= visual rating of the surface after 50 cycles)	ASTM C672	x=4,5	x=2,3	x=0,1	
Abrasion (x= average depth of wear)	ASTM C944	$2.0 > x > 1.0$ mm ($0.08 > x > 0.04$ in.)	$1.0 > x \geq 0.5$ mm ($0.04 > x > 0.02$ in.)	$x < 0.5$ mm ($x < 0.02$ in.)	
Chloride Penetration (x=Coulombs)	AASHTO T277 ASTM C1202	$3000 \geq x > 2000$	$2000 \geq x > 800$	$800 \geq x$	

- ❑ Aggregates from specific quarries
- ❑ HPC Classified as Grade 1 or 2 based on most properties
- ❑ Did not meet Grade based on Elastic Modulus
- ❑ HPC Rejected

Performance Characteristic	Standard Test Method	Batch No.	Experimental Results	FH\ Perform. Grade
Strength (MPa (psi))	ASTM C39	1	47.5 (6890)	1
		2	51.9 (7525)	1
		3	55.2 (8003)	2
		4	57.6 (8360)	2
Elasticity (GPa (ksi))	ASTM C469	1	21.3 (3089)	< 1
		2	19.4 (2811)	< 1
		3	24.1 (3492)	< 1
		4	24.1 (3501)	< 1
Shrinkage (microstrain)	ASTM C157	Shrinkage tests were not performed		
Creep (microstrain/pressure unit)	ASTM C512	Creep tests were not performed.		
Freeze-thaw durability (relative dynamic modulus of elasticity at 300 cycles, %)	ASTM C666 (Procedure A)	1	---	---
		2	---	---
		3	---	---
		4	>90	2
Scaling (visual rating of the surface after 50 cycles)	ASTM C672	1	4	1
		2	3	2
		3	---	---
		4	---	---
Abrasion (average depth of wear, mm (in.))	ASTM C944	1	1.410 (0.0555)	1
		2	1.711 (0.0674)	1
		3	---	---
		4	---	---
Sulfate Penetration (Coulombs)	ASTM C1202	1	2144	1
		2	2632	1
		3	2683	1
		4	1065	2

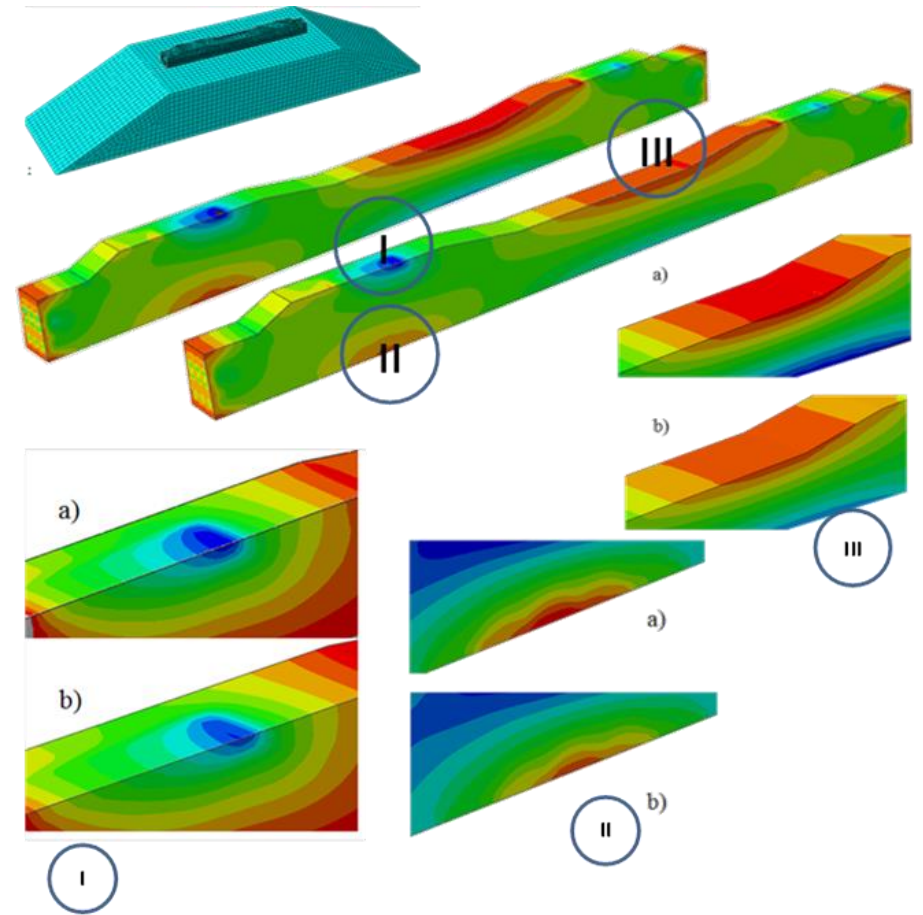


- ❑ Historical Background
- ❑ **Hypothesis**
- ❑ Material Development and Characterization
- ❑ Prototype Tie Design and Fabrication
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Benefits of Using Higher Resilience Concrete in Prestressed Ties:

- ❑ Better load distribution
- ❑ Smoother stress gradient
- ❑ Lower stress amplitudes
- ❑ Delay of onset of damage
- ❑ Relative rigidity

Critical Location	Stress Reduction due to HSRM-HPC [%]
I	15%
II	50%
III	48%



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- ▶ US Major Tie Manufacturer Design
 - ▶ Min. 28 Day = 7000psi
 - ▶ Min. Transfer Strength = 4000psi
- ▶ Direct substitution of aggregates
- ▶ 4 Aggregate Sources
 - ▶ CA1: Plum Run Stone (Standard)
 - ▶ CA2: Weathered Granite Source A
 - ▶ CA3: Weathered Granite Source B
 - ▶ CA4: Weathered Granite Source C





Test		ASTM
Coarse Ag.	Los Angles Abrasion Test	C131
	Sieve Analysis (Particle Size Distribution)	C136
	Bulk Density and Voids	C29
	Density, Specific Gravity and Absorption	C127
Rock	Compressive Strength	D7012 - 14
	Modulus of Elasticity	D7012 - 14
Concrete	Slump	C143
	Density	C138
	Air Content by pressure method	C231
	Compressive Strength of Concrete	C39
	Flexural Strength of Concrete	C78
	Modulus of Elasticity of Concrete	C469
	Shrinkage	C157
Mortar	Compressive Strength	C 109- 13
	Tensile Strength	C 307-12
	Modulus of Elasticity	C 580-02
	Setting Time (Initial and Final)	C191 - 13

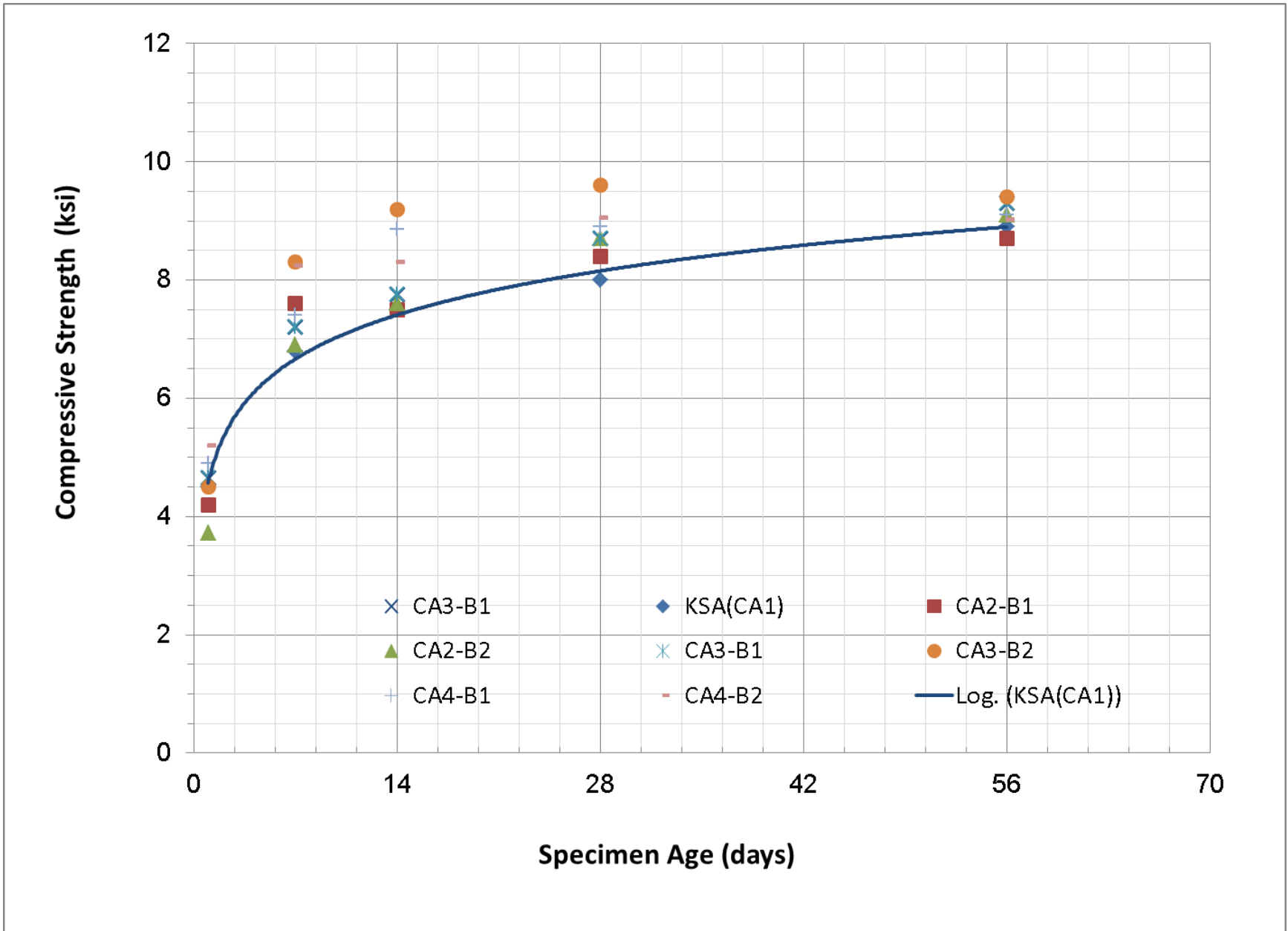
□ Durability - Abrasion

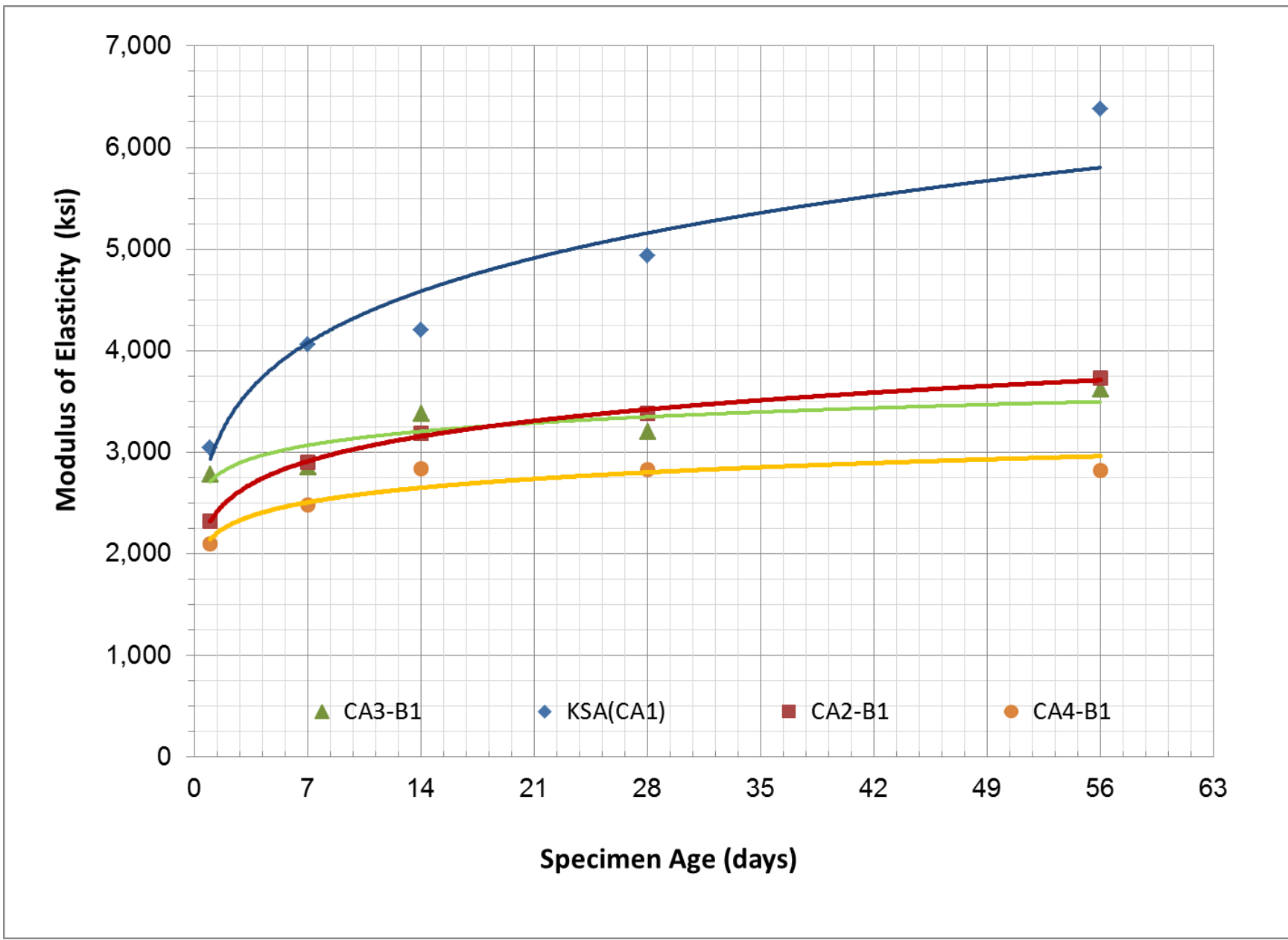
Procedures and Lapping Machine at UIUC

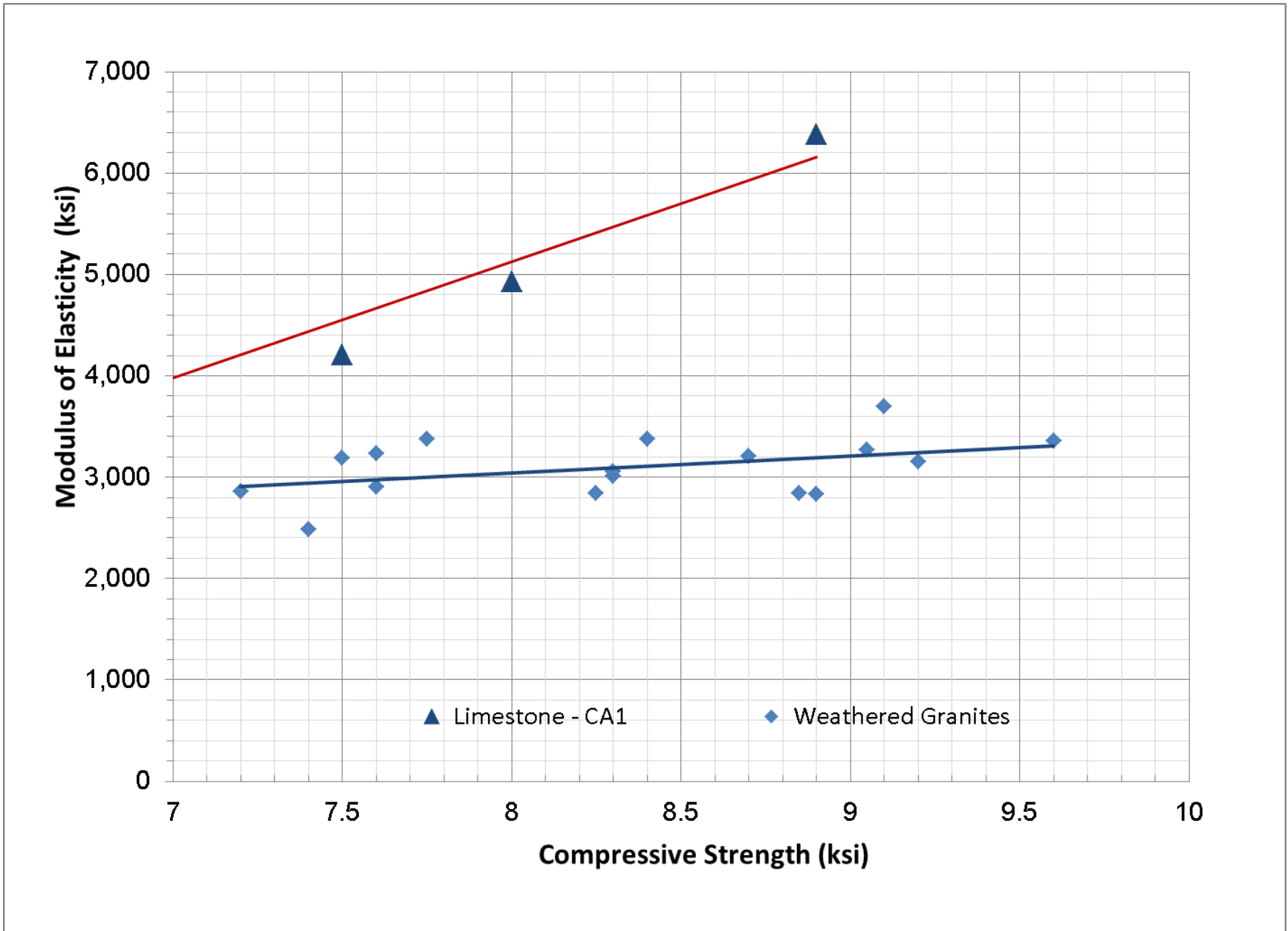
- 12 4x8 specimens from each Mix
- Specimens to UIUC on 6/22 (28 day min)



Abrasion Resistance Testing of Concrete Railway Crossties, E. Van Dam, et al. <http://www.purdue.edu/discoverypark/nextrans/assets/pdfs/Van%20Dam>



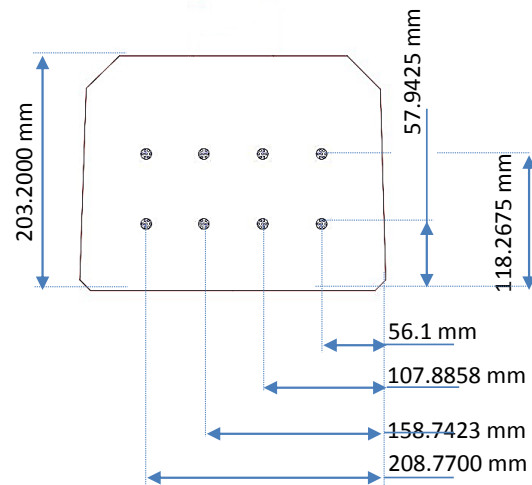
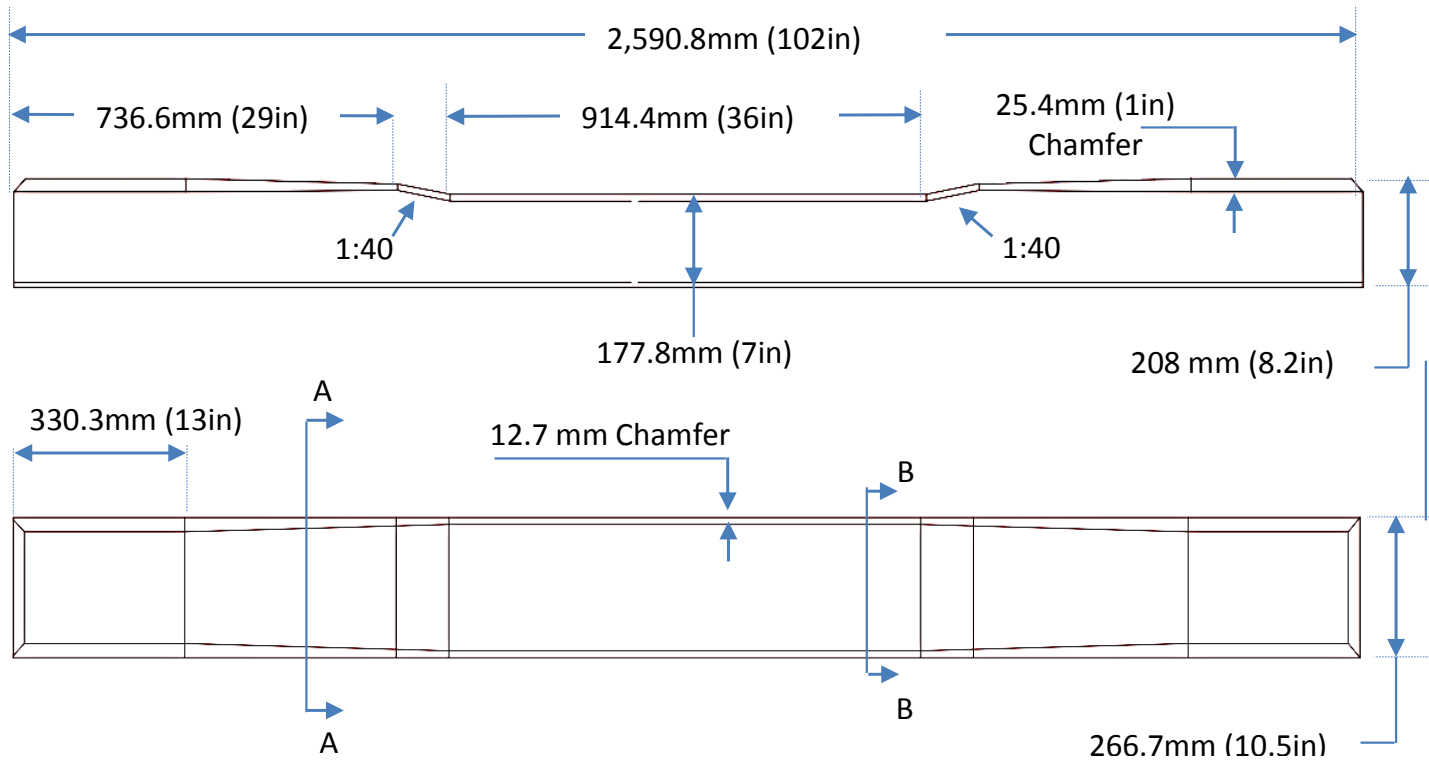




Property		AGGREGATE			
		KSA (CA1)	CA2	CA3	CA4
Aggreg	Voids	42.73	42.51	39.90	39.10
	Density (lb/ft ³)	161.65	164.50	165.00	167.50
	Relative Density	2.58	2.60	2.65	2.69
	LA Abrasion	27.5%	33.9%	44.3%	46.0%
Fresh Concr	Density (lb/ft ³)	152.90	153.73	154.14	158.55
	Yield (yd ³)	0.15	0.15	0.14	0.14
	Cement Content (lb/yd ³)	618.23	621.53	623.21	632.05
	Slump (in)	7.00	6.50	7.50	4.00
	Air Content (%)	5.0%	5.9%	4.8%	4.0%
Concrete	Compressive Strength (psi)	8.8E+03	8.8E+03	9.2E+03	8.7E+03
	<i>Increase/Reduction %</i>	0%	0%	4%	-1%
	Flexural Strength (psi)	0.13fc'	0.125fc'	0.12fc'	-
	Elastic Modulus (psi)	5.6E+06	3.6E+06	3.2E+06	2.8E+06
	<i>Elastic Modulus Reduction %</i>	0%	-37%	-43%	-50%
	Lapping Test Abrasion Rate (mm/min)	0.042	0.023	0.029	0.039

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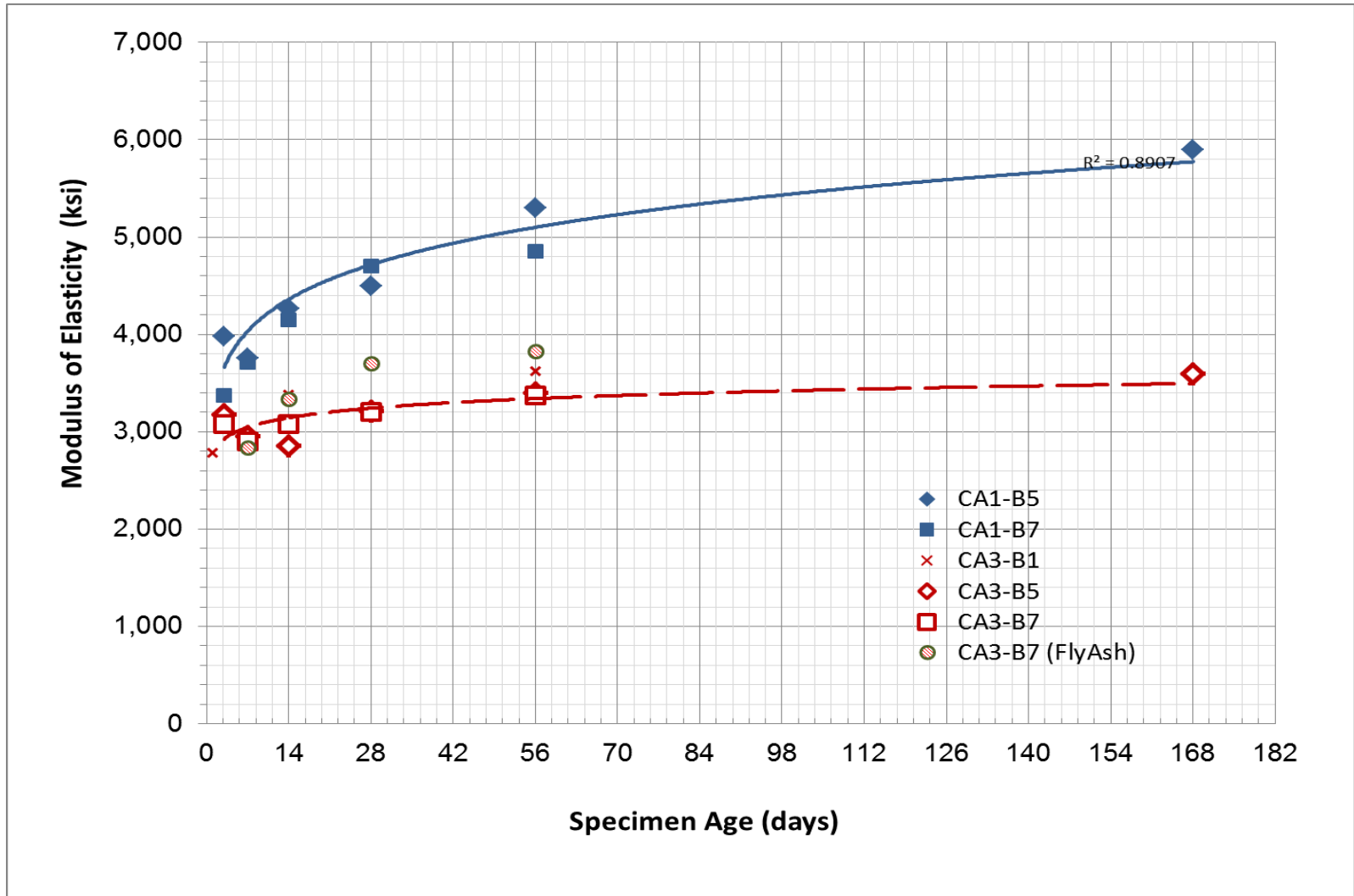
- Historical Background
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- **Prototype Tie Design and Fabrication**
 - 9/2015 and 7/2016
- Product Qualification
- Benefits
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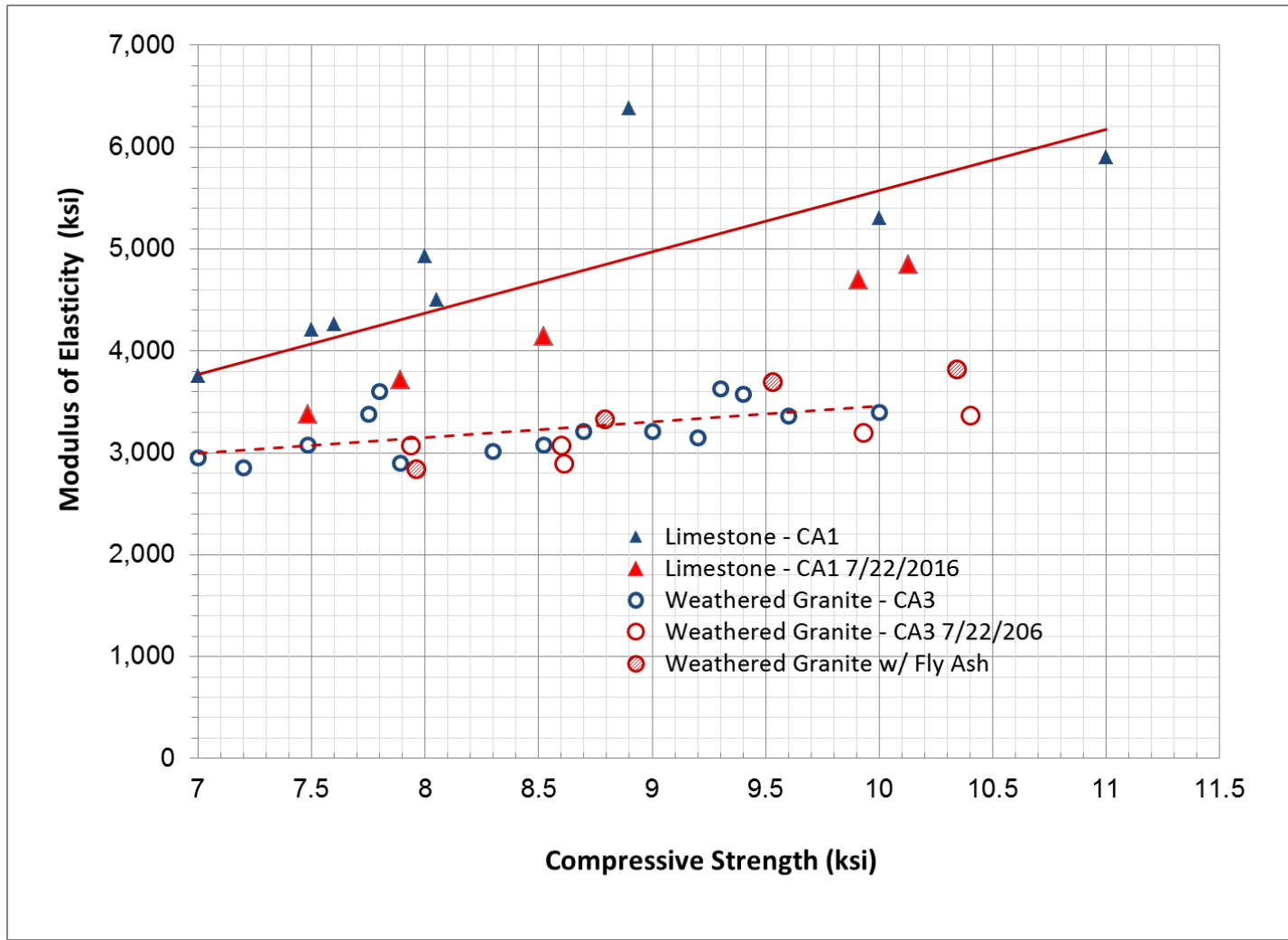


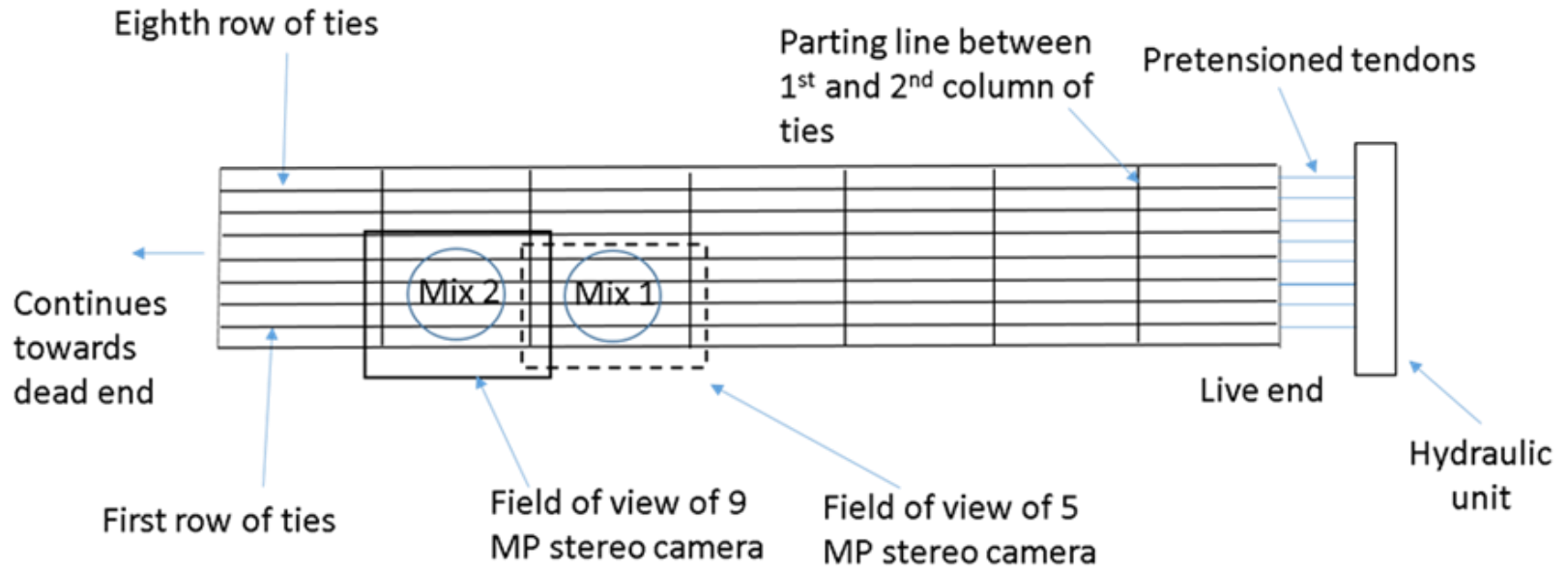


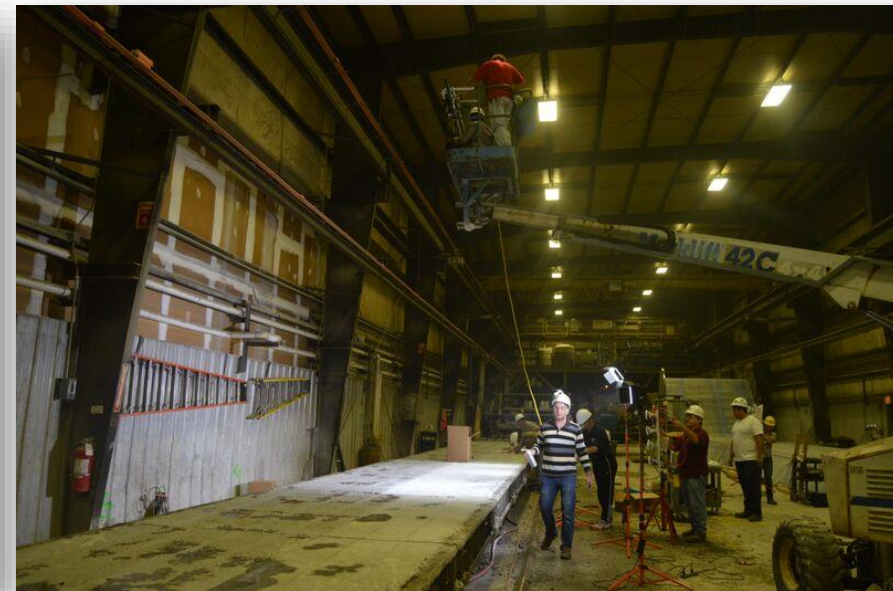




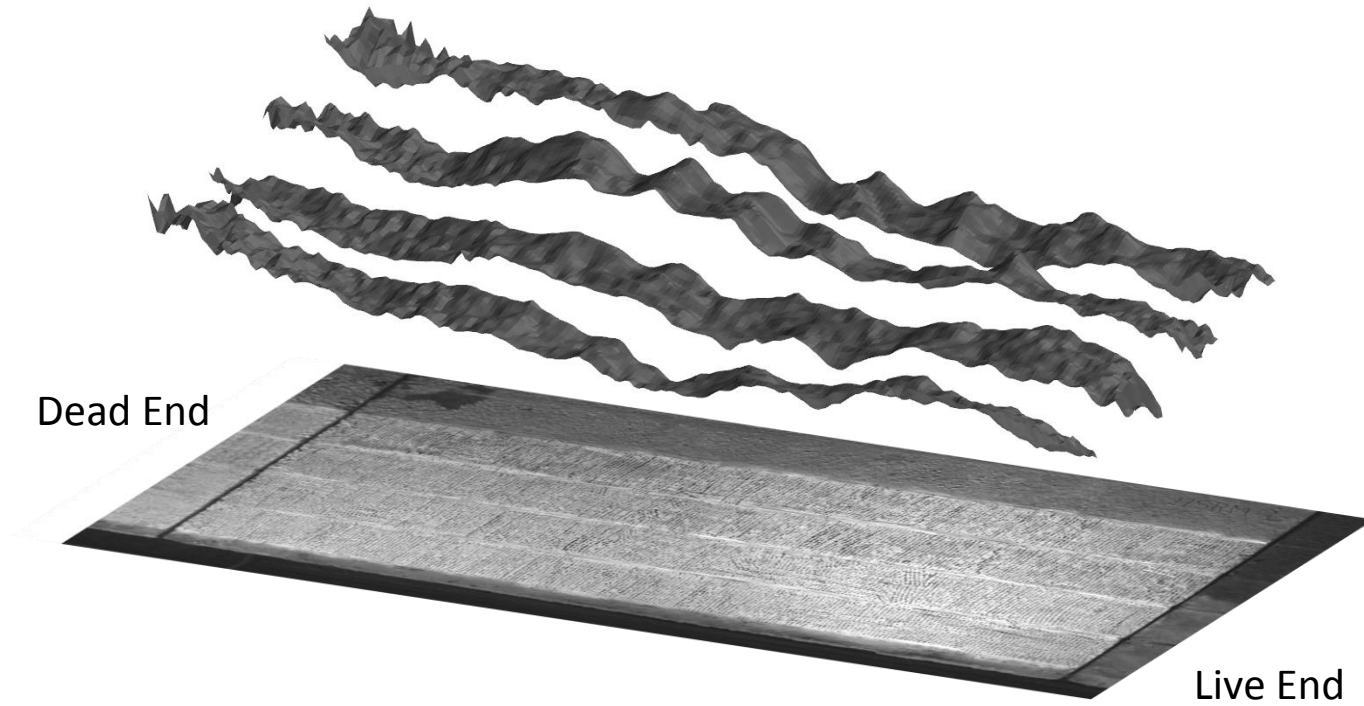


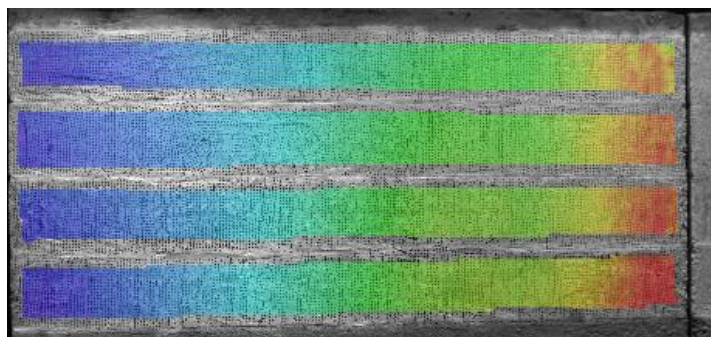






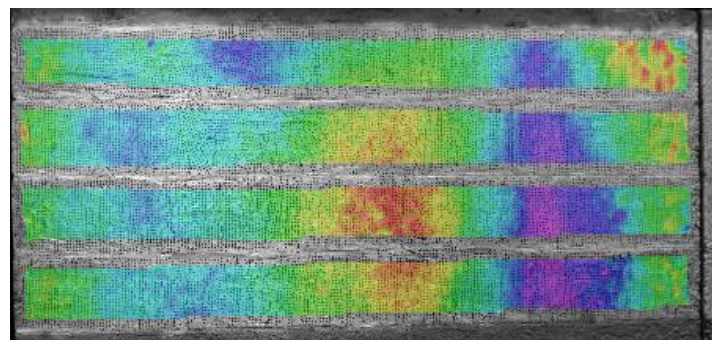






Live End

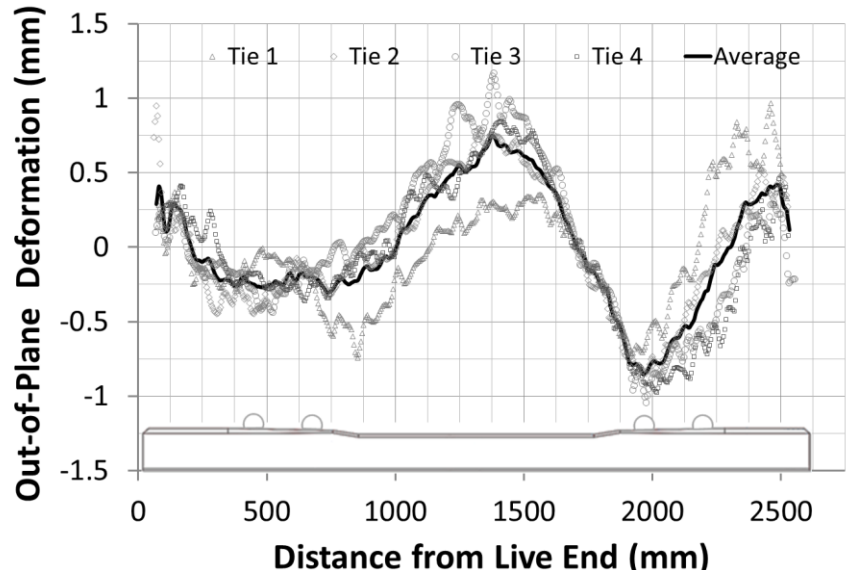
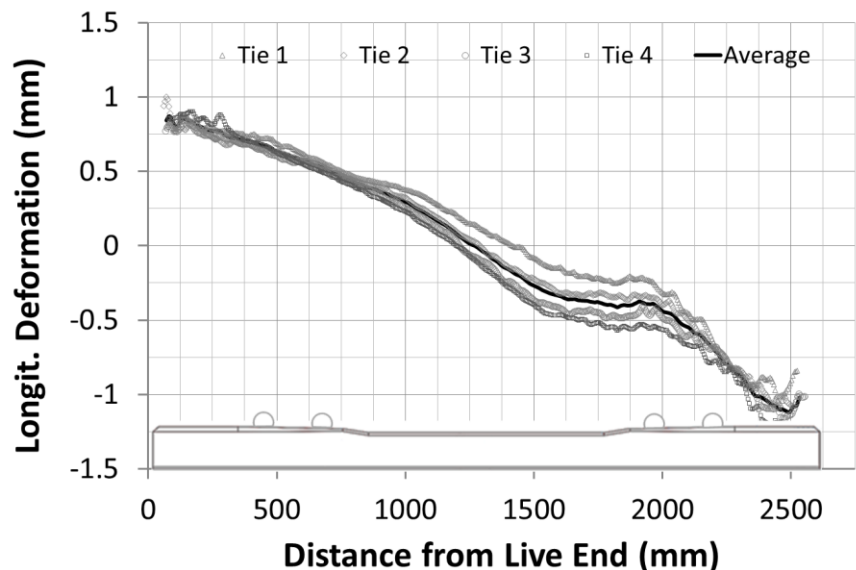
Dead End

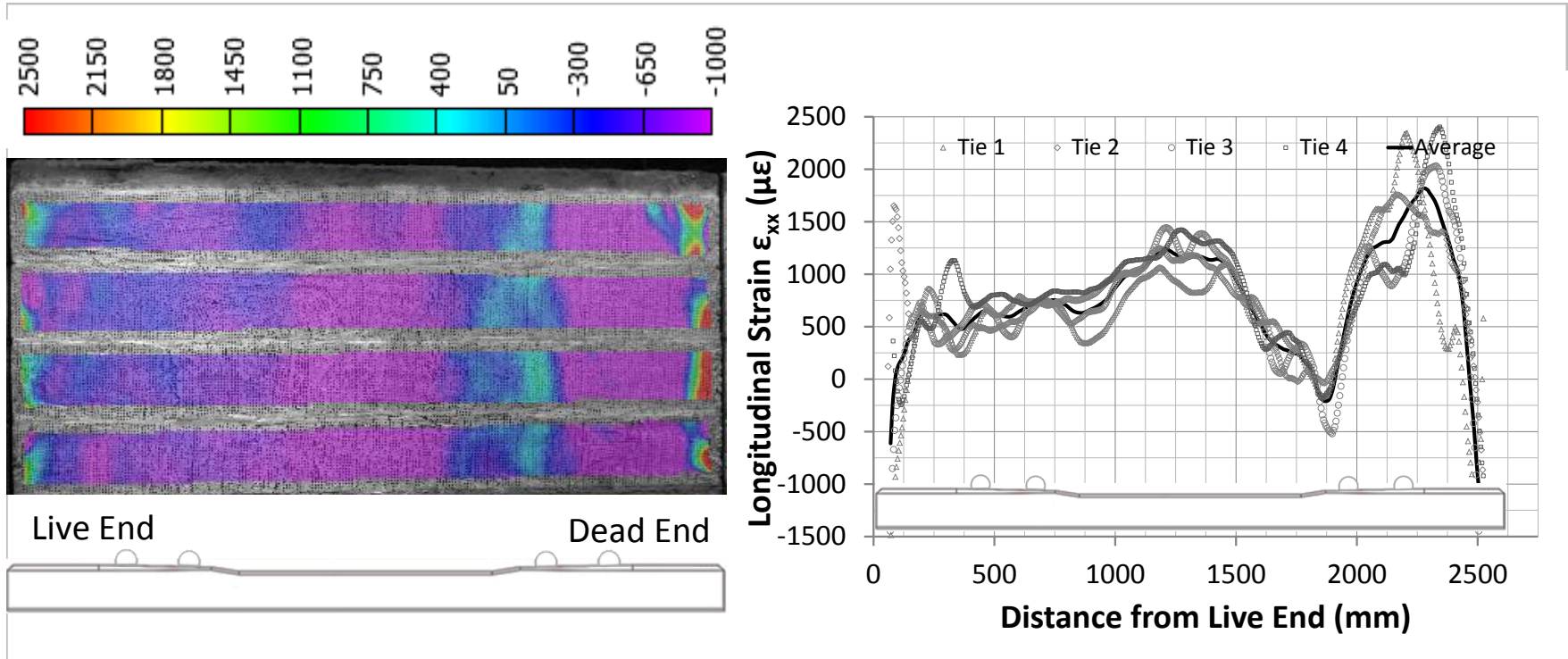


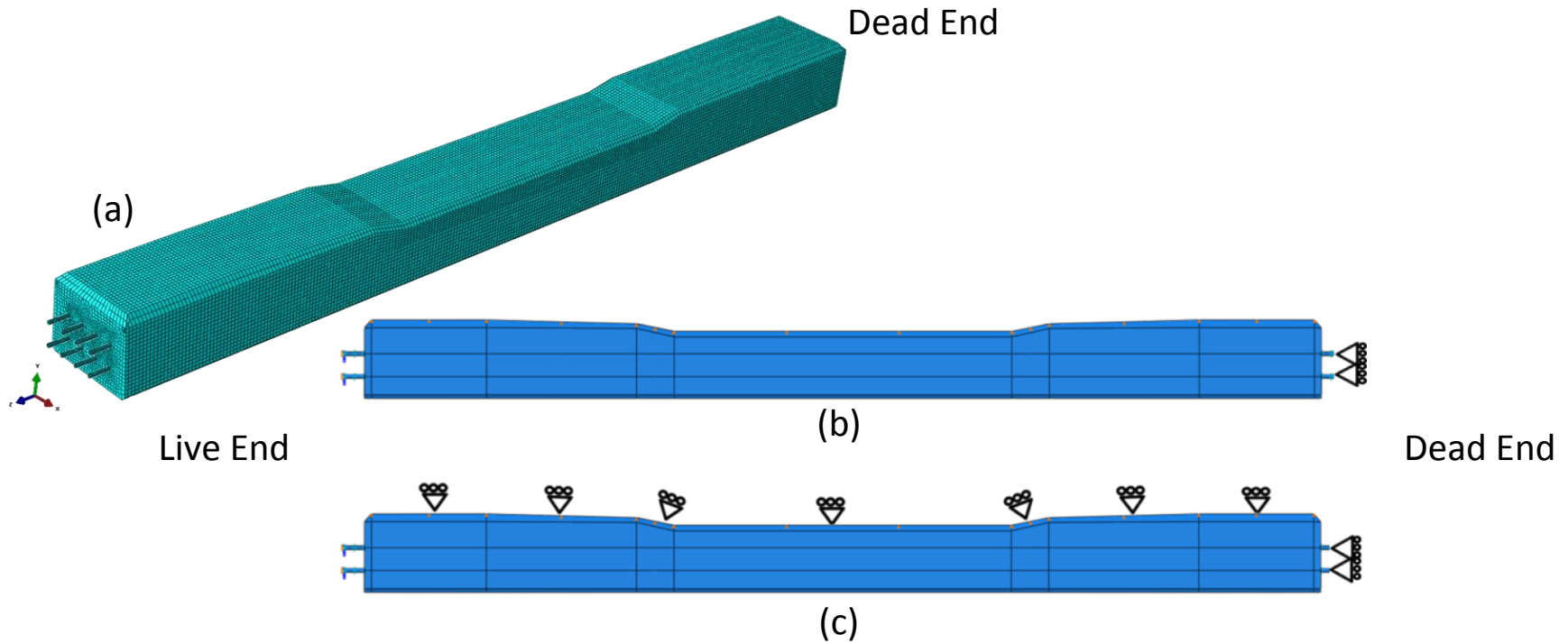
Tie 4
Tie 3
Tie 2
Tie 1

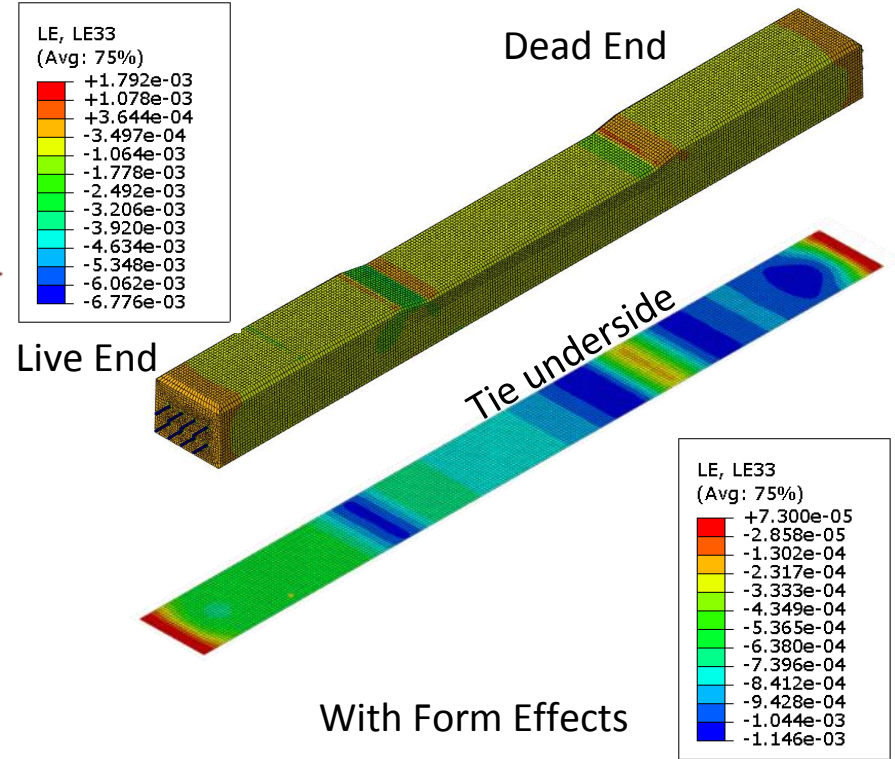
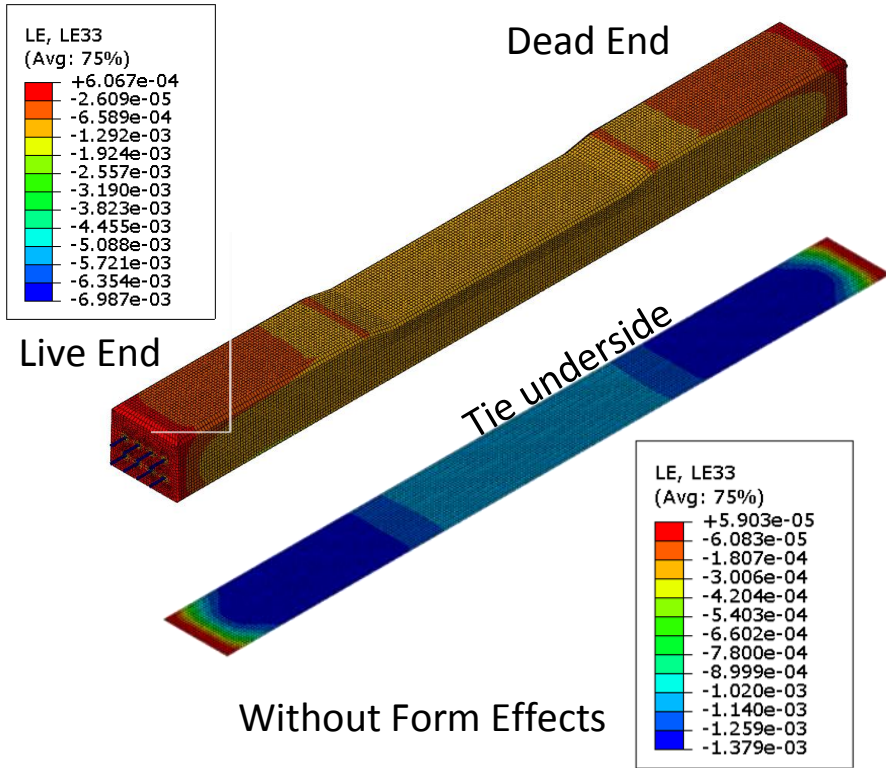
Live End

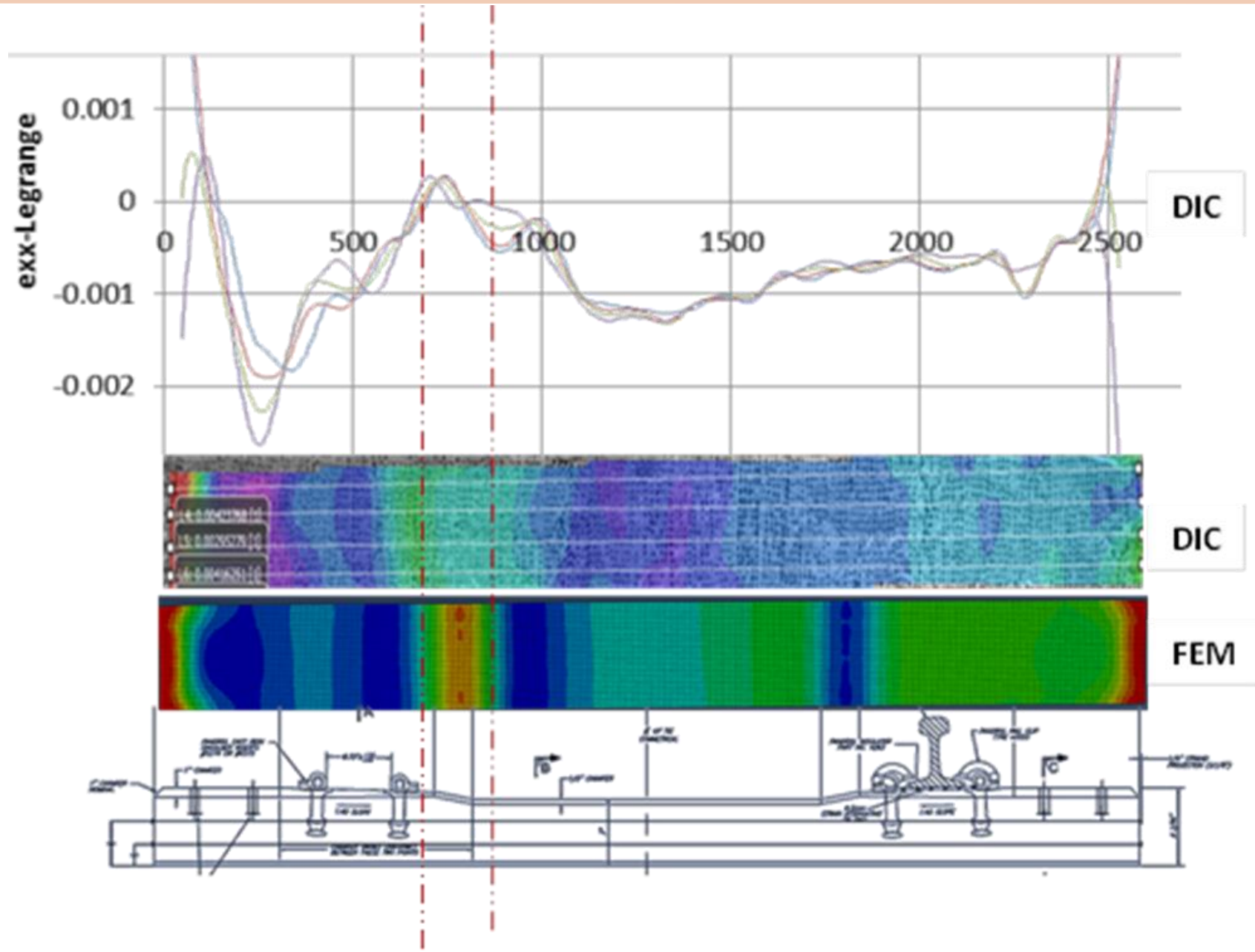
Dead End











Transfer Length	HSRM-HPC	Standard
Average	11.9 in	16.2 in
Std. Deviation	1.0 in	2.5 in
Coeff. Var.	8.4%	15.4%

- ❑ Historical Background
- ❑ Hypothesis
- ❑ Material Development and Characterization
- ❑ Prototype Tie Design and Fabrication
- ❑ **Product Qualification**
- ❑ Benefits
- ❑ Conclusions

4.9.1.1 Sequence of Design Tests (Tie “1”)

- a. Rail Seat Vertical Load Test - Rail seat A (4.9.1.4)
- b. Center Negative Bending Moment Test (4.9.1.6)
- c. Center Positive Bending Moment Test (4.9.1.7)
- d. Rail Seat Vertical Load Test – Rail seat B (4.9.1.4)
- e. Bond Development, Tendon Anchorage, and Ultimate Load Test – Rail seat A (4.9.1.8)
- f. Rail Seat Repeated Load Test – Rail seat B(4.9.1.5)

4.9.1.2 Sequence of Design Tests (Tie “2”)

- a. Fastening Insert Test (4.9.1.9)
- b. Fastening Uplift Test (4.9.1.10)
- c. Electrical Resistance and Impedance Test (4.9.1.14)

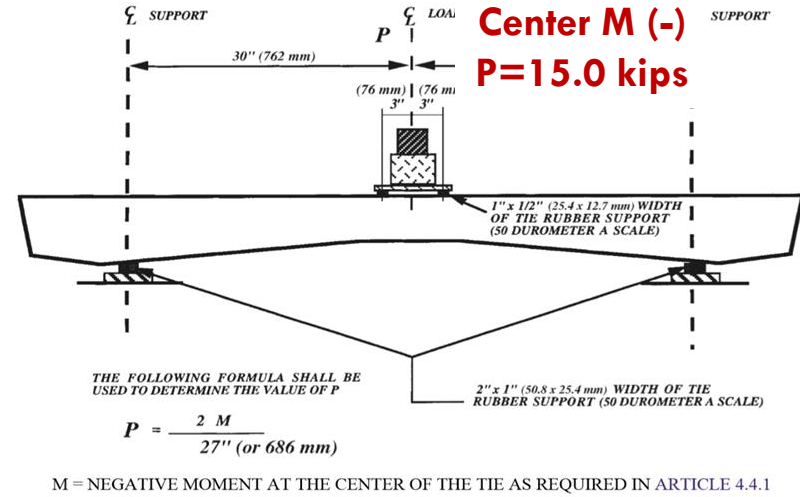
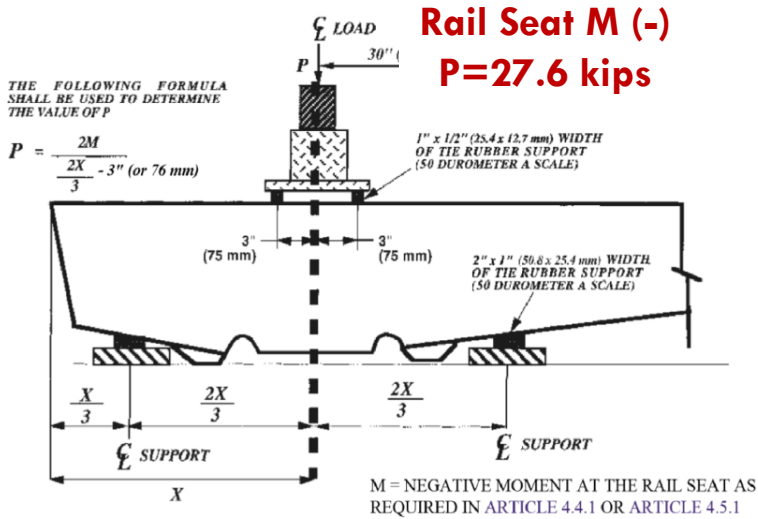


Figure 30-4-10. Tie Center Negative Moment Test

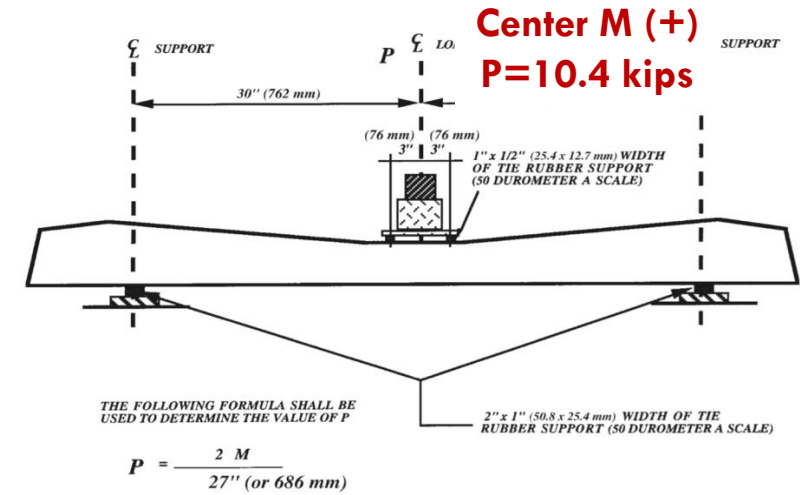
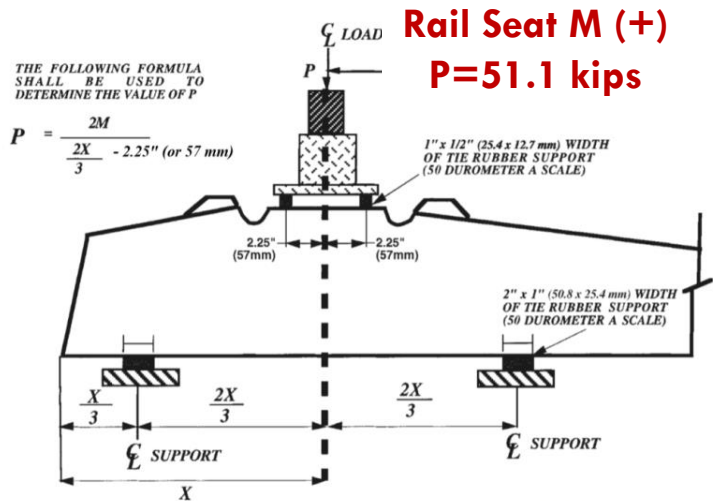
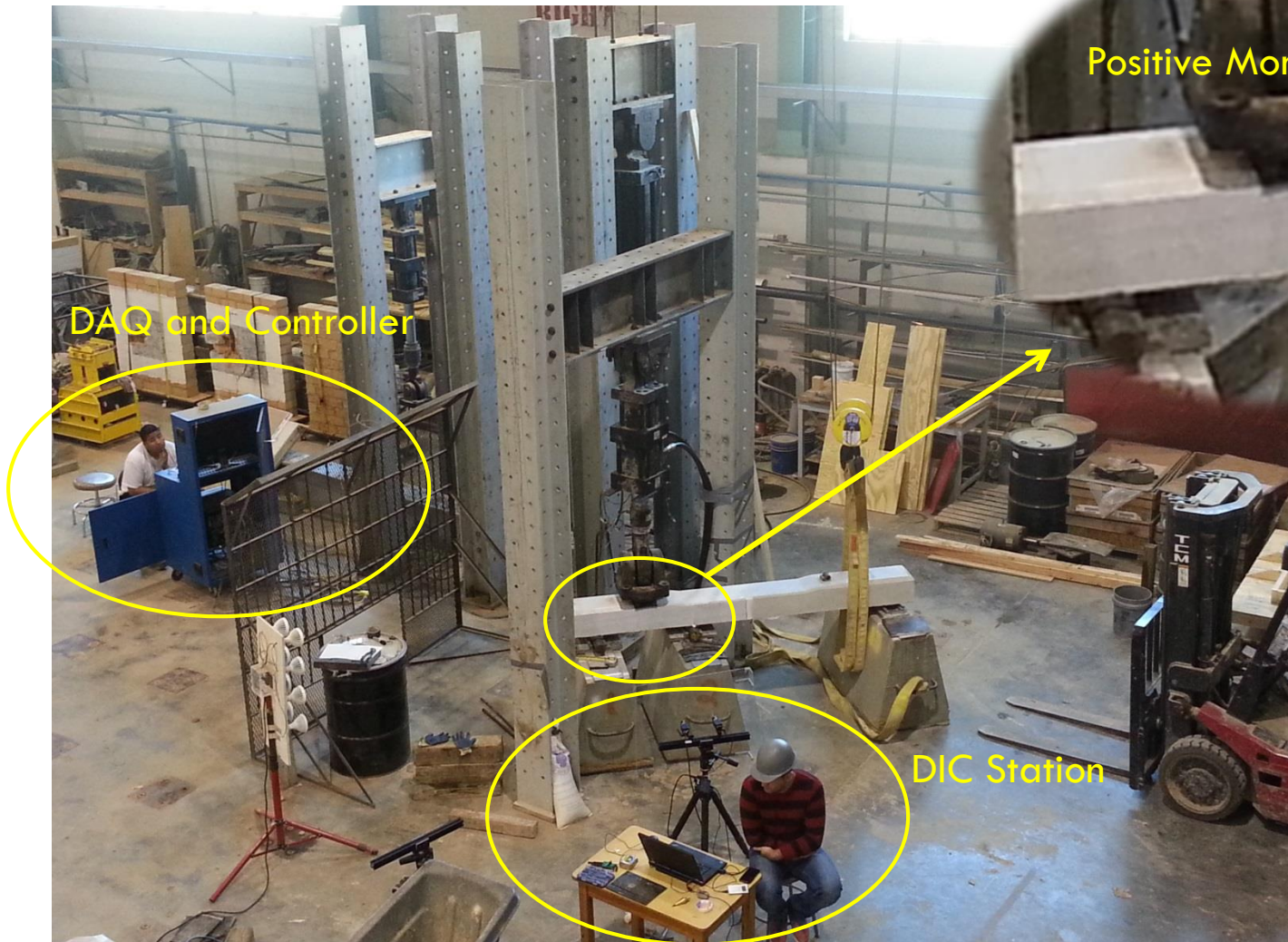


Figure 30-4-11. Tie Center Positive Moment Test

Figure 30-4-8. Rail Seat Positive Moment Test

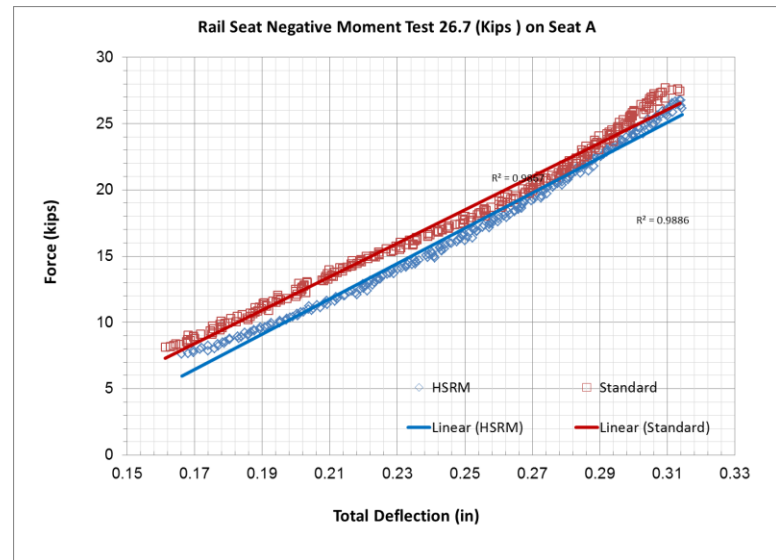


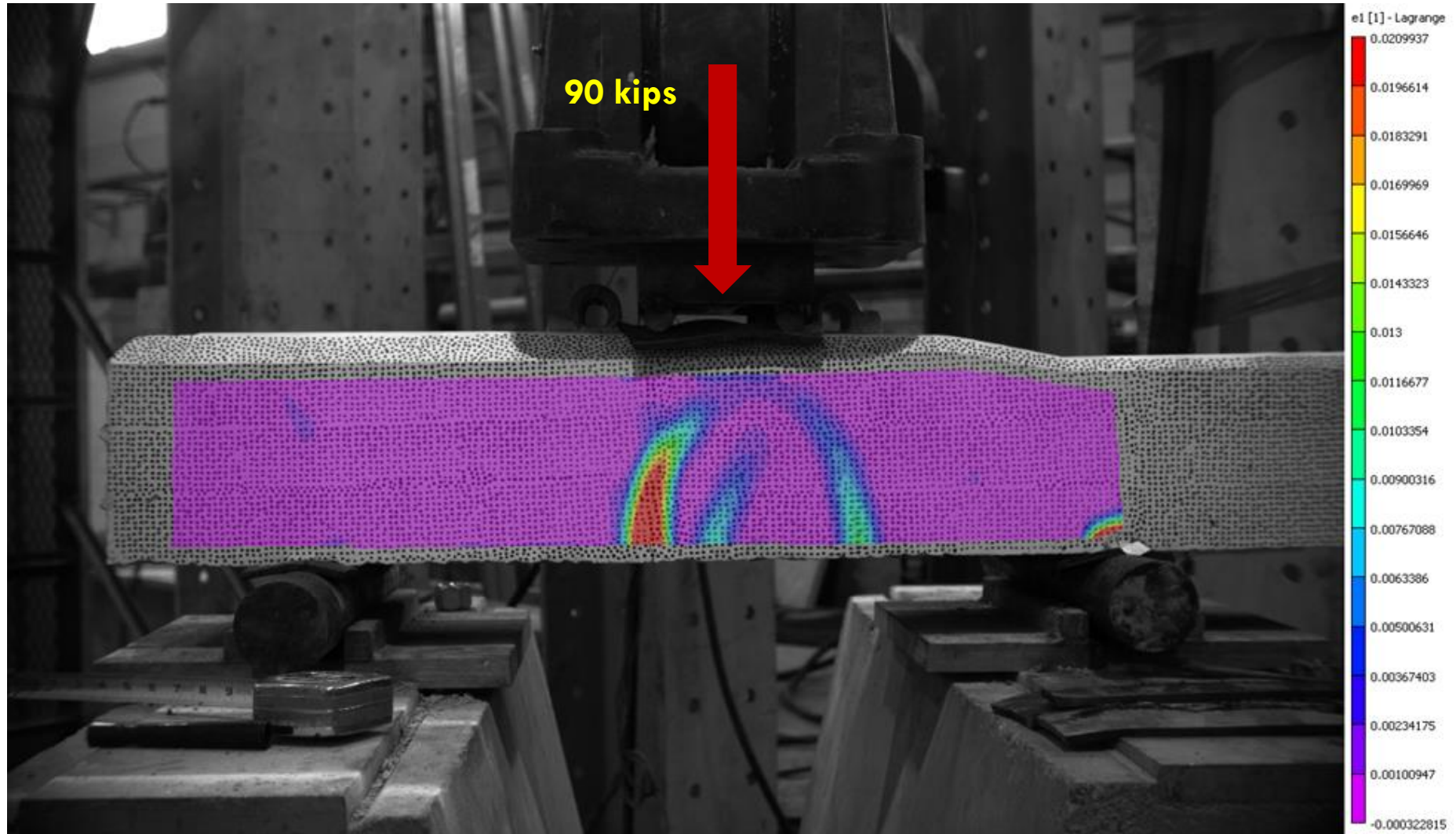


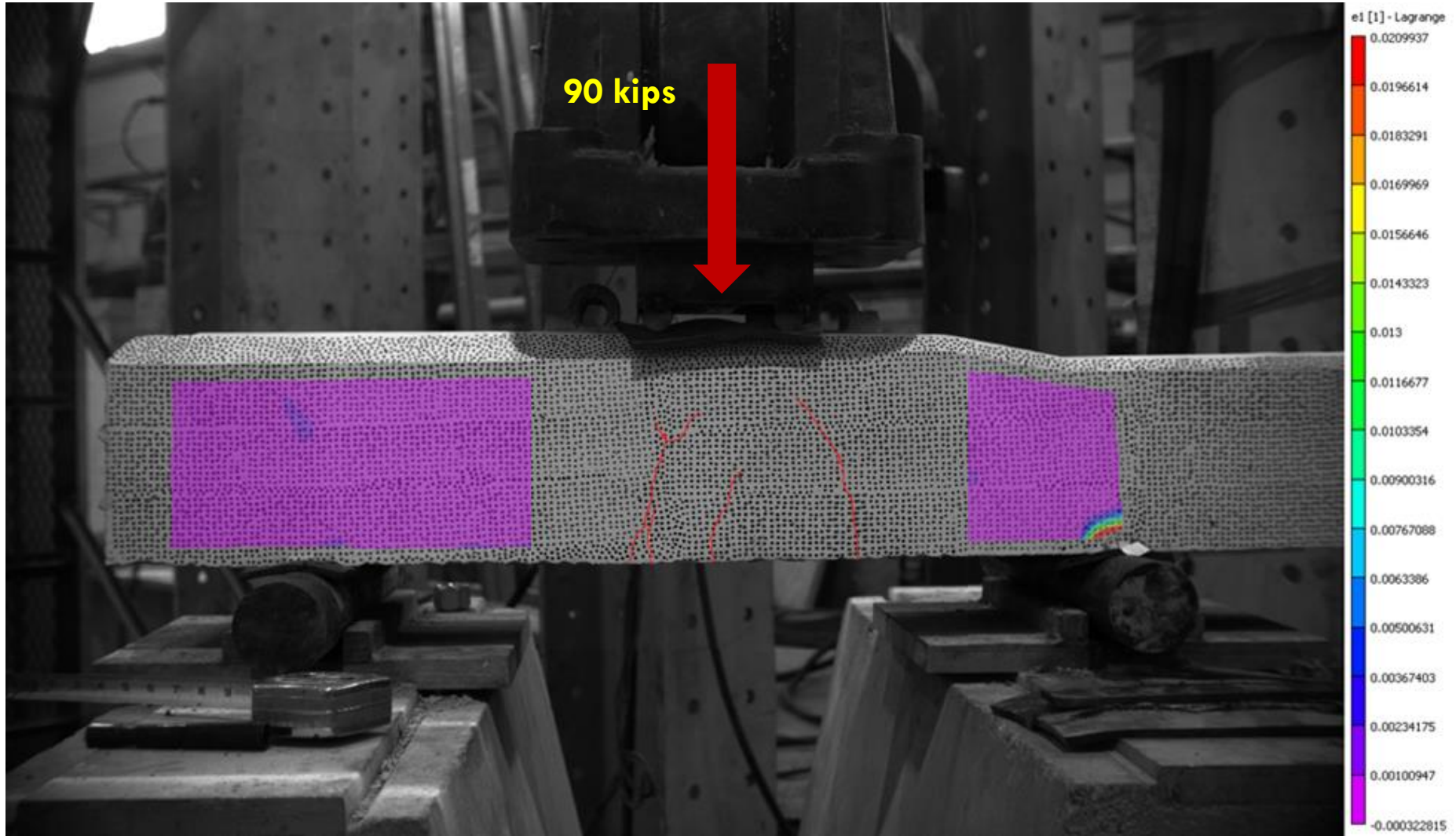
Positive Moment Railseat

DAQ and Controller

DIC Station



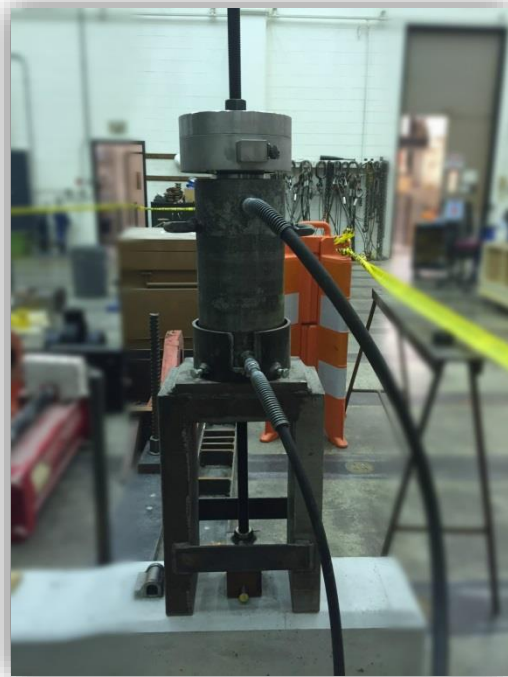




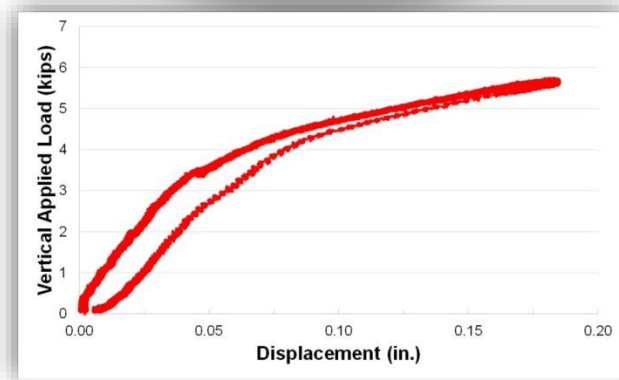
Tie ID		Rail Seat A		Rail Seat B		Center	
		M +	M -	M +	M -	M +	M -
Prototype	HSRM-Q1	Pass	Pass	Pass	Pass	Pass	Pass
	HSRM-Q2	Pass	Pass	Pass	Pass	Pass	Pass
	HSRM-Q3	Pass	Pass	Pass	Pass	Pass	Pass
	HSRM-Q4	Pass	Pass	Pass	Pass	Pass	Pass
	HSRM-Q5	Pass	Pass	Pass	Pass	Pass	Pass
Baseline	STANDARD-Q1	Pass	Pass	Pass	Pass	Pass	Pass
	STANDARD-Q2	Pass	Pass	Pass	Pass	Pass	Pass
	STANDARD-Q3 (9-1)	Pass	Pass	Pass	Pass	Pass	Pass
	STANDARD-Q4 (11-3)	Pass	Pass	Pass	Pass	Pass	Pass
	STANDARD-Q7	Pass*	Pass	Pass	Pass	Pass	Pass
Other	STANDARD-Q5-A	Pass*	Pass	Pass	Pass	Pass	Pass
	STANDARD-Q6-A	Pass	Pass	Pass	Pass	Pass	Pass

*Marginally

Tie ID		Rail Seat A					Strand Slippage
		$\epsilon_{\text{prestress}}$ (+/- 10%)	ϵ_{crack}	P_{crack}	1.5P	P_u	
Prototype	HSRM-Q1	~800 $\mu\epsilon$	~320 $\mu\epsilon$	56	Pass	>100	No
	HSRM-Q2						
	HSRM-Q3			57	Pass	>100	No
	HSRM-Q4						
	HSRM-Q5			52	Pass	96	No
Baseline	STND-Q1	~500 $\mu\epsilon$	~220 $\mu\epsilon$				
	STND-Q2						
	STND-Q3 (9-1)			57.9	Pass	88.9	No
	STND-Q4 (11-3)			52.1	Pass	105.3	No
	STND-Q7			49	Pass	97	No
Other	STND-Q5-A						
	STND-Q6-A						



Crosstie	Rail Seat	Location	Pull-out (12kips)	Torque (250lb-ft)
Rocla	A	Field	PASS	PASS
		Gauge	PASS	PASS
	B	Field	PASS	PASS
		Gauge	PASS	PASS
USC Prototype	A	Field	PASS	PASS
		Gauge	PASS	PASS
	B	Field	PASS	PASS
		Gauge	PASS	PASS



Crosstie	Rail Seat	Result
Standard Crosstie	A	PASS
	B	PASS
USC Prototype Crosstie	A	PASS
	B	PASS

Crosstie	Level of Distress	Load (kips)
Standard	Crack Initiation at	31.6
	Insert Pulled out	34.6
HSRM	Crack Initiation	33.2
	Insert Pulled out	35.1

Standard

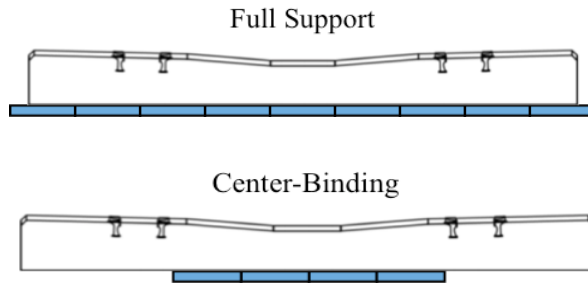


HSRM



- ❑ Historical Background
- ❑ Hypothesis
- ❑ Material Development and Characterization
- ❑ Prototype Tie Design and Fabrication
- ❑ Product Qualification
- ❑ **Benefits / Performance Assessment**
- ❑ Conclusions

Flexural Tests – Variable Support

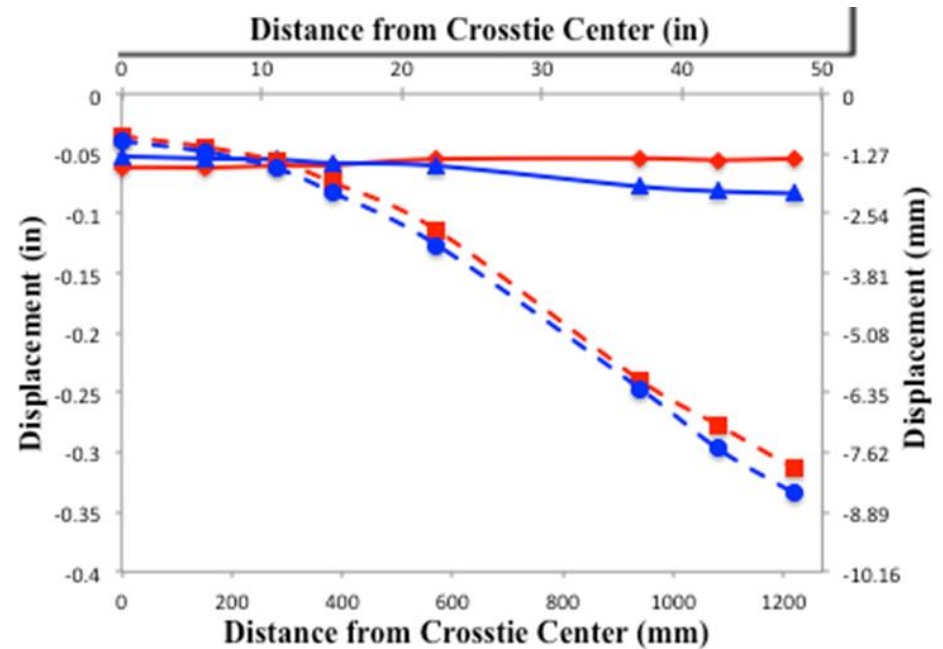
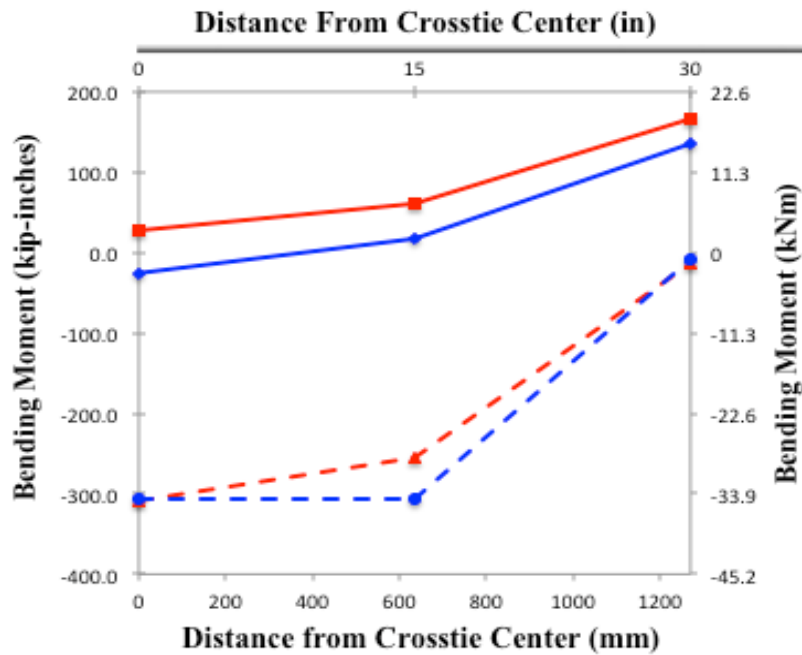


Standard- Full Support

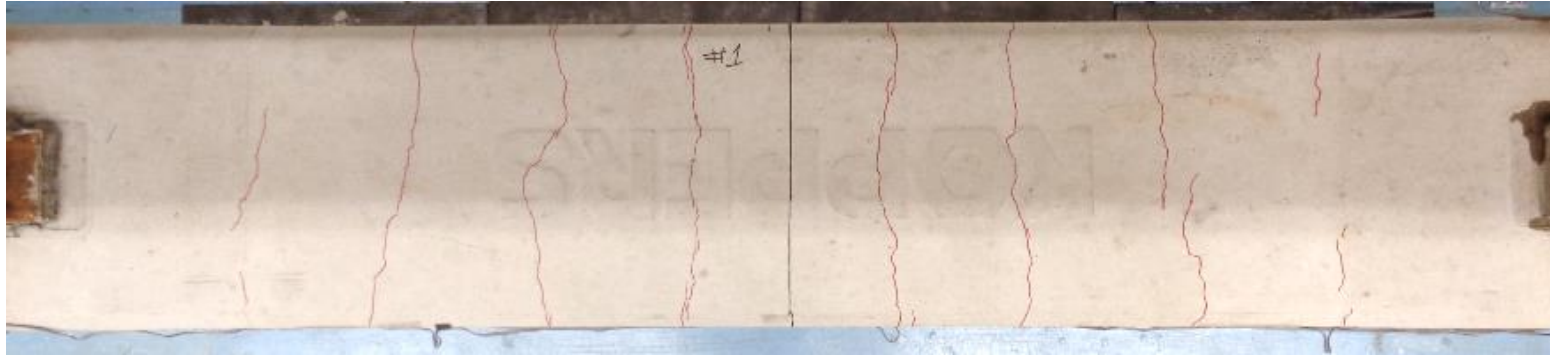
Standard- Center Bound

HSRM- Full Support

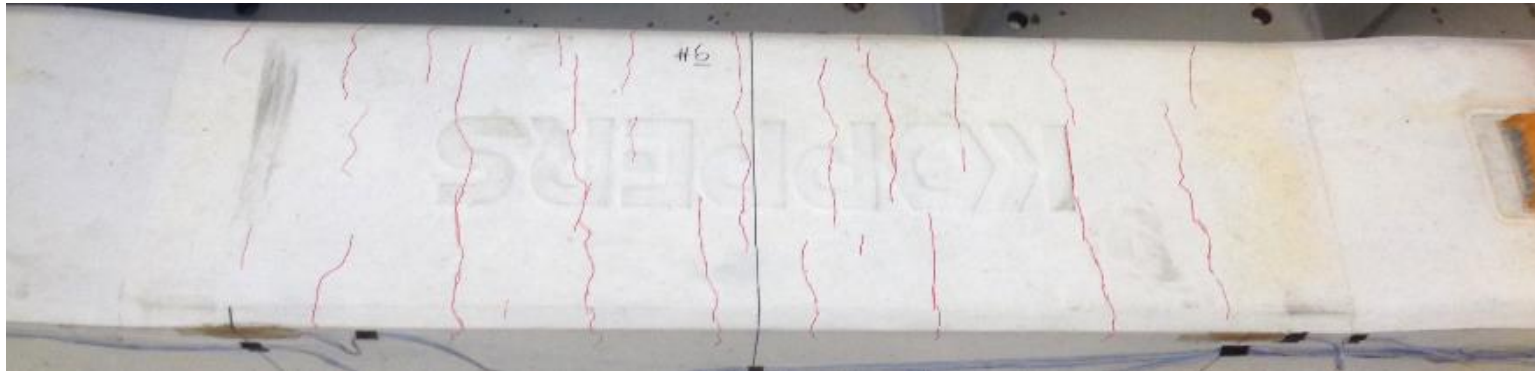
HSRM- Center Bound



Standard Tie

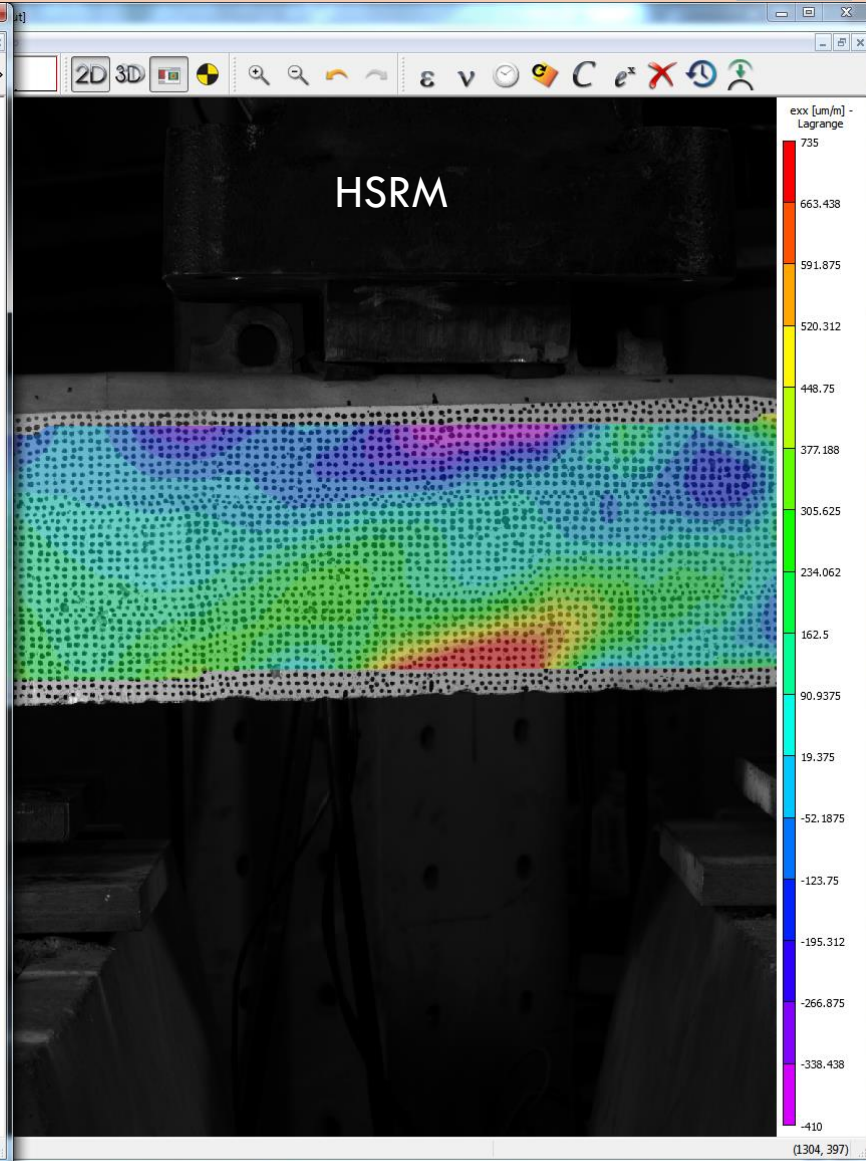
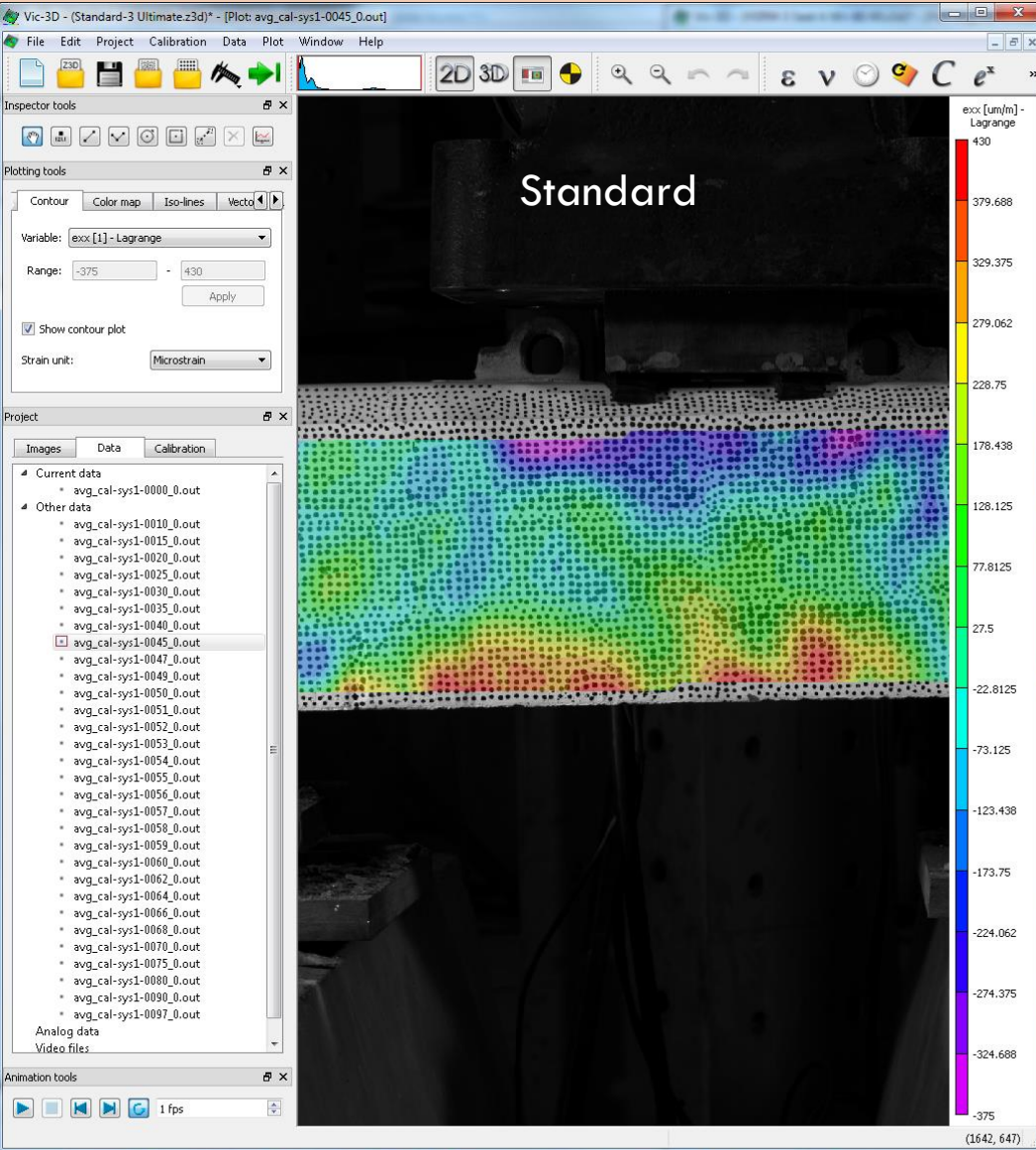


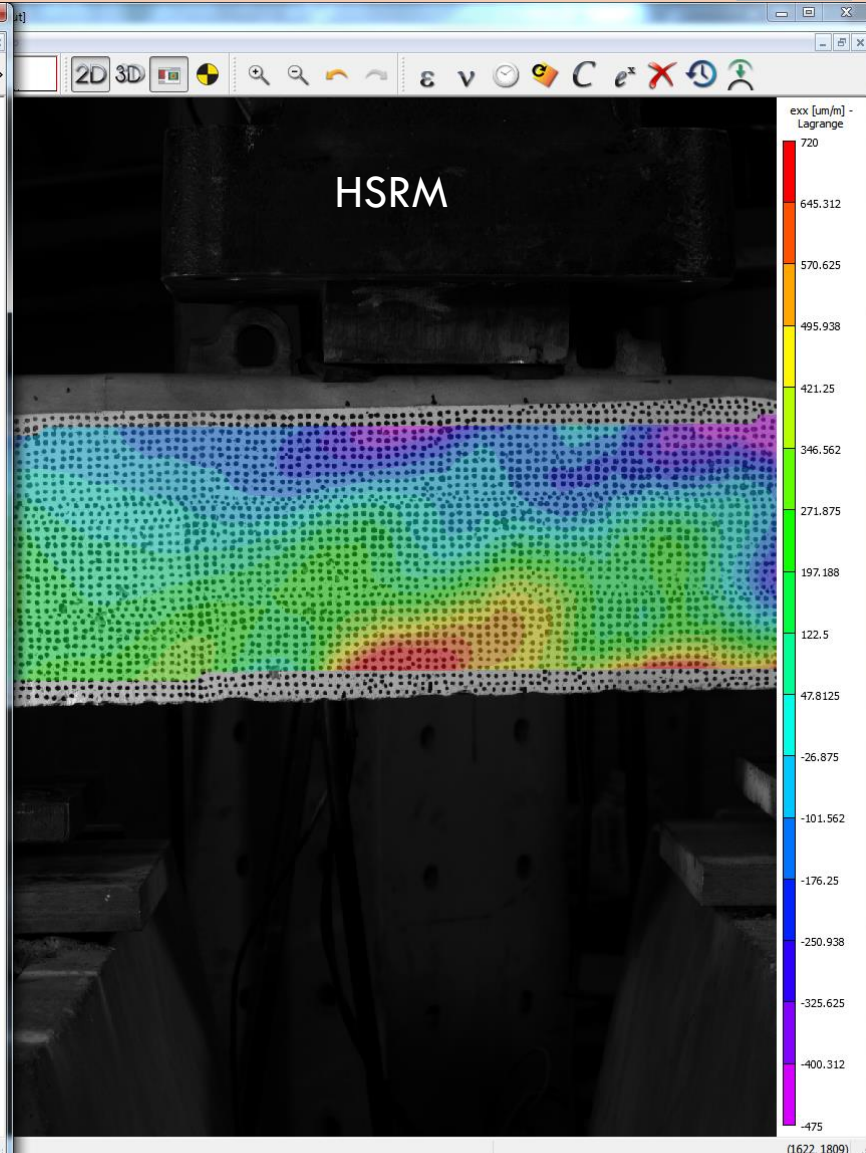
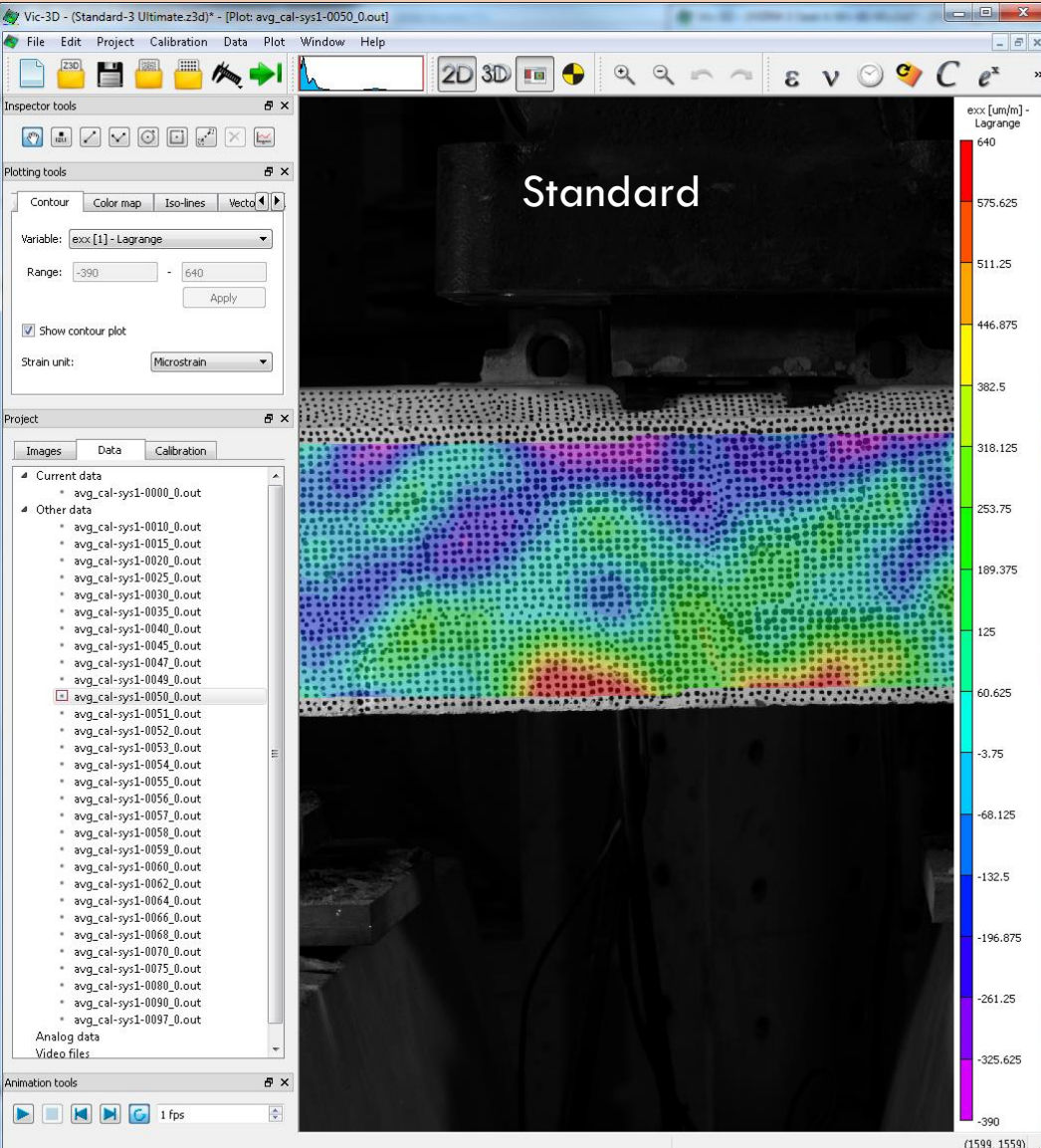
HSRM Tie

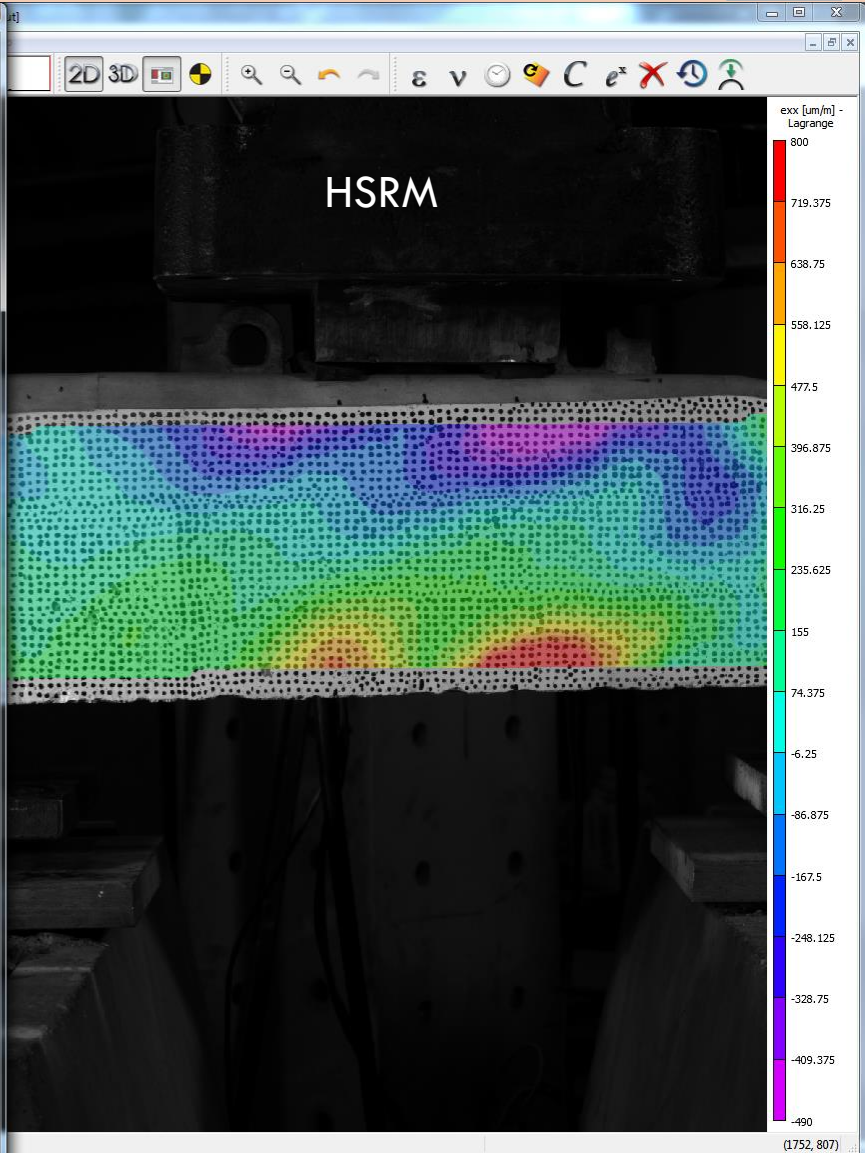
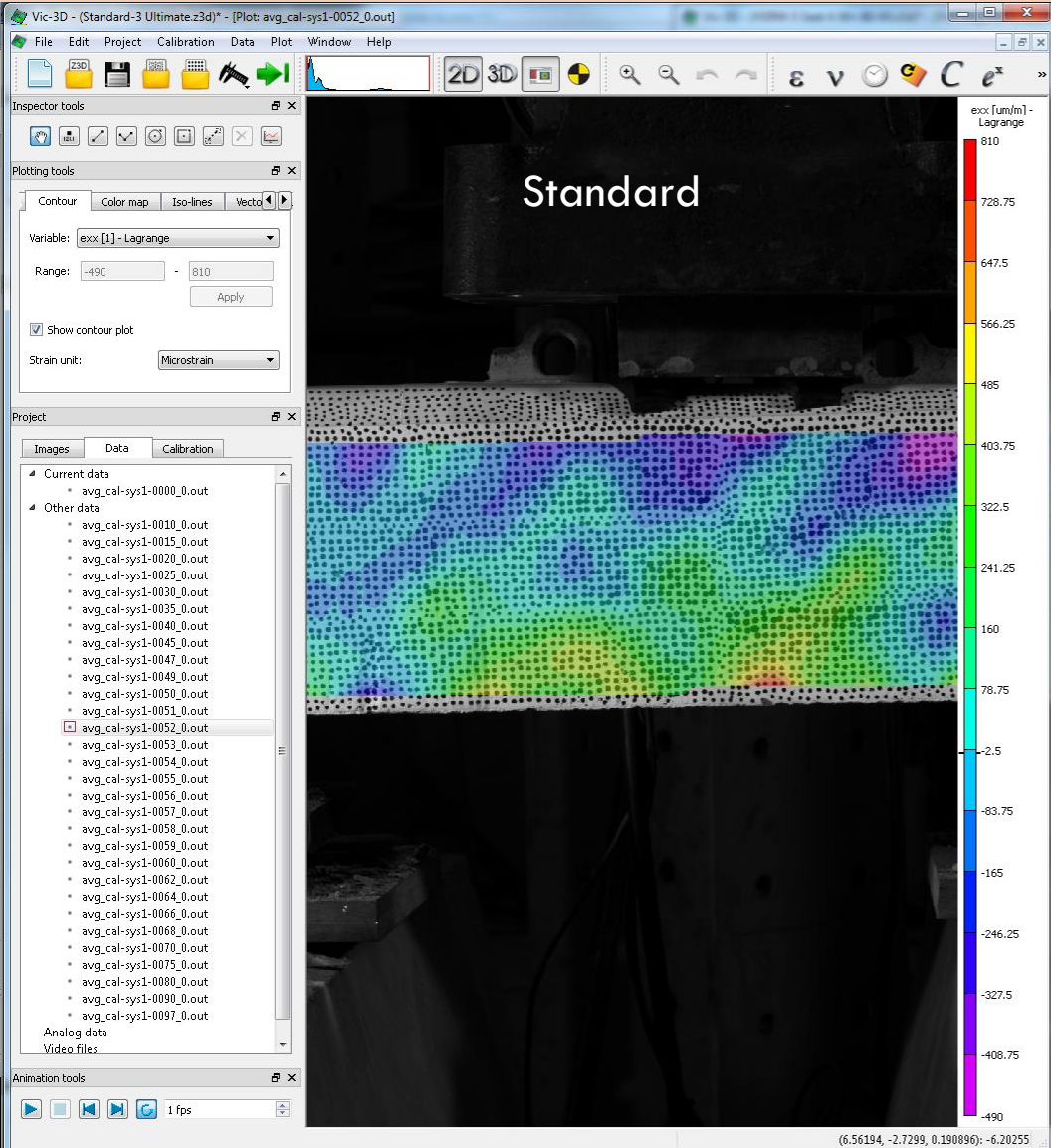


(center-binding conditions at 20 kips)	Standard		HSRM		CXT505S	
<i>End Displacement (in/mm)</i>	-0.314	-7.98	-0.334	-8.48	-0.234	-5.94
<i>Expected Gauge-Widening (in/mm)</i>	0.119	3.02	0.114	2.90	0.101	2.57
<i>Center Moment (kip-in/kNm)</i>	-309	-34.8	-306	-34.5	-413	-46.6

Rail Seat – Ultimate Positive

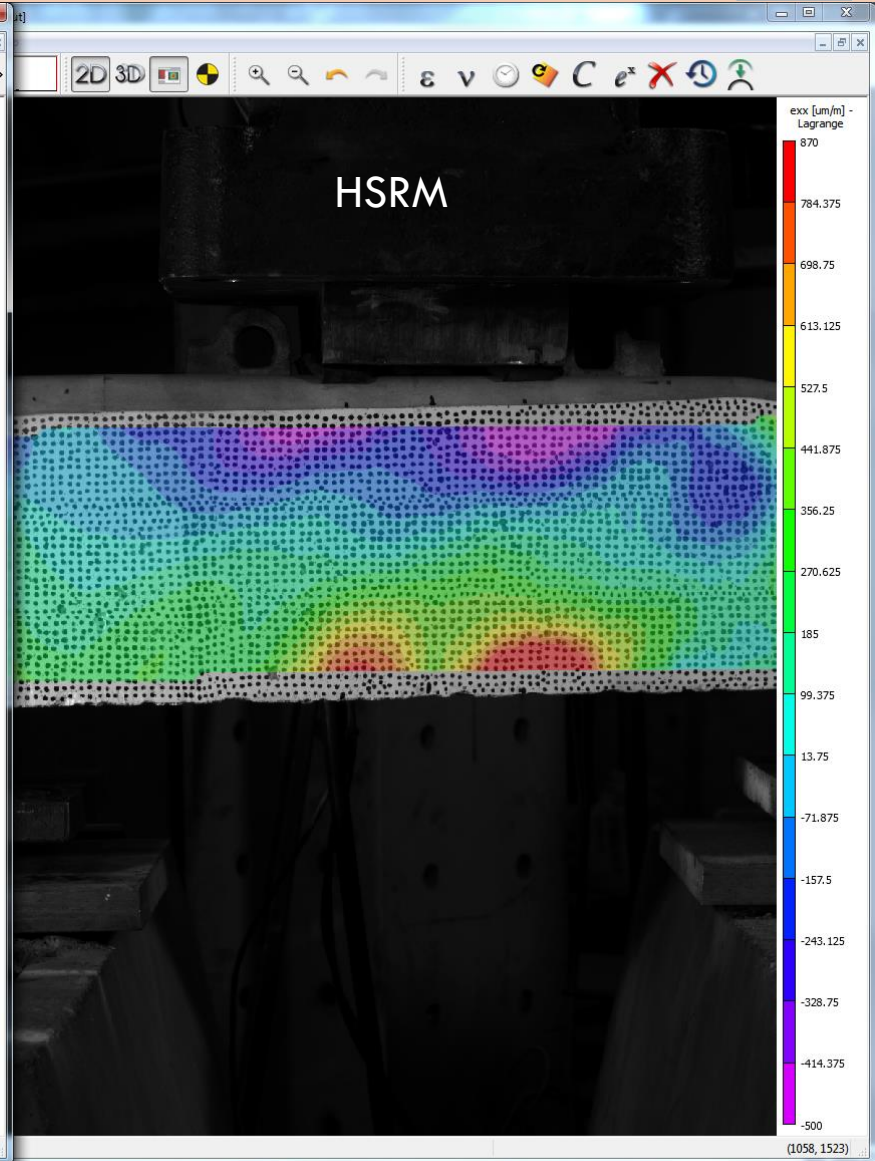
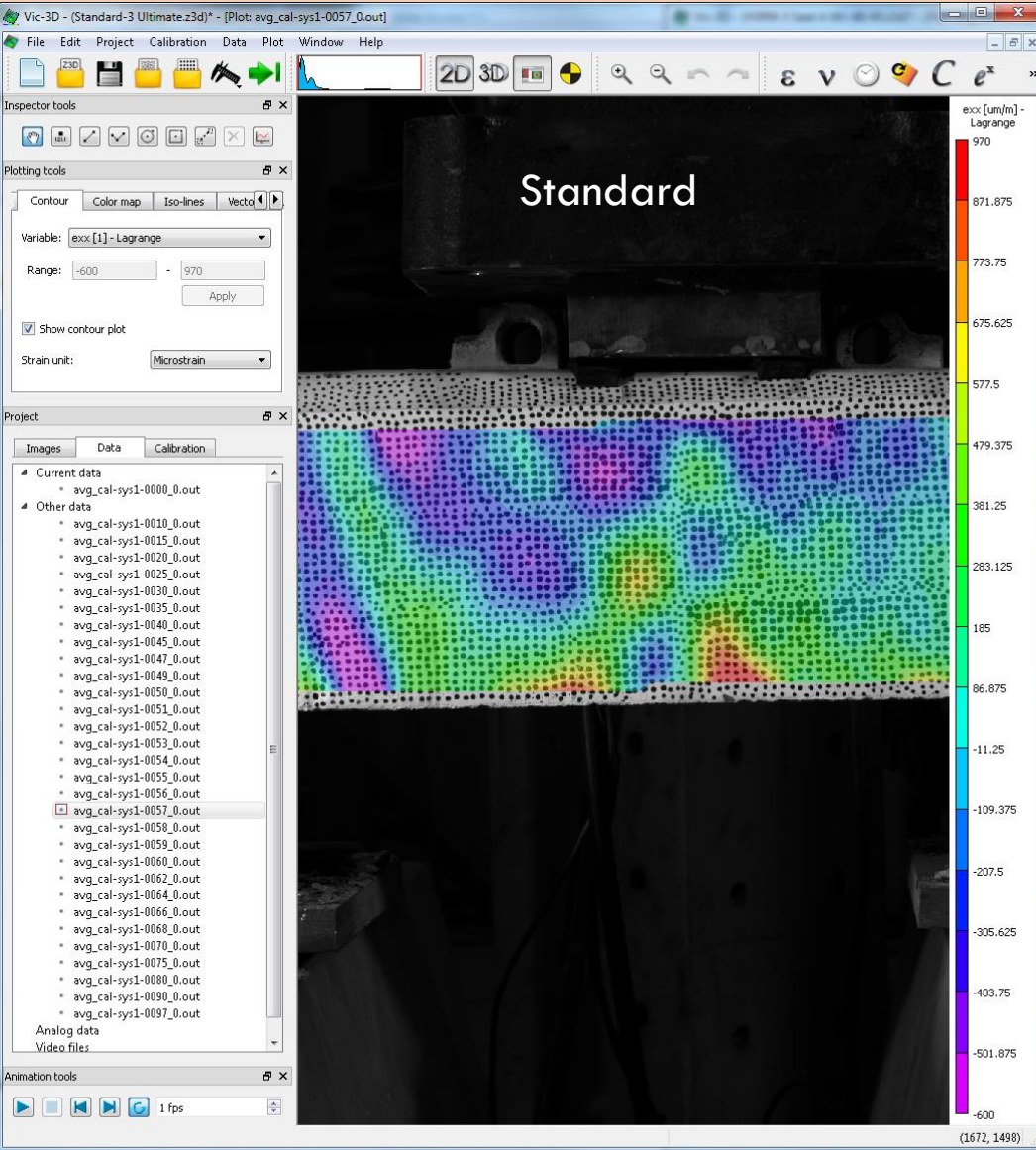








P=57 kips



Vic-3D - (Standard-3 Ultimate.z3d) - [Plot: avg_cal-sys1-0060_0.out]

File Edit Project Calibration Data Plot Window Help

Inspector tools

Plotting tools

Contour Color map Iso-lines Vectd

Variable: `exx[1] - Lagrange`

Range: `-660` - `1310`

Show contour plot

Strain unit: `Microstrain`

Project

Images Data Calibration

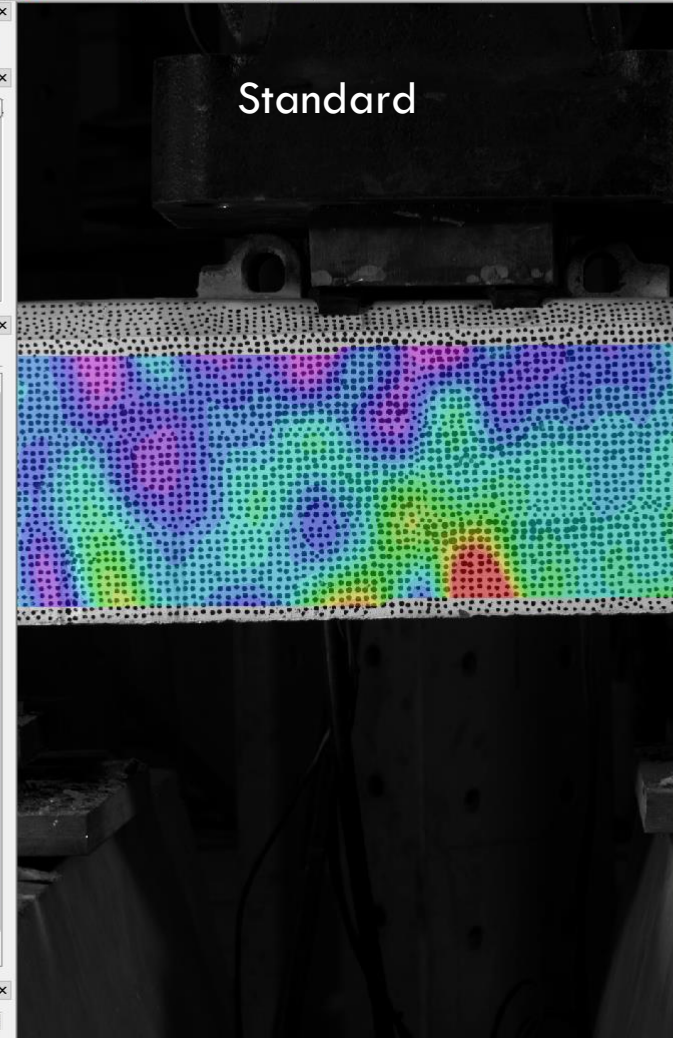
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 - avg_cal-sys1-0000_0.out
- Other data
 - avg_cal-sys1-0010_0.out
 - avg_cal-sys1-0015_0.out
 - avg_cal-sys1-0020_0.out
 - avg_cal-sys1-0025_0.out
 - avg_cal-sys1-0030_0.out
 - avg_cal-sys1-0035_0.out
 - avg_cal-sys1-0040_0.out
 - avg_cal-sys1-0045_0.out
 - avg_cal-sys1-0047_0.out
 - avg_cal-sys1-0049_0.out
 - avg_cal-sys1-0050_0.out
 - avg_cal-sys1-0051_0.out
 - avg_cal-sys1-0052_0.out
 - avg_cal-sys1-0053_0.out
 - avg_cal-sys1-0054_0.out
 - avg_cal-sys1-0055_0.out
 - avg_cal-sys1-0056_0.out
 - avg_cal-sys1-0057_0.out
 - avg_cal-sys1-0058_0.out
 - avg_cal-sys1-0059_0.out
 - avg_cal-sys1-0060_0.out**
 - avg_cal-sys1-0062_0.out
 - avg_cal-sys1-0064_0.out
 - avg_cal-sys1-0066_0.out
 - avg_cal-sys1-0068_0.out
 - avg_cal-sys1-0070_0.out
 - avg_cal-sys1-0075_0.out
 - avg_cal-sys1-0080_0.out
 - avg_cal-sys1-0090_0.out
 - avg_cal-sys1-0097_0.out

Analog data

Video files

Animation tools

1 fps



Standard

exx [$\mu\text{m}/\text{m}$] - Lagrange

1310

1186.88

1063.75

940.625

817.5

694.375

571.25

448.125

325

201.875

78.75

-44.375

-167.5

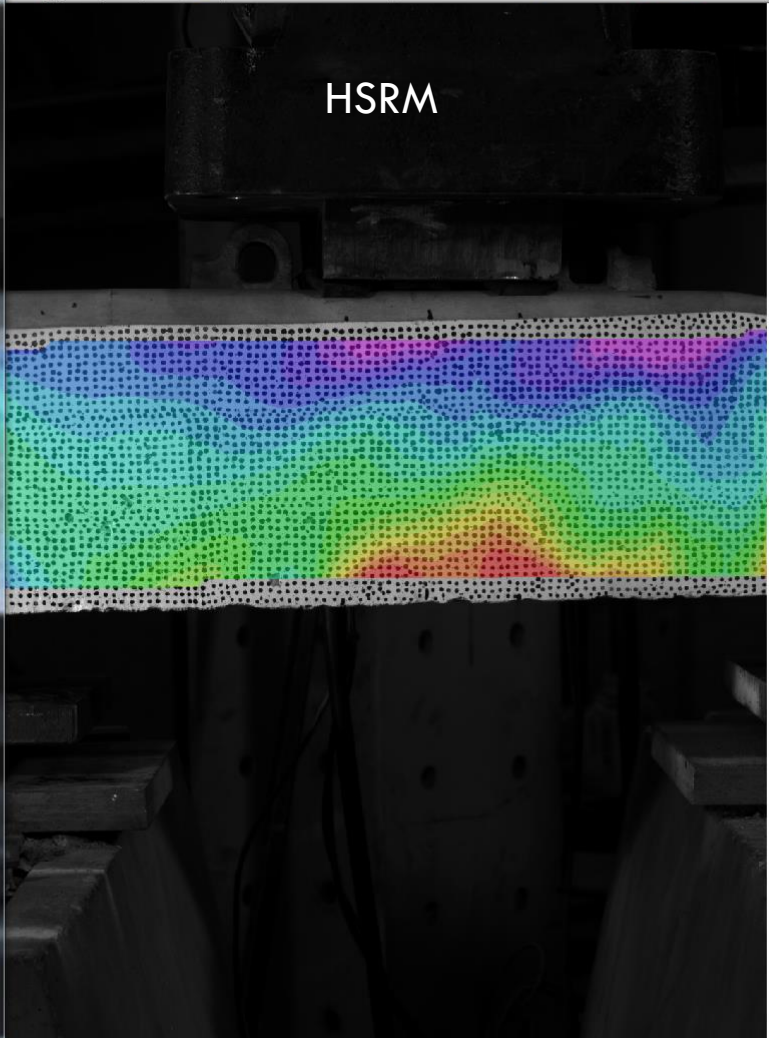
-290.625

-413.75

-536.875

-660

(756, 1395)



HSRM

exx [$\mu\text{m}/\text{m}$] - Lagrange

950

858.75

767.5

676.25

585

493.75

402.5

311.25

220

128.75

37.5

-53.75

-145

-236.25

-327.5

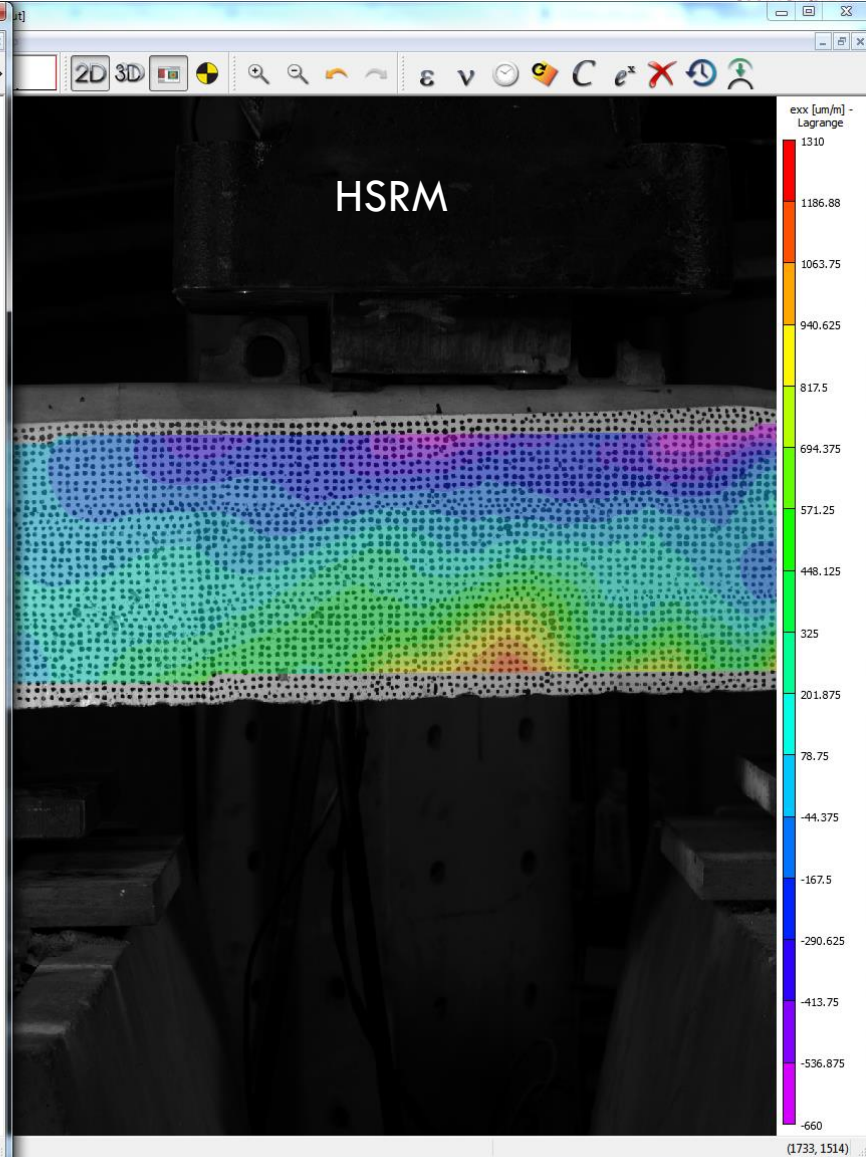
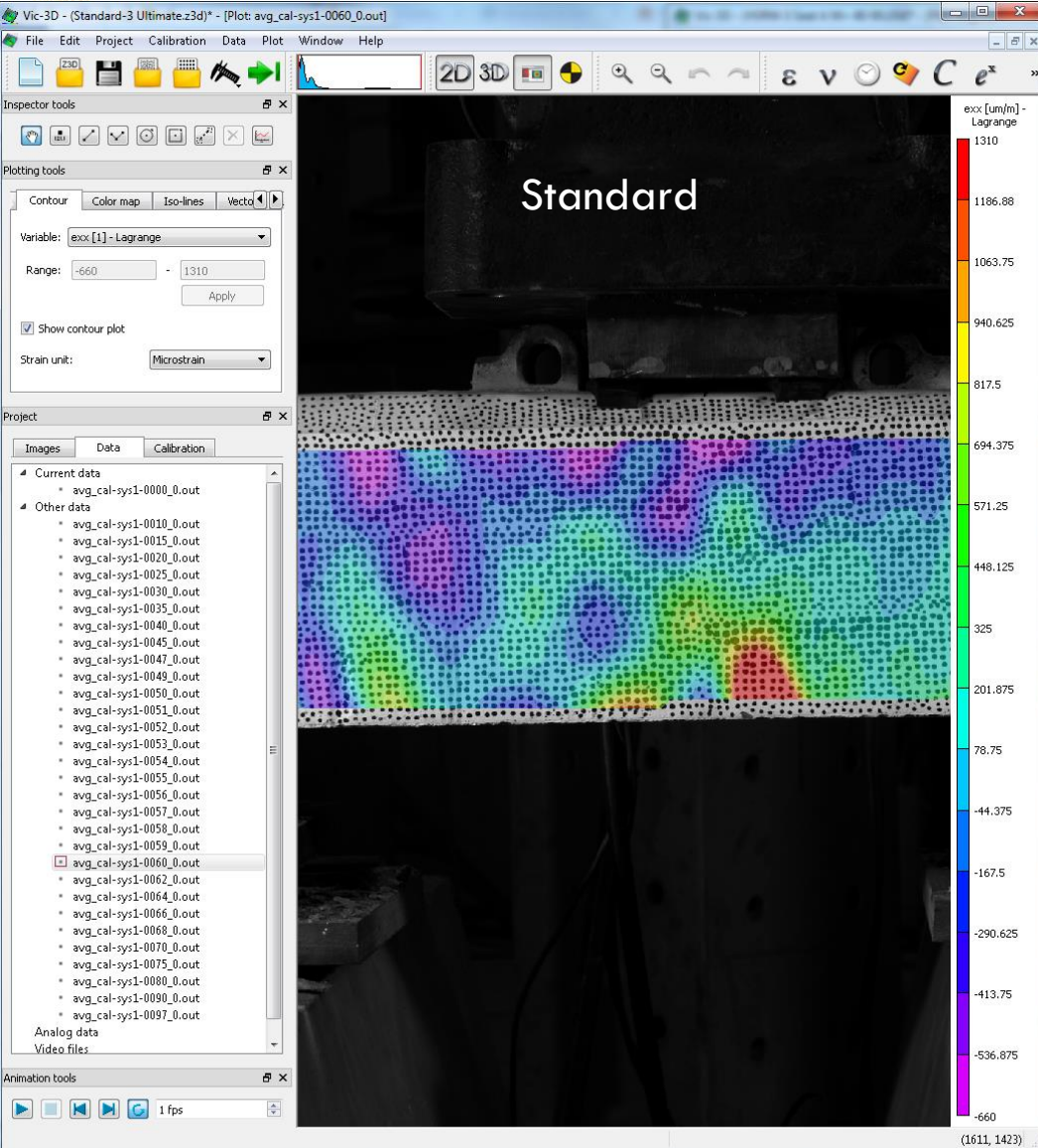
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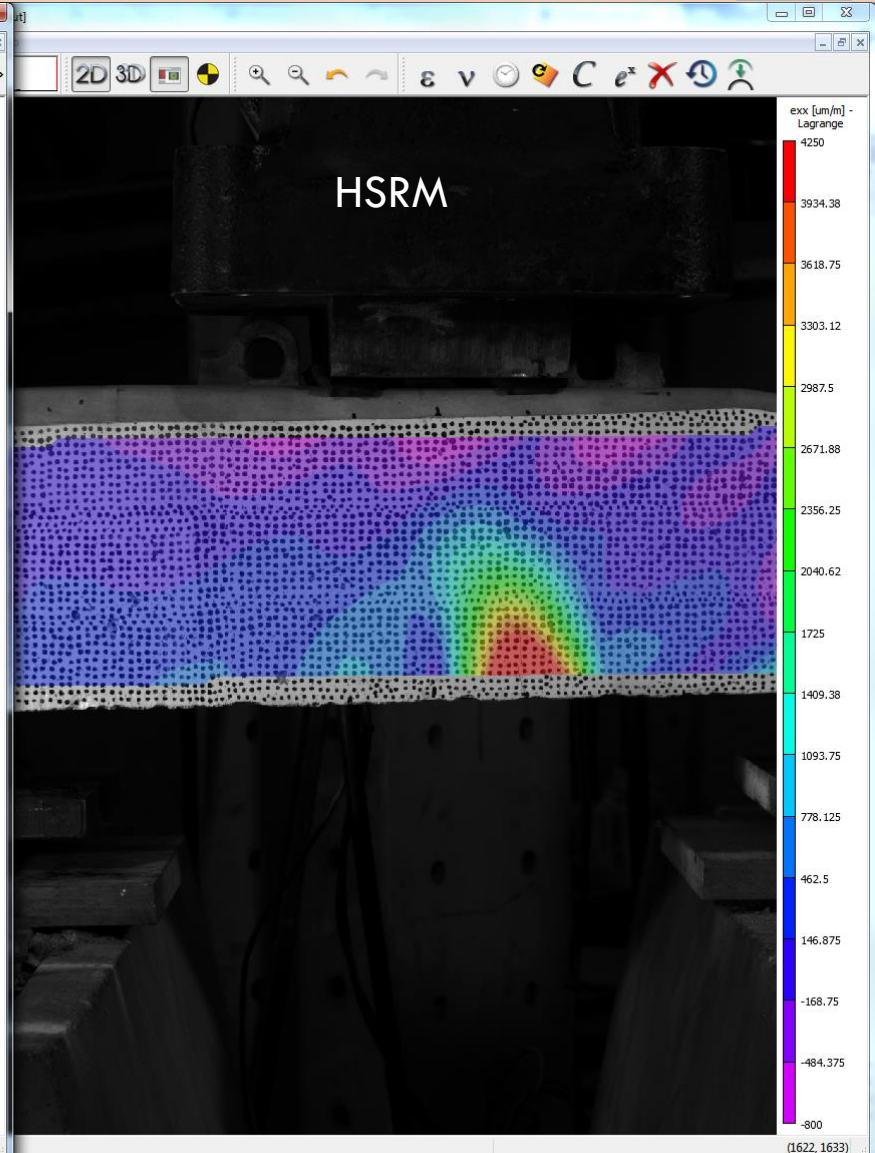
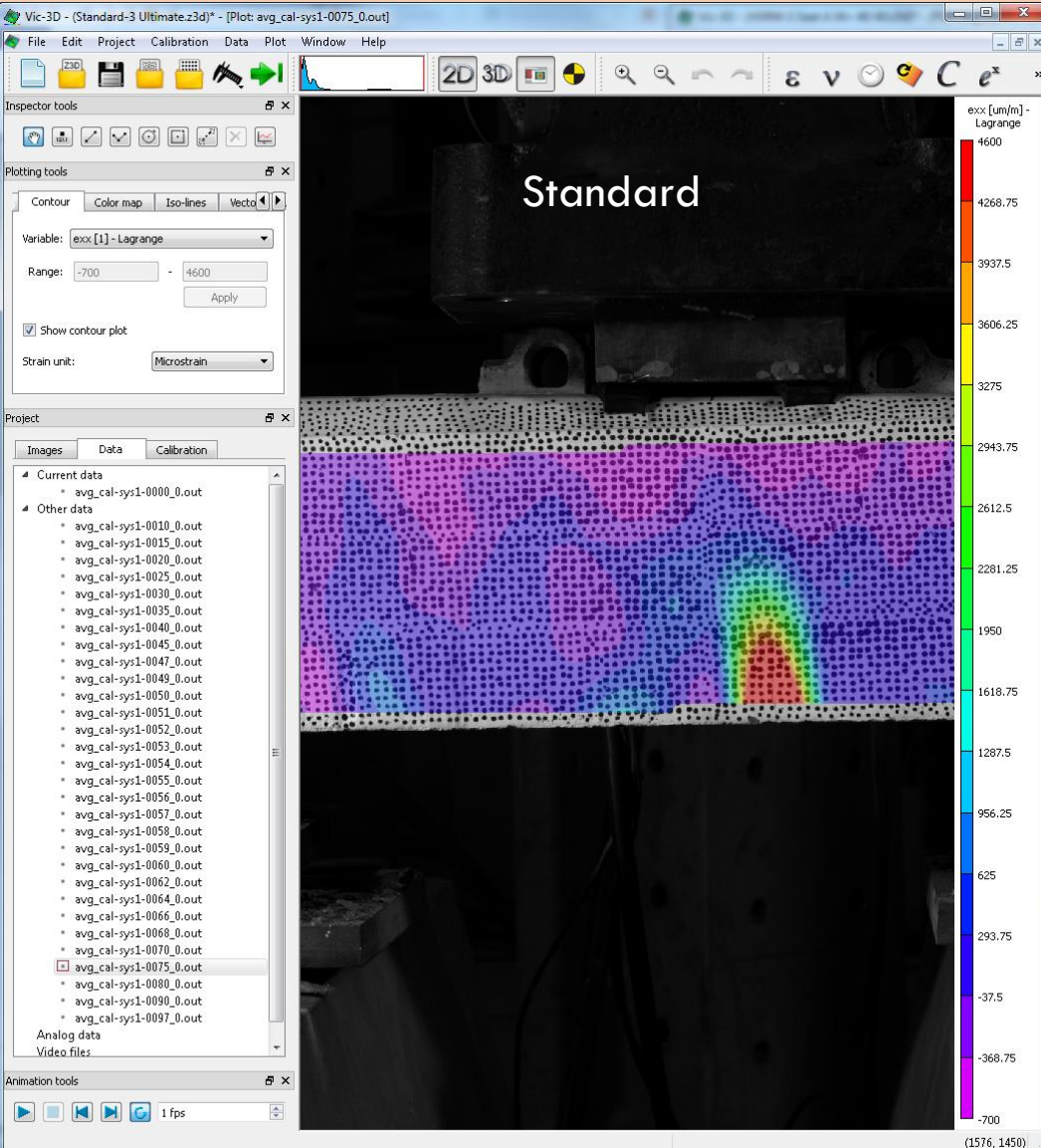
-510

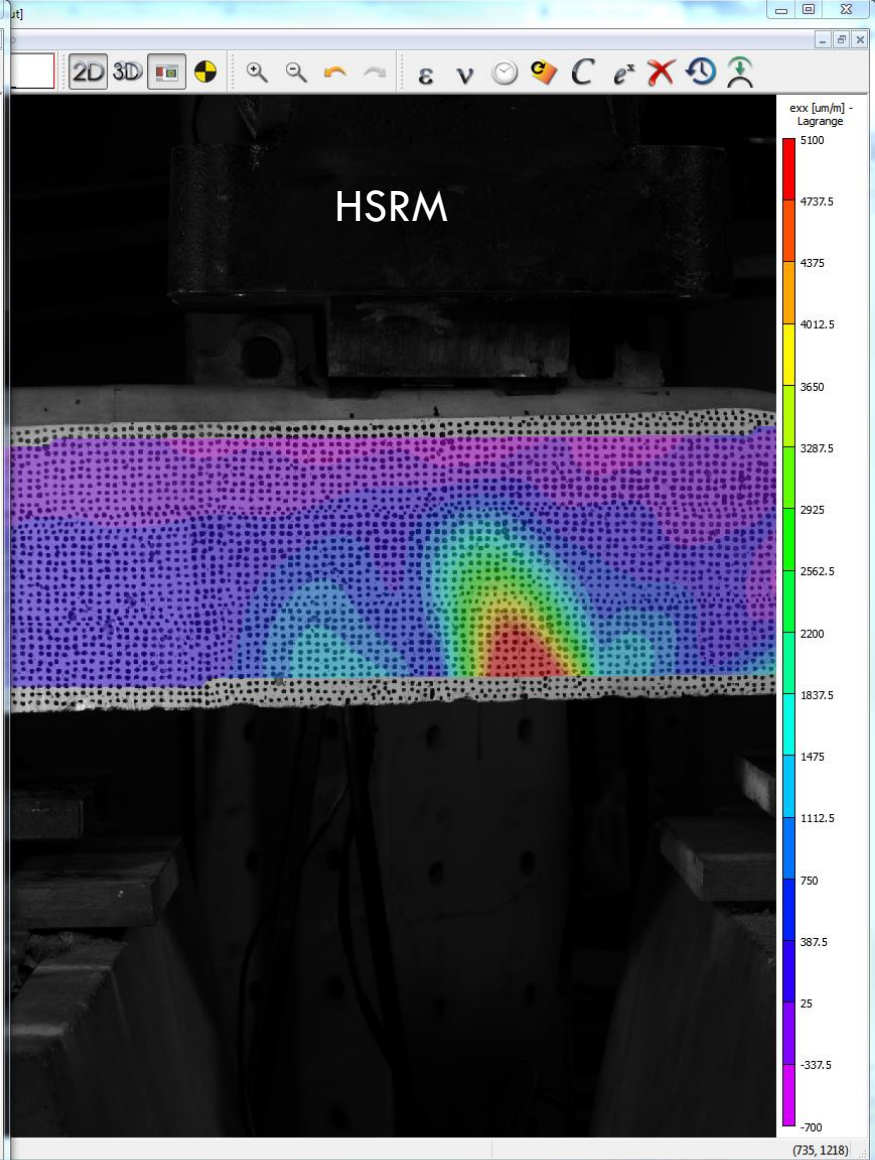
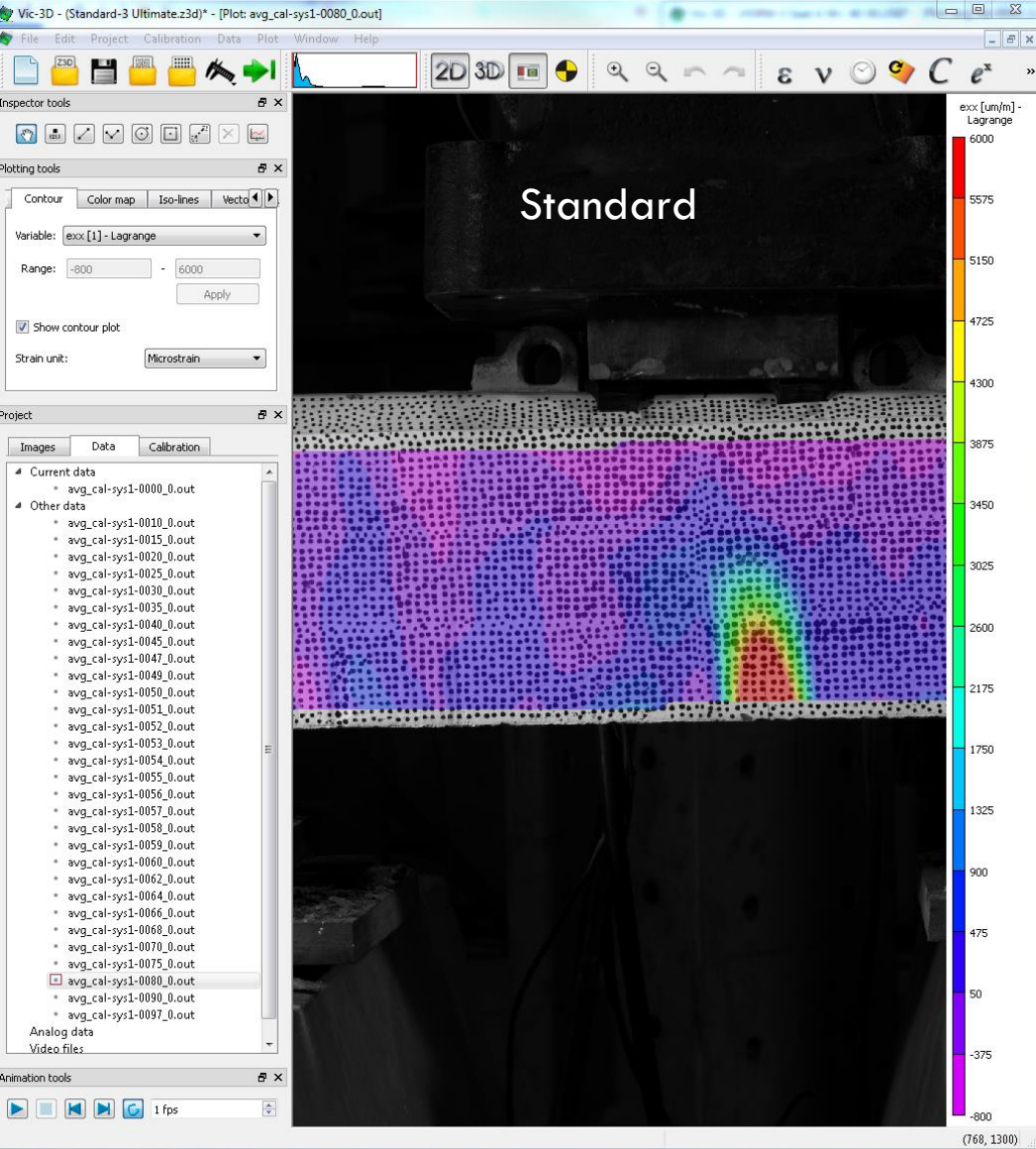
(684, 1402)

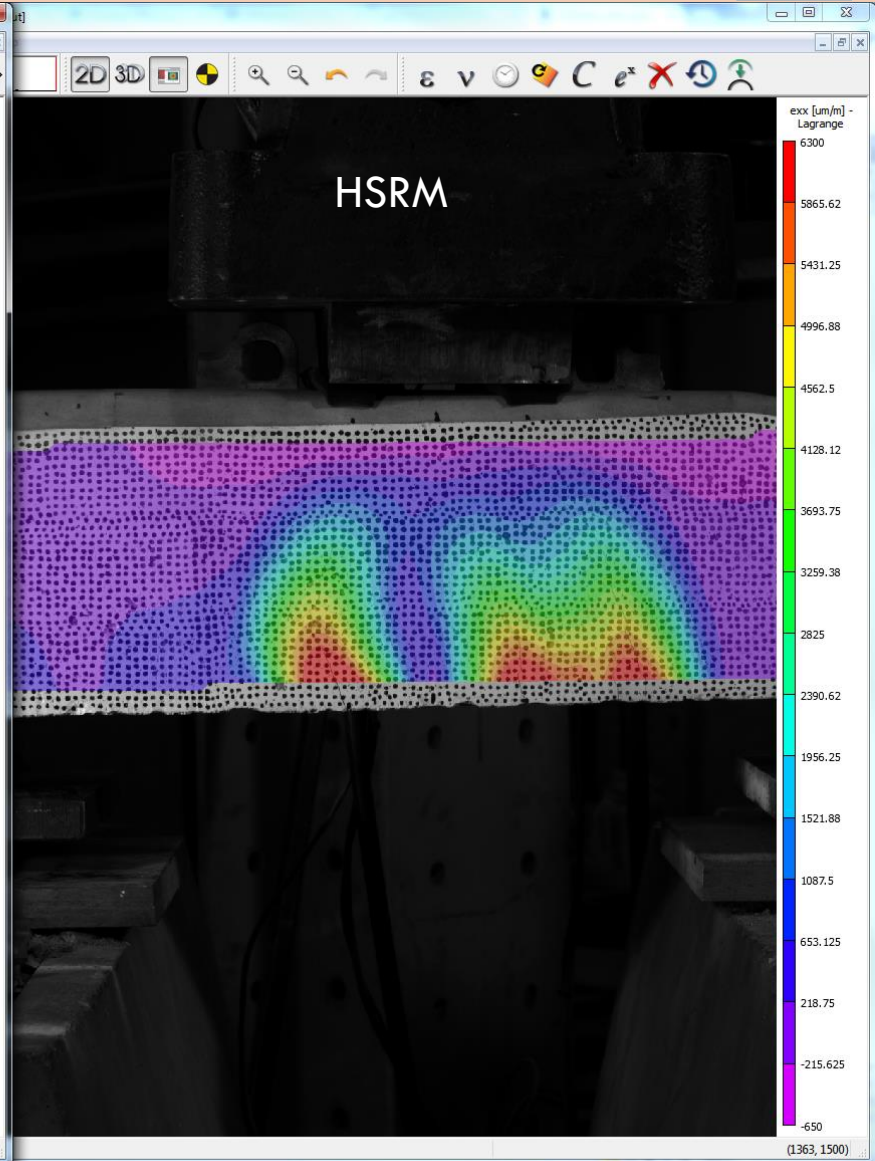
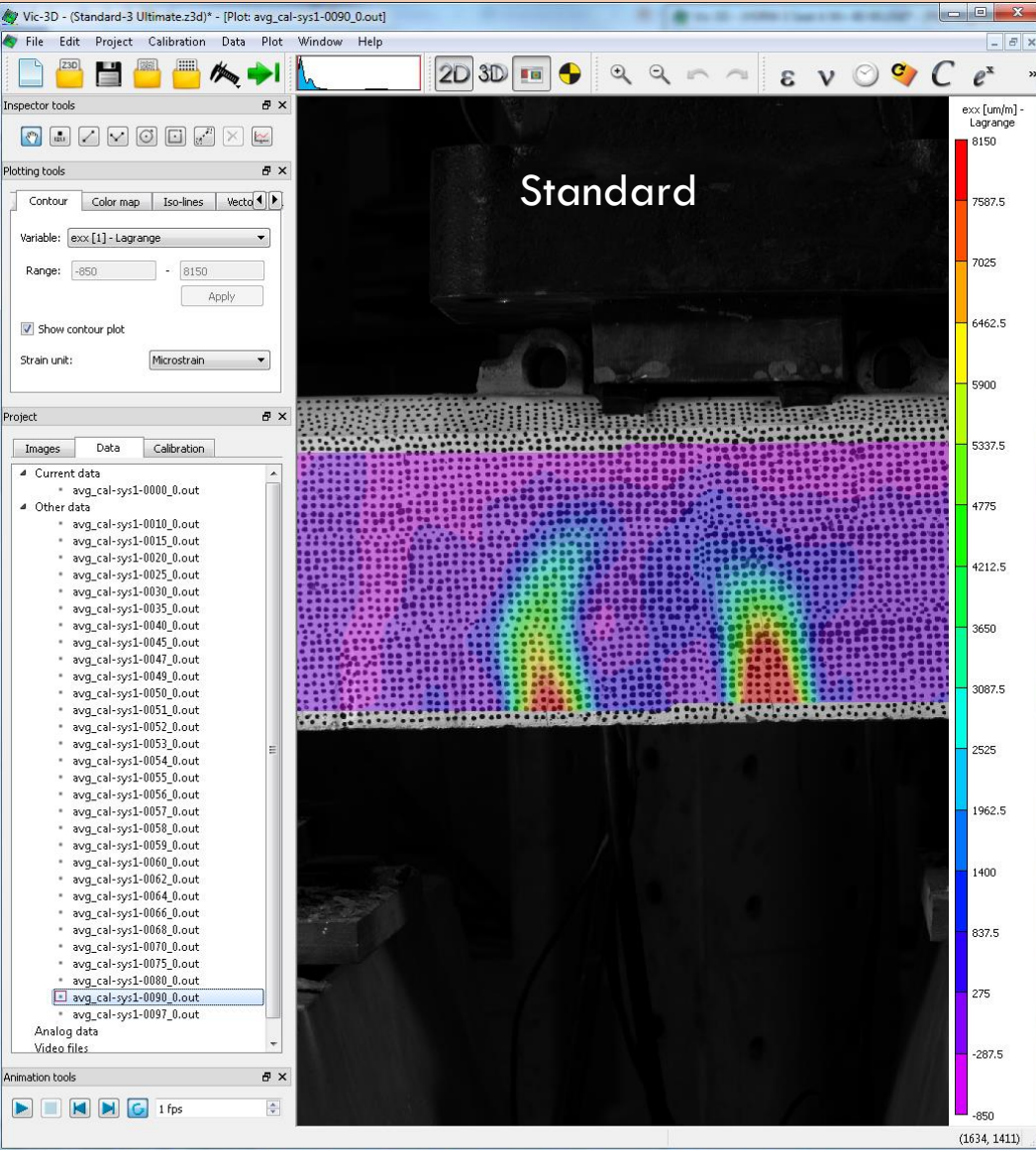


P=60 kips Same Scale



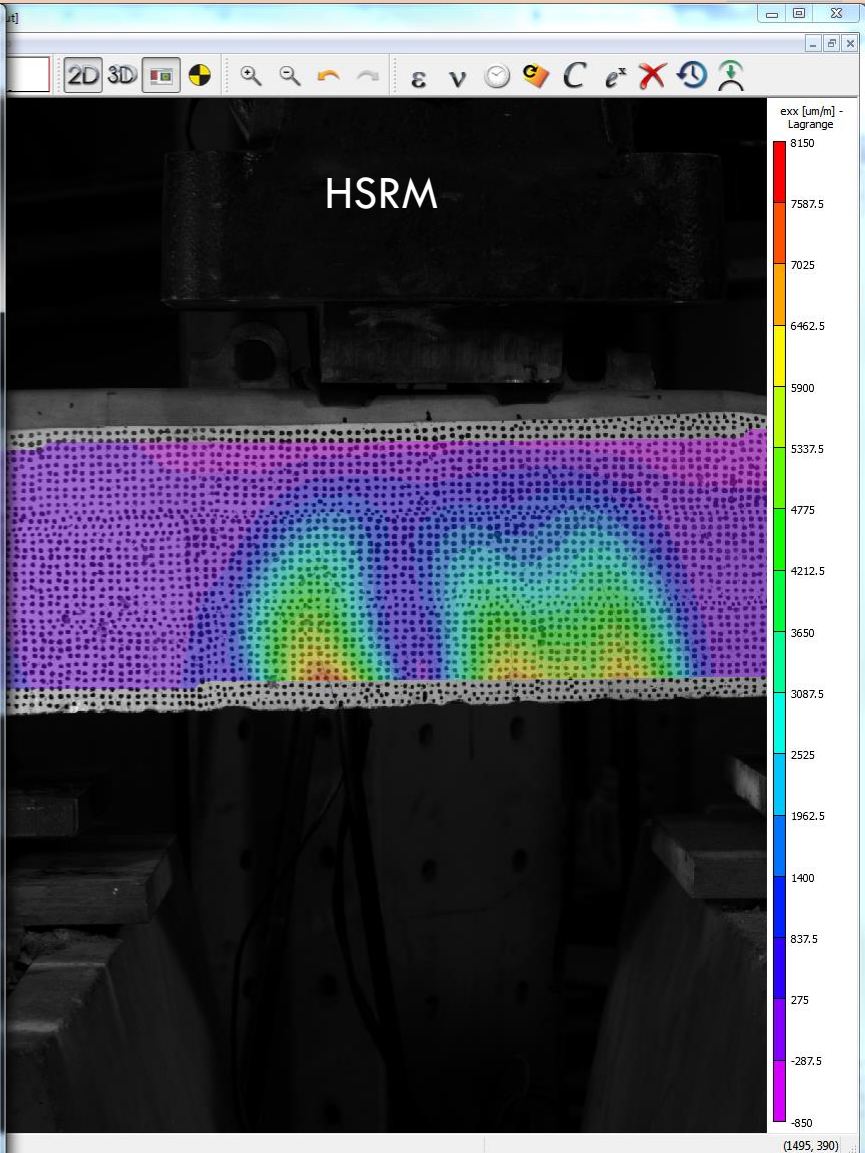
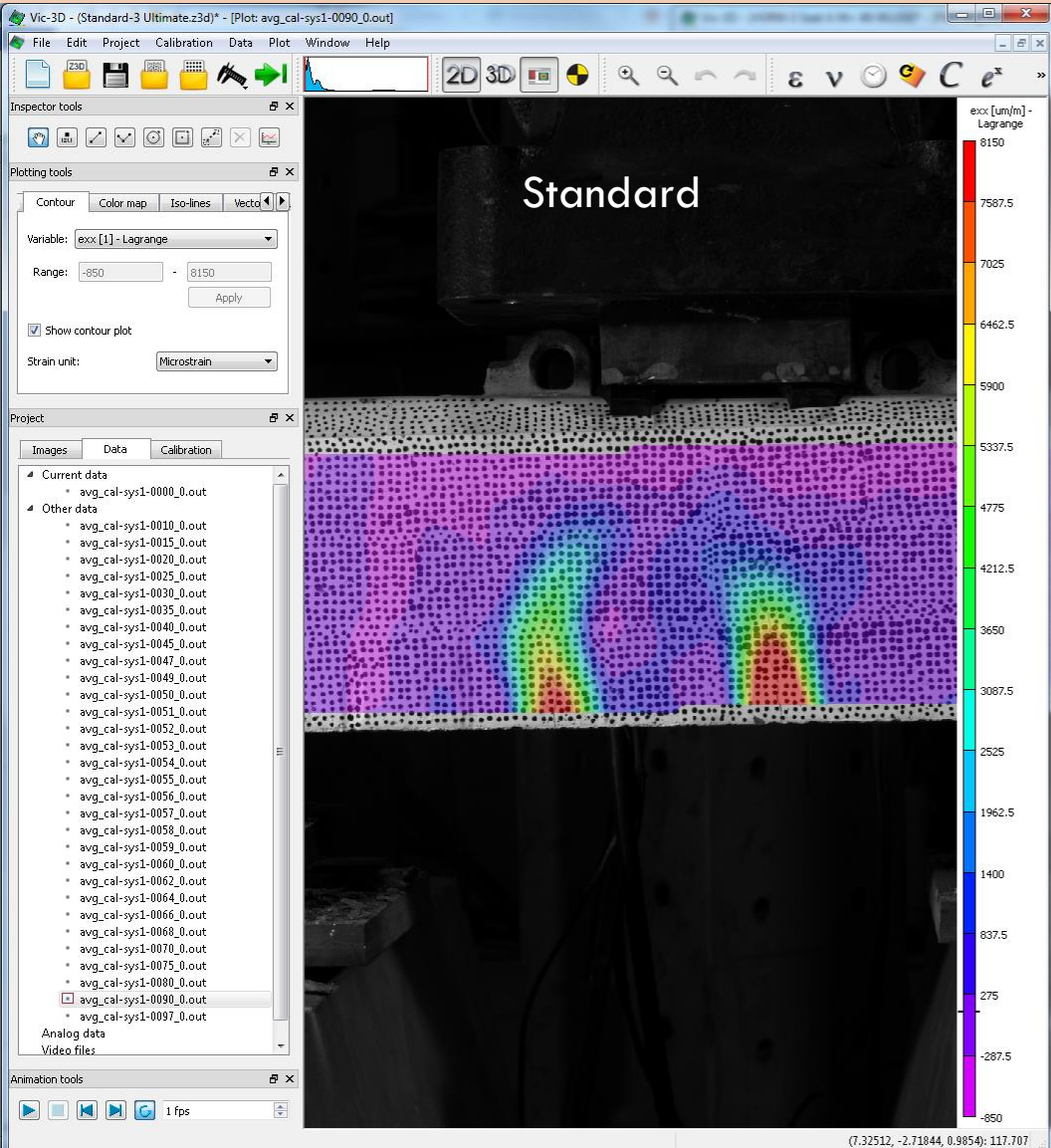


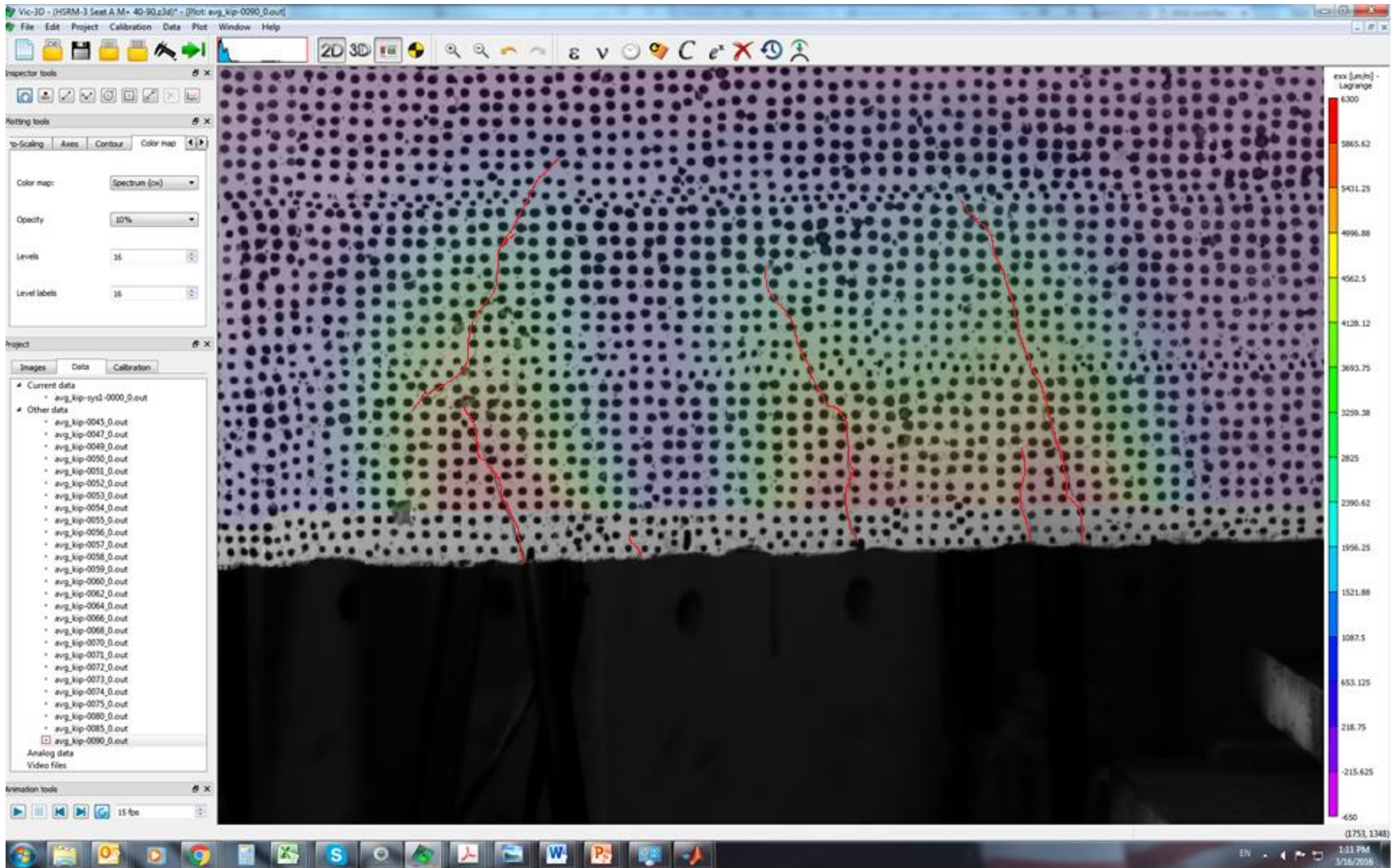






P=90 kips – Same Scale





Fatigue - Center Negative

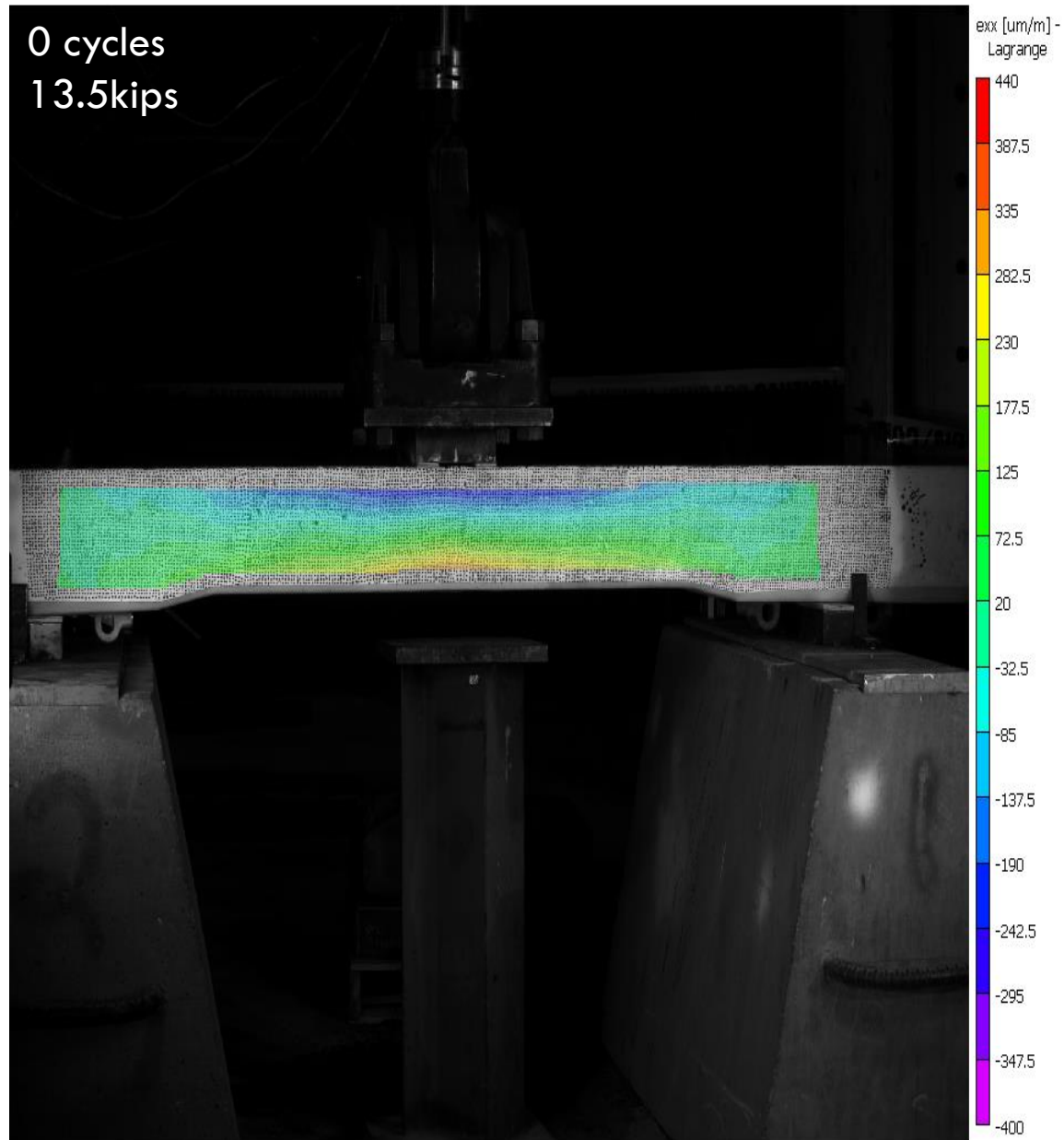
Test Setup

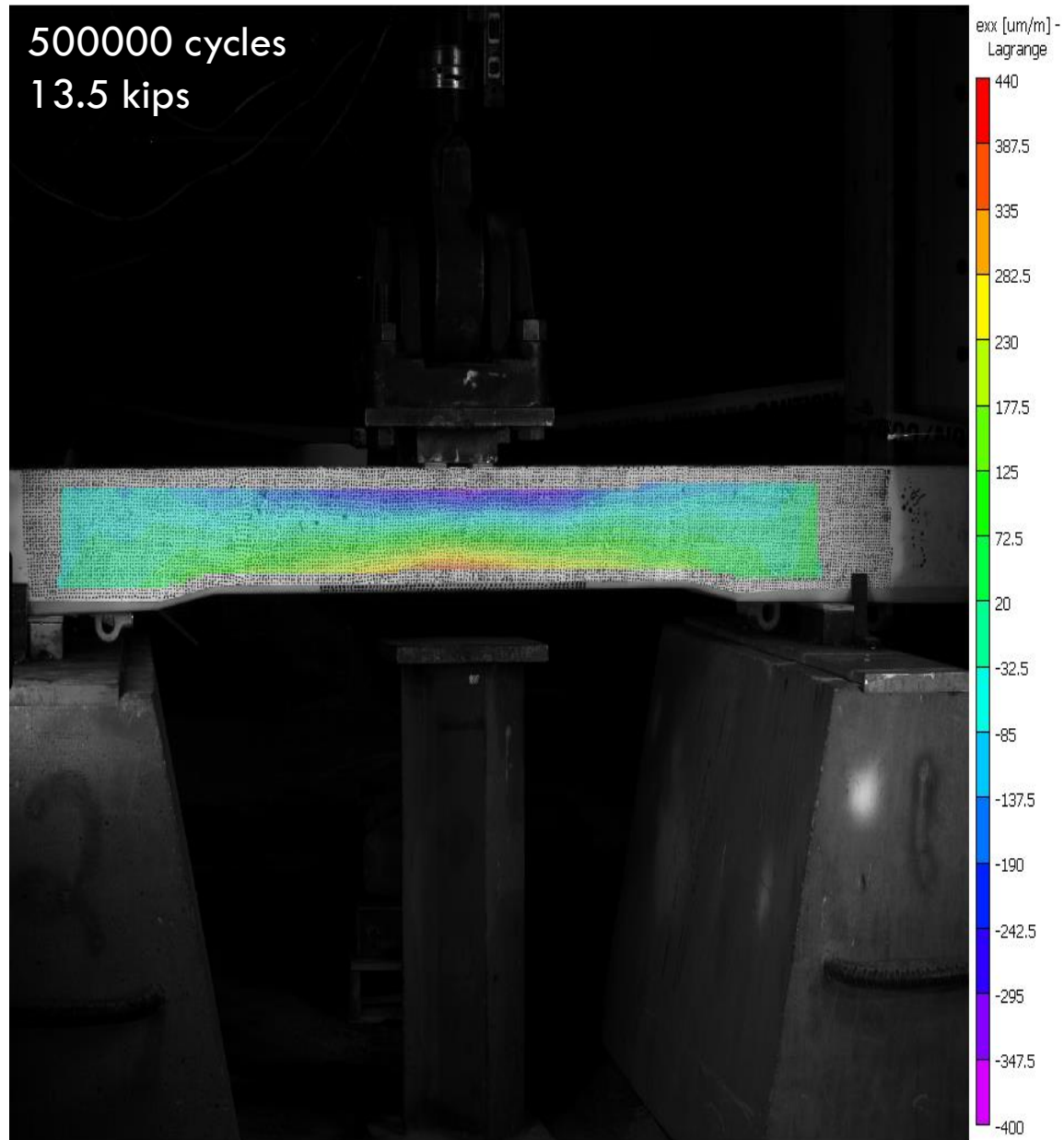


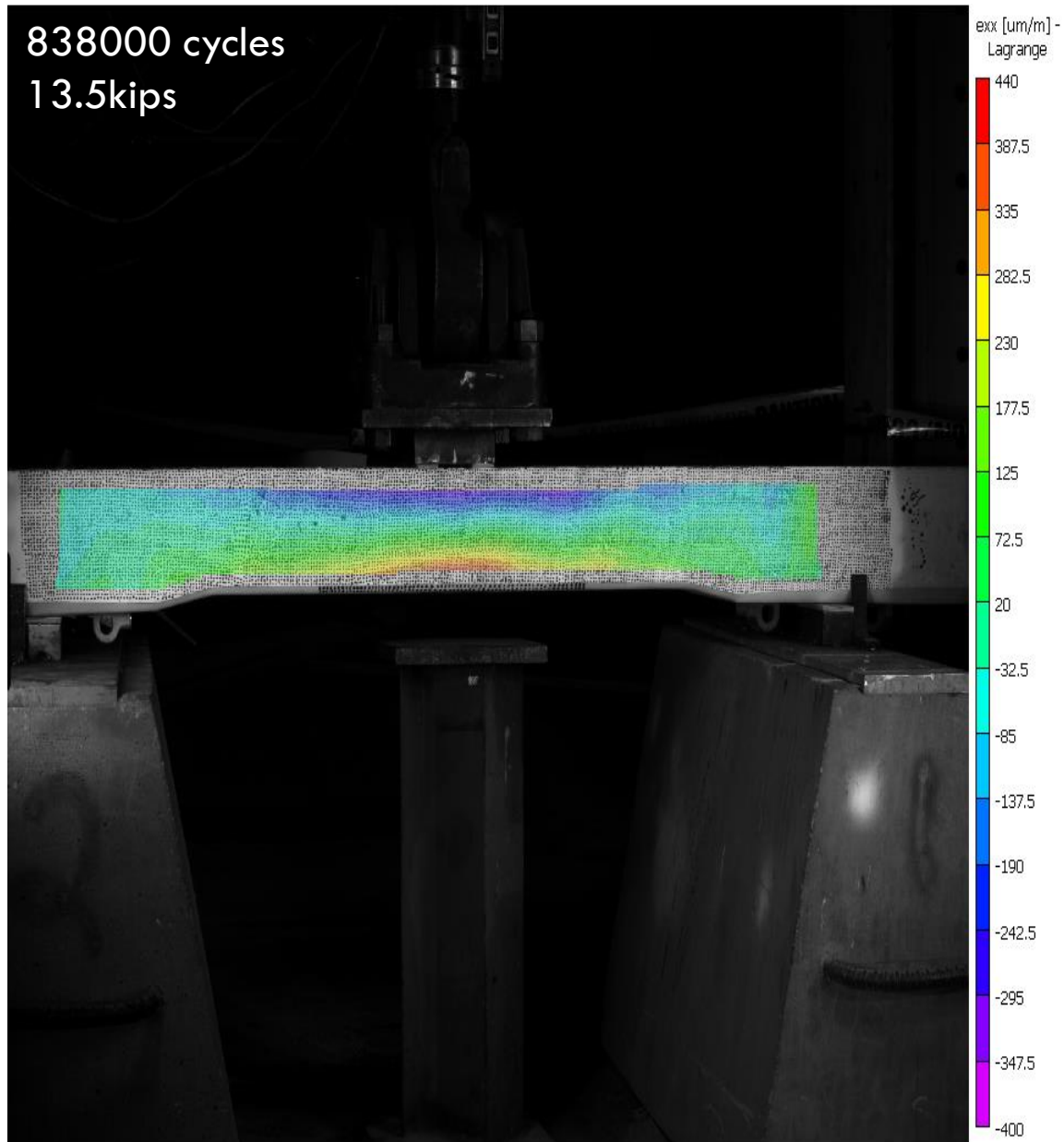
1. Specimen loaded to 90% of design load (13.5 kips)
 - Strain field captured every 2 kips
2. Cyclic Loading in the range 2-13.5 kips at a rate of 2 load cycles/sec
3. At 500,000 load cycles cyclic loading is paused and the specimen is loaded statically to 90% of design load
 - Strain field captured every 2 kips
4. Cyclic load resumes and continues for ~48 hours (~345,000 additional cycles)
5. Cyclic loading is paused and the specimen is loaded statically to 90% of design load
 - Strain field captured every 2 kips
6. Steps 4-6 are repeated until number of loading cycles exceeds 3 million.

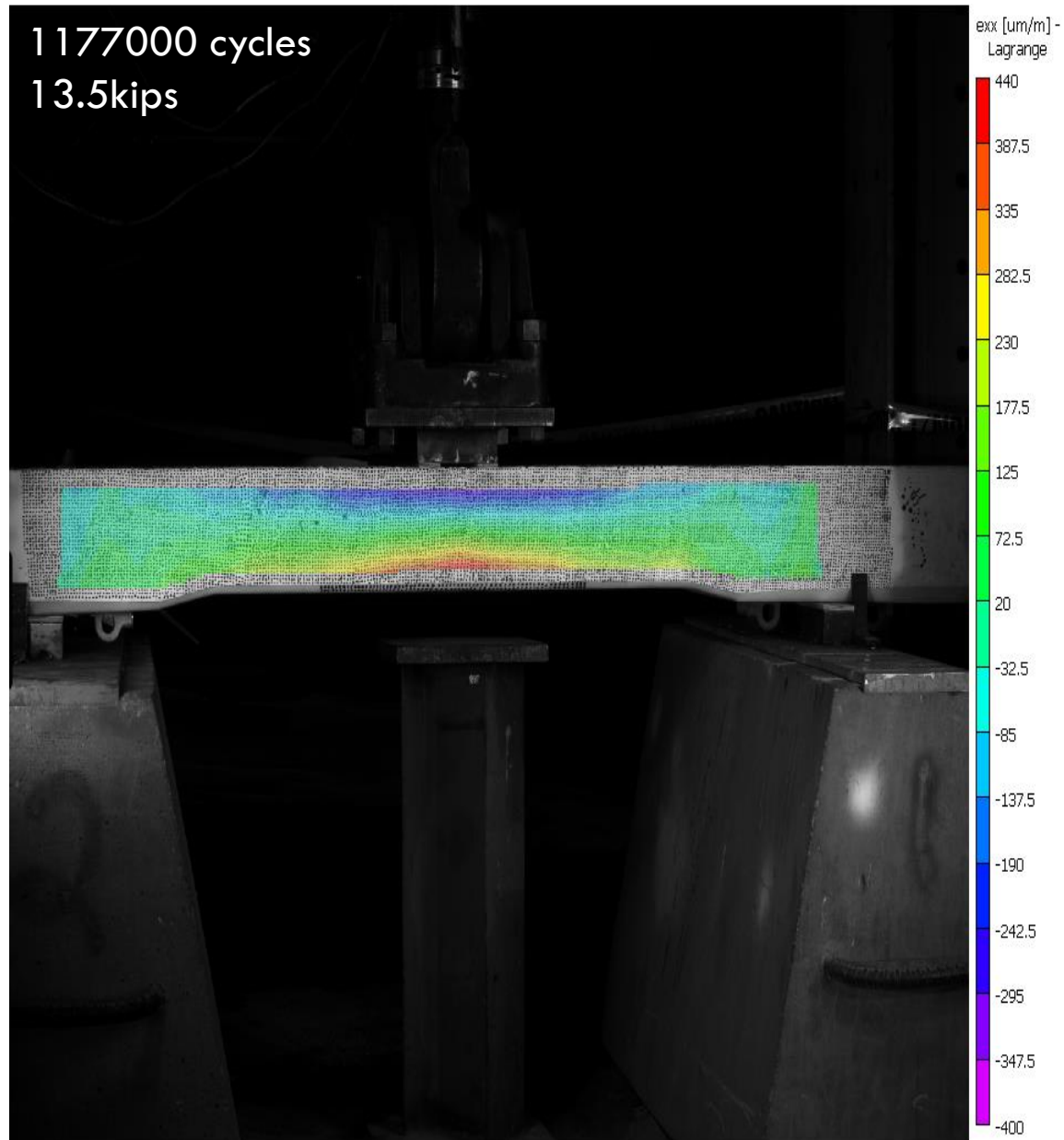
7. A crack is induced to the first line of strands and the corresponding load P_{crack} is recorded as 17.5 kips (to first strand).
 - Strain field captured every 2 kips
8. Cyclic Loading in the range 2 kips - 110% of design load (2-16.5 kips) at a rate of 2 load cycles/sec.
9. At 500,000 load cycles cyclic loading is paused and the specimen is loaded statically to design load.
 - Strain field captured every 2 kips
10. Cyclic load resumes and continues for ~48 hours (~345,000 additional cycles)
11. Cyclic loading is paused and the specimen is loaded statically to 110% design load (16.5 kip)
 - Strain field captured every 2 kips
12. Steps 10-12 are repeated until number of loading cycles exceeds 3 million.
13. Specimen is loaded to failure
 - Strain field captured every 2 kips

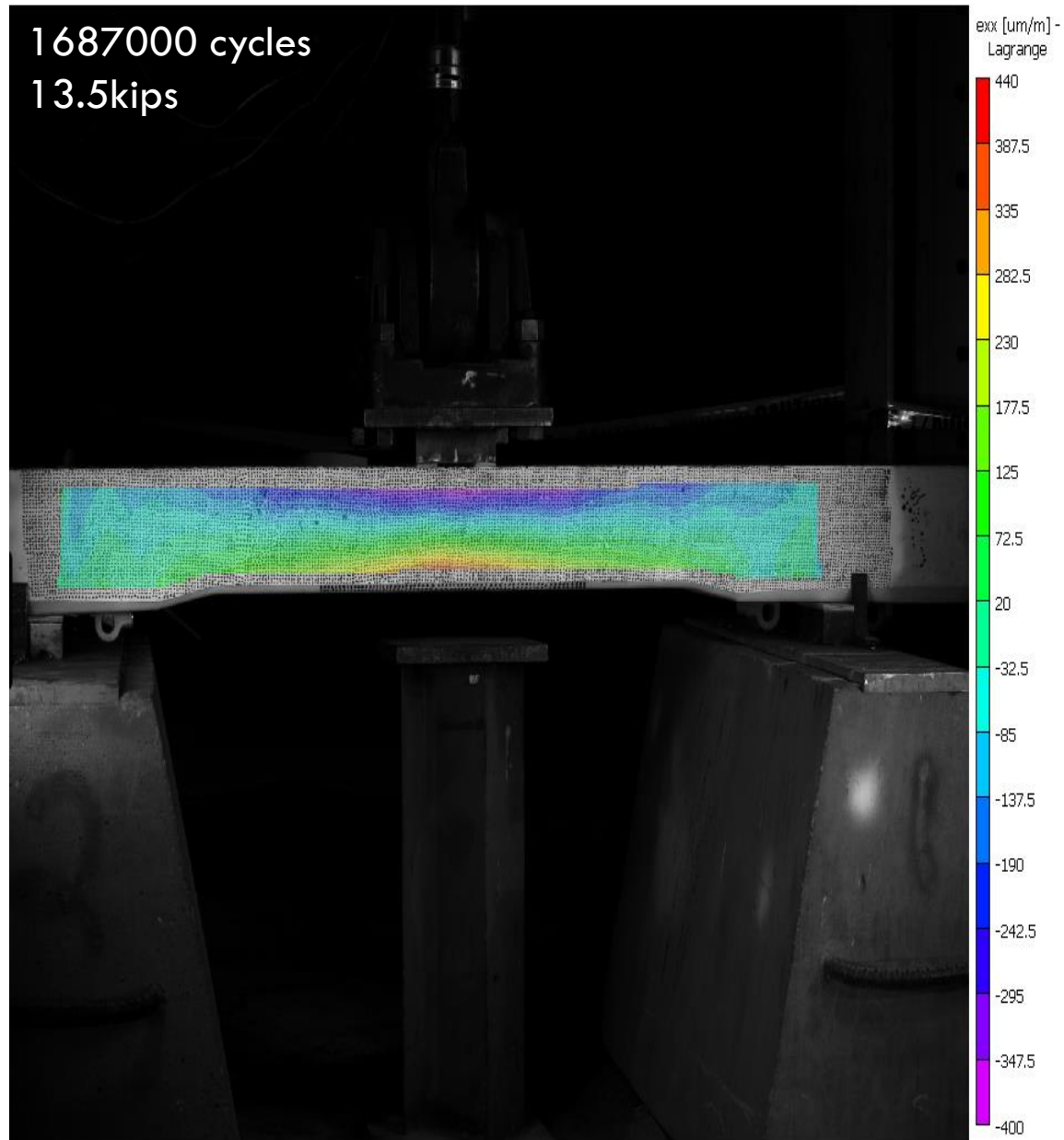
Stage 1 – No Crack
3,000,000 cycles

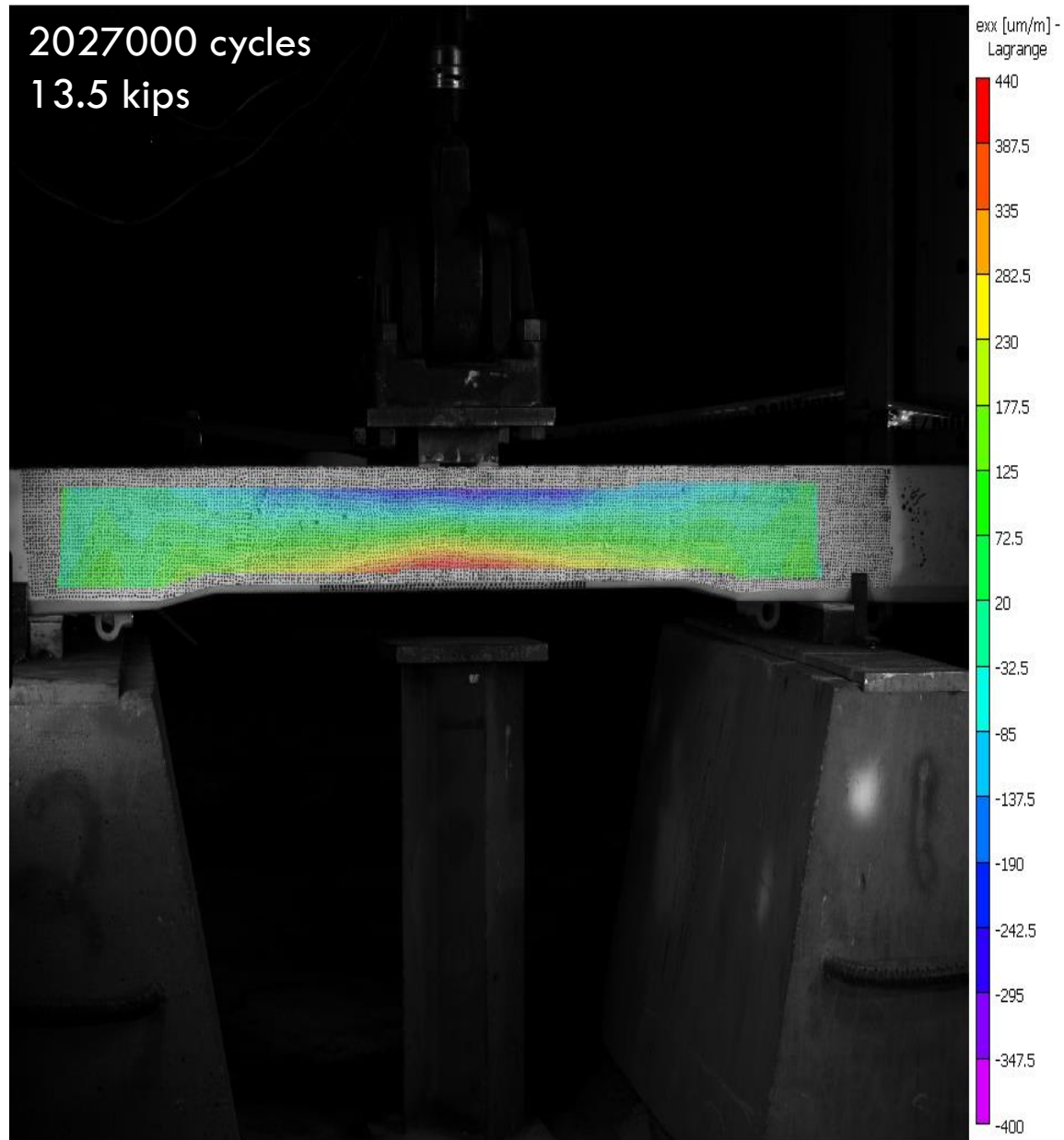


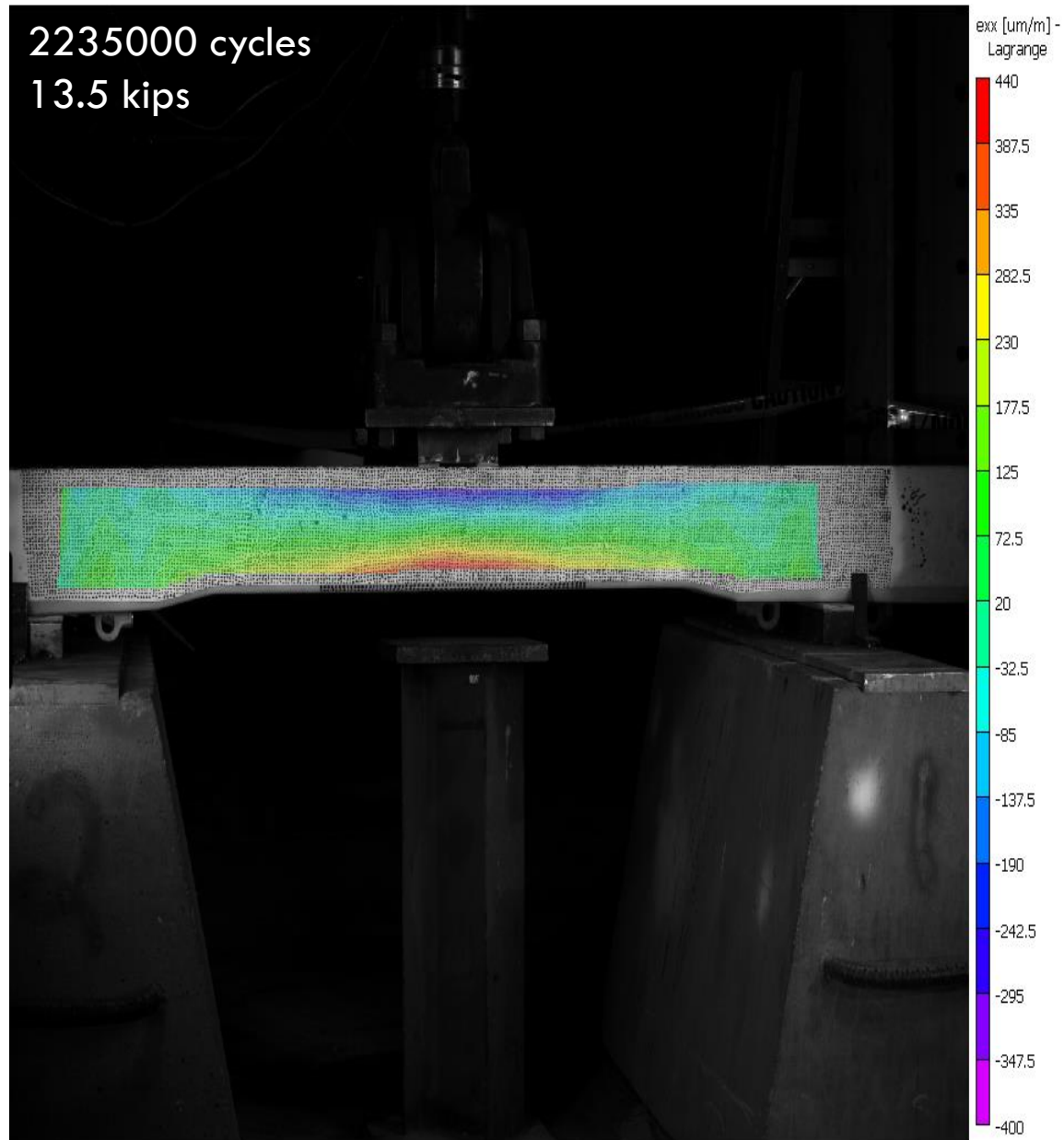


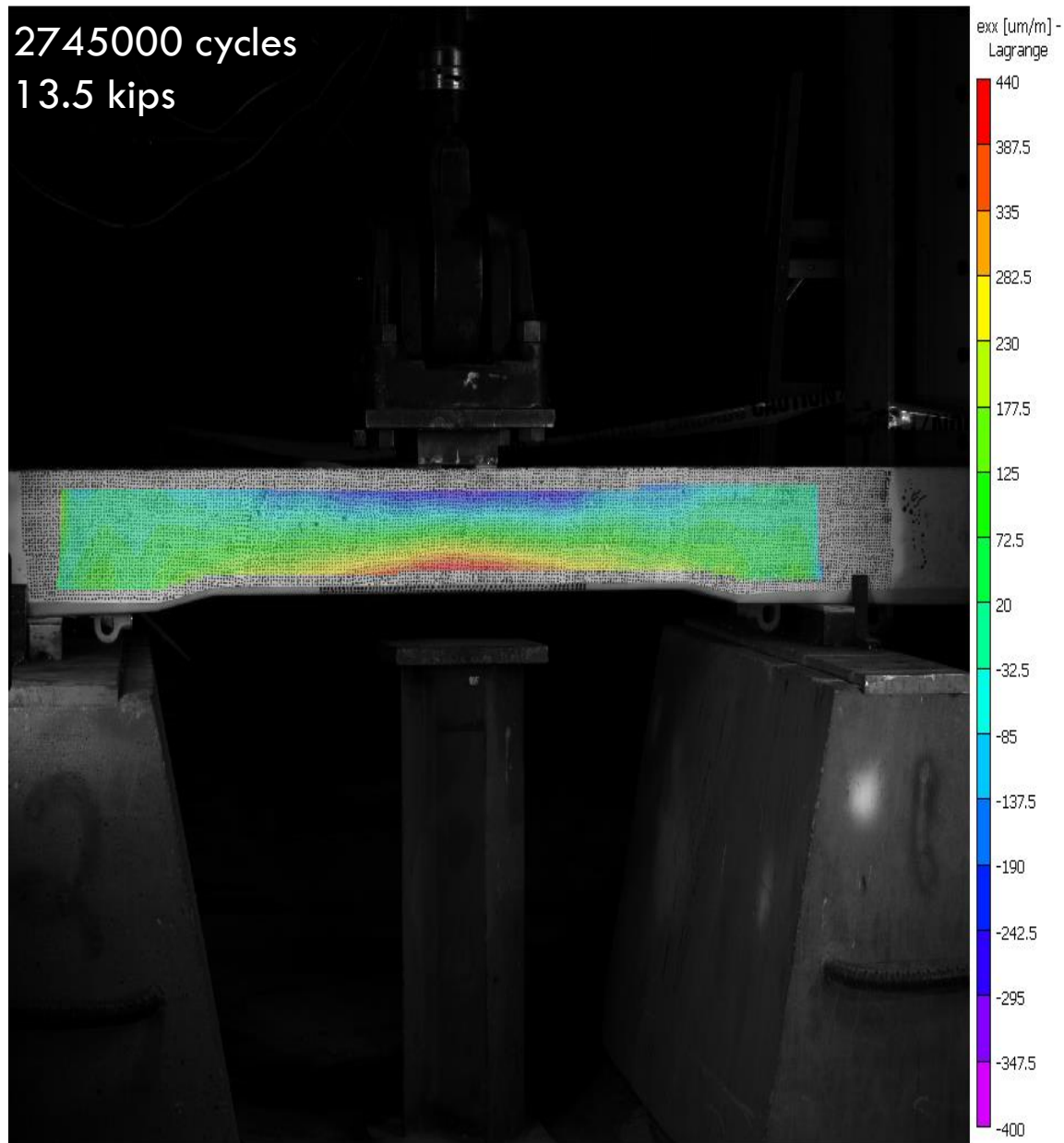


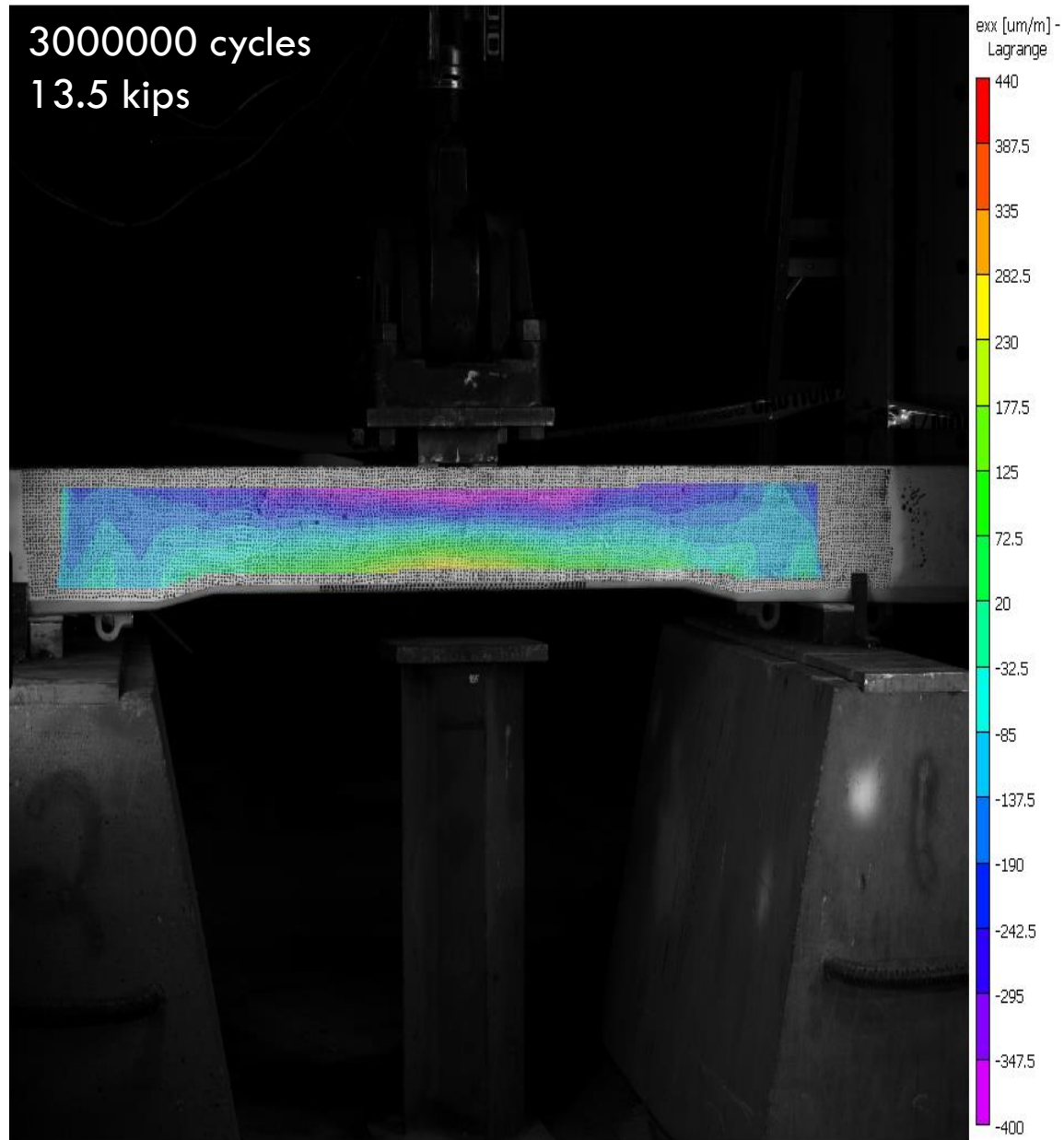








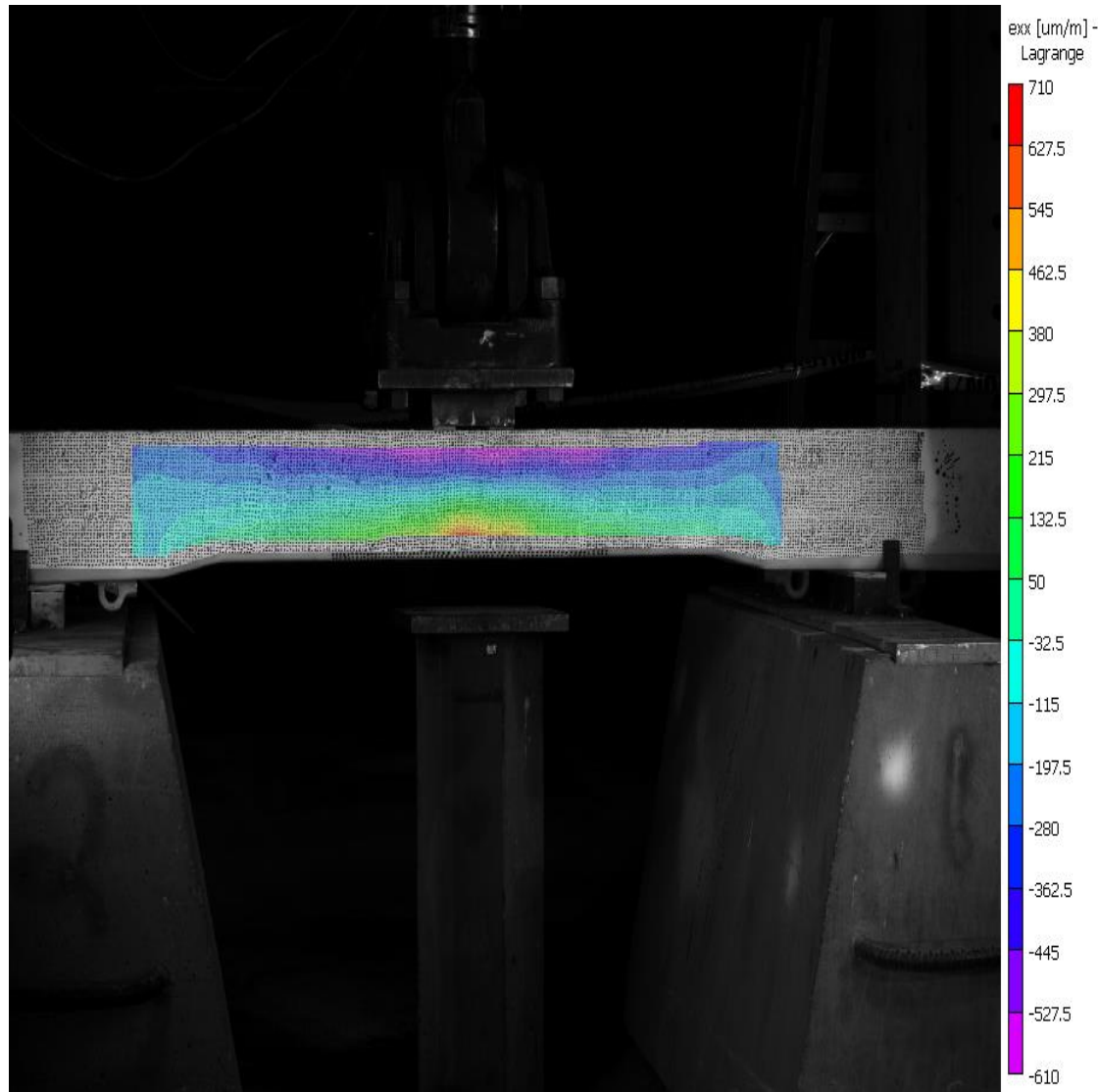




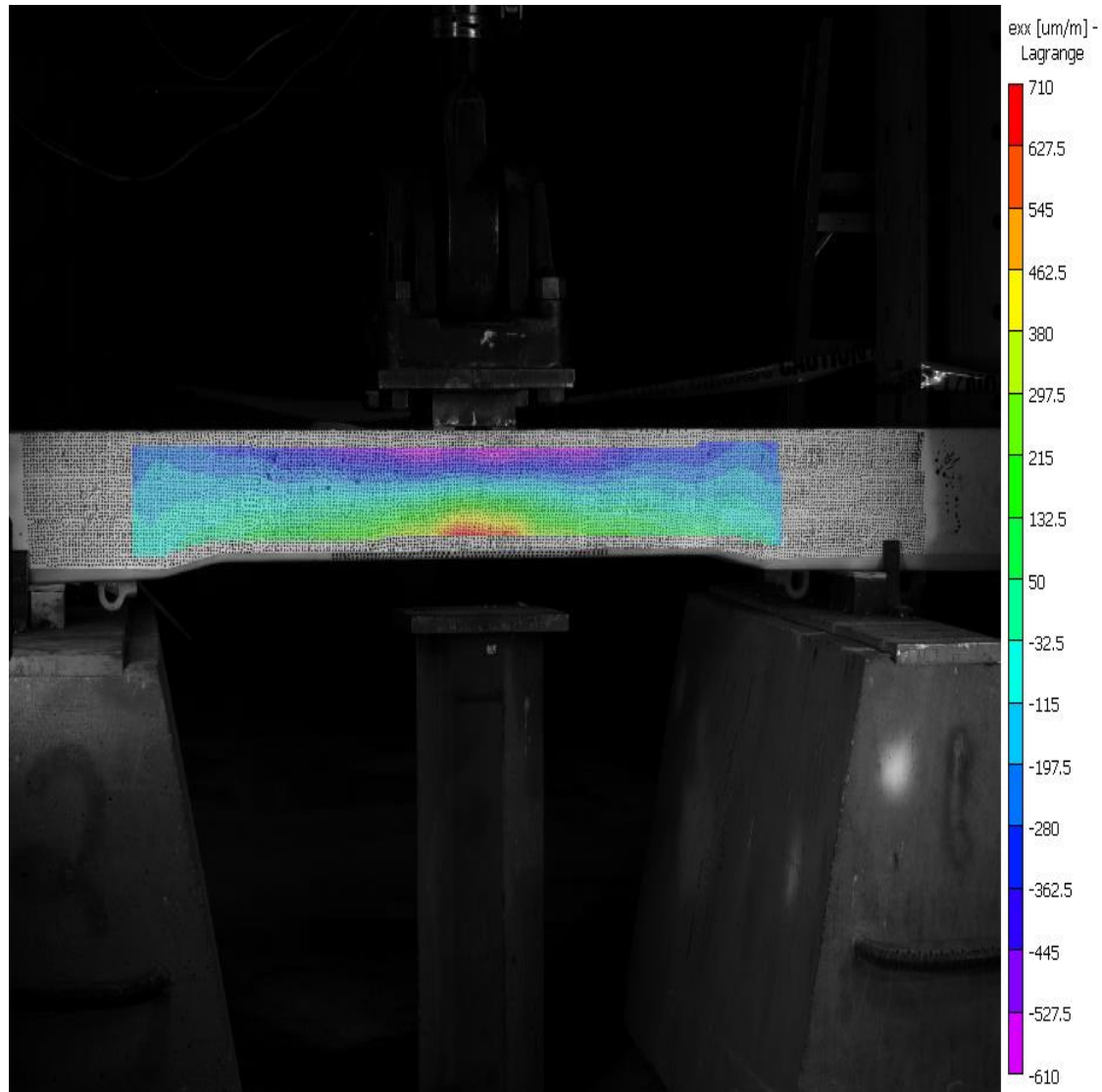
- ❑ No significant changes in the strain field as load accumulates
- ❑ No cracks observed through visual inspection and DIC measurements

Stage 2 - Cracking induced to first strand
Additional 3,000,000 cycles

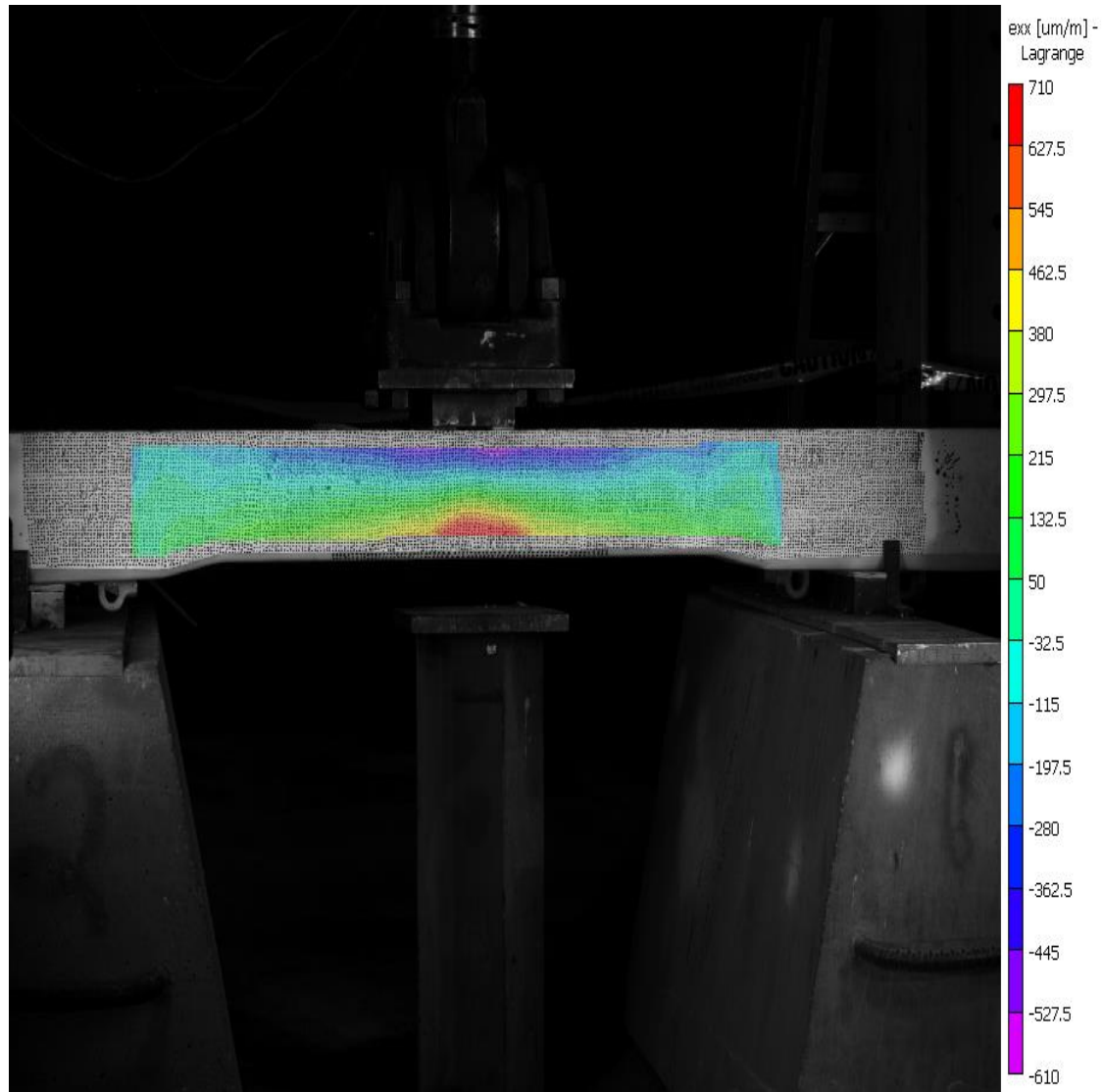
16.5 kip , 0 cycles



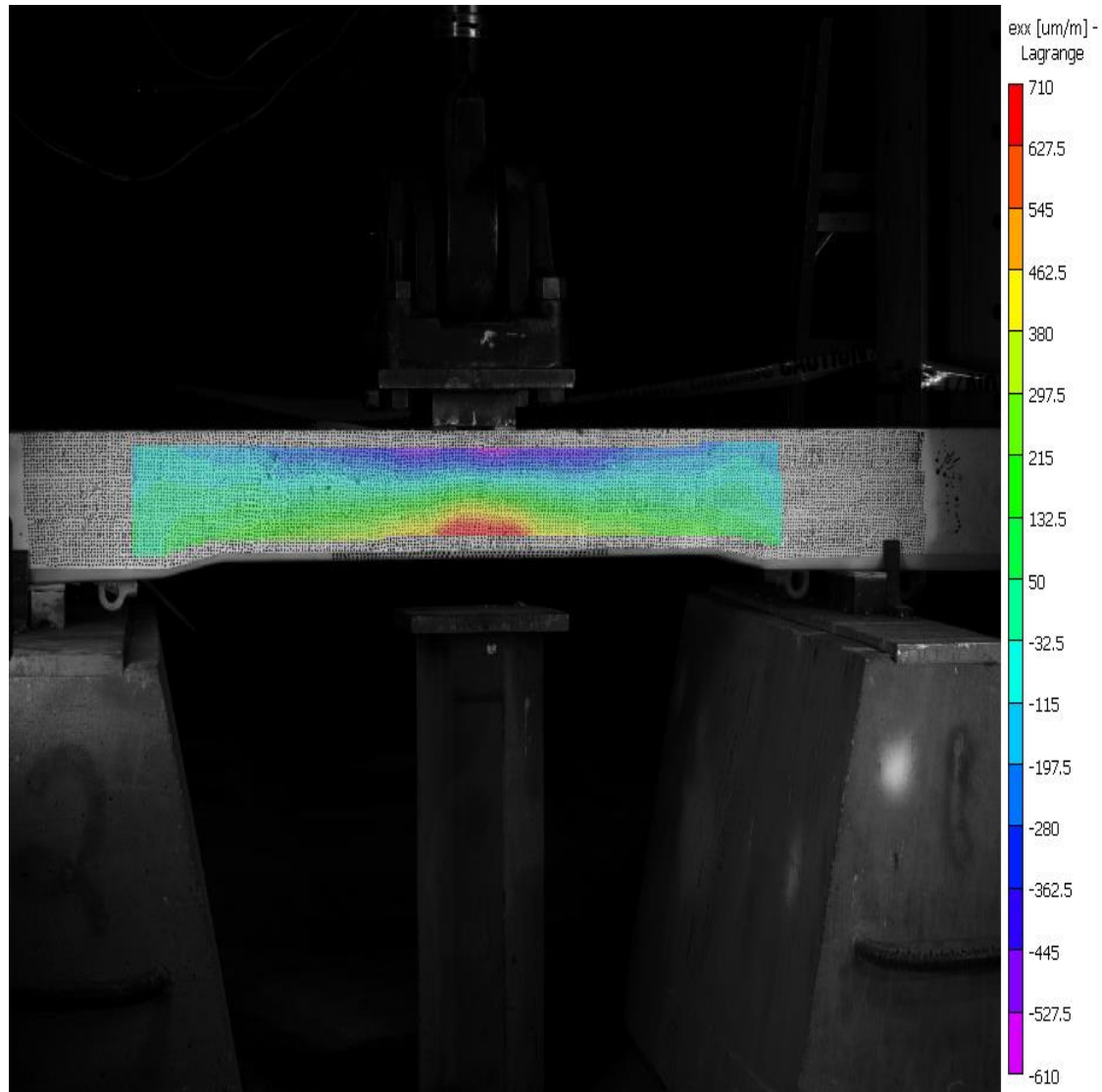
16.5 kip, 333250 cycles



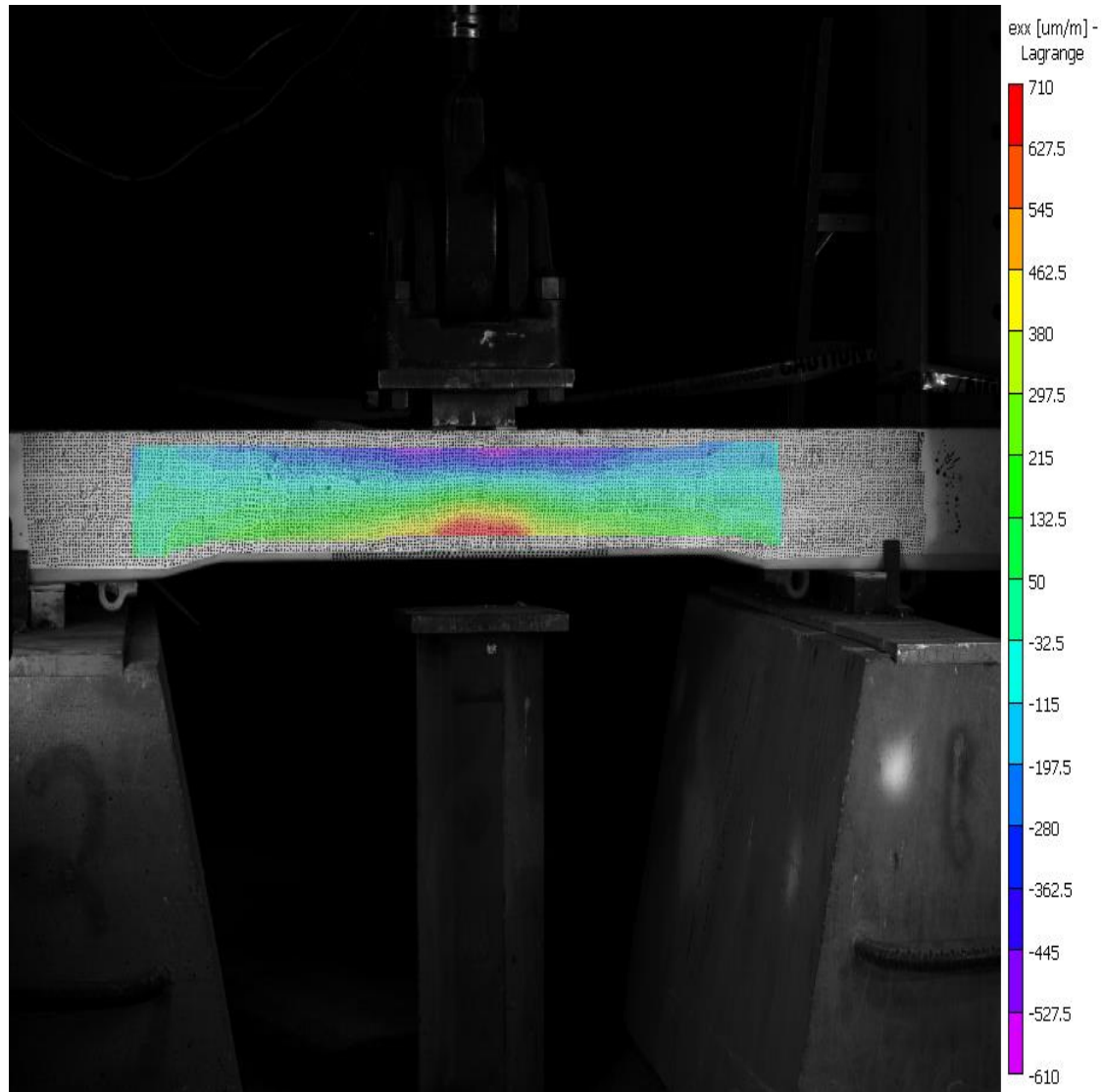
16.5kip , 848250 cycles



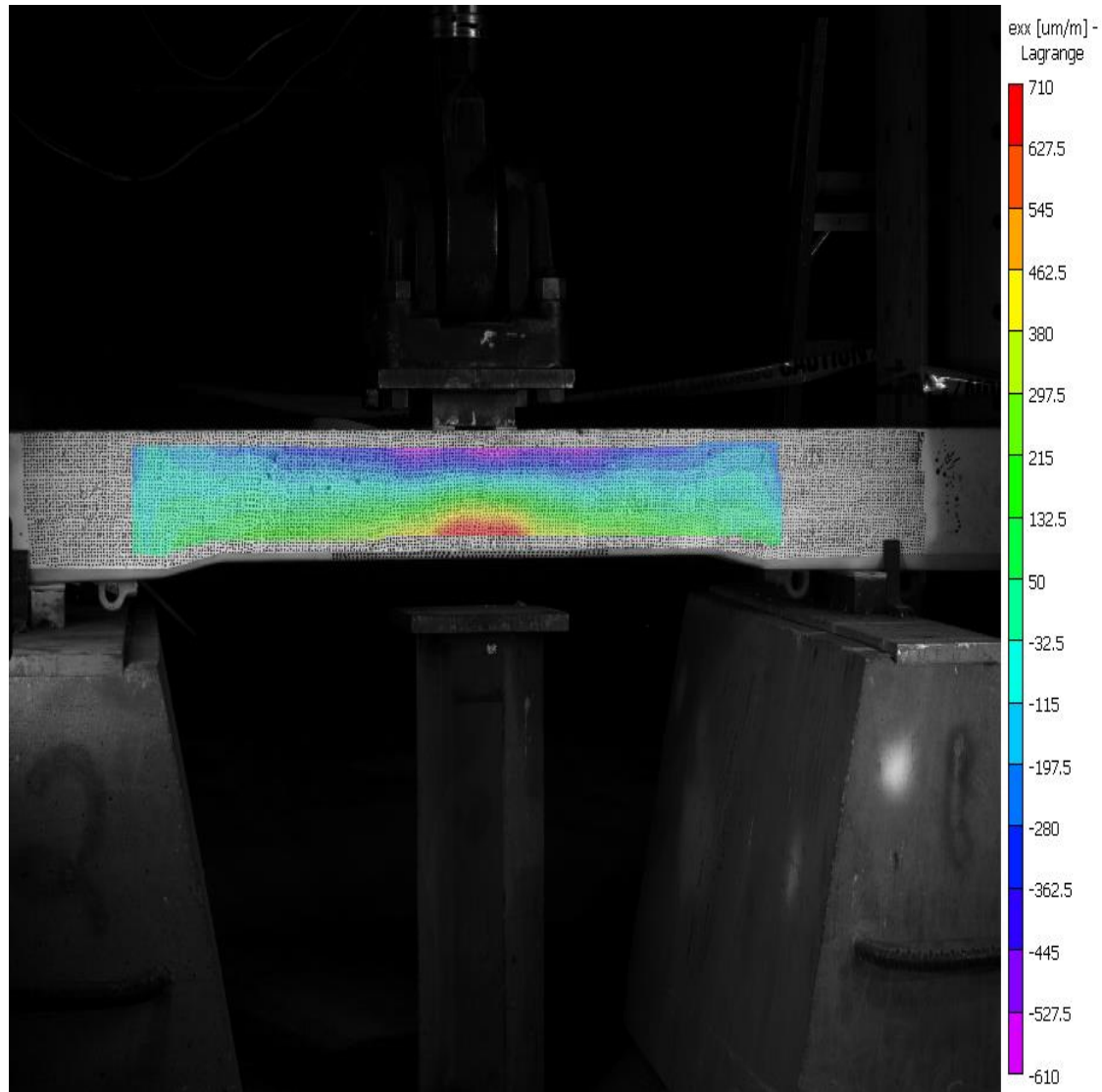
16.5kip , 1 348000 cycles



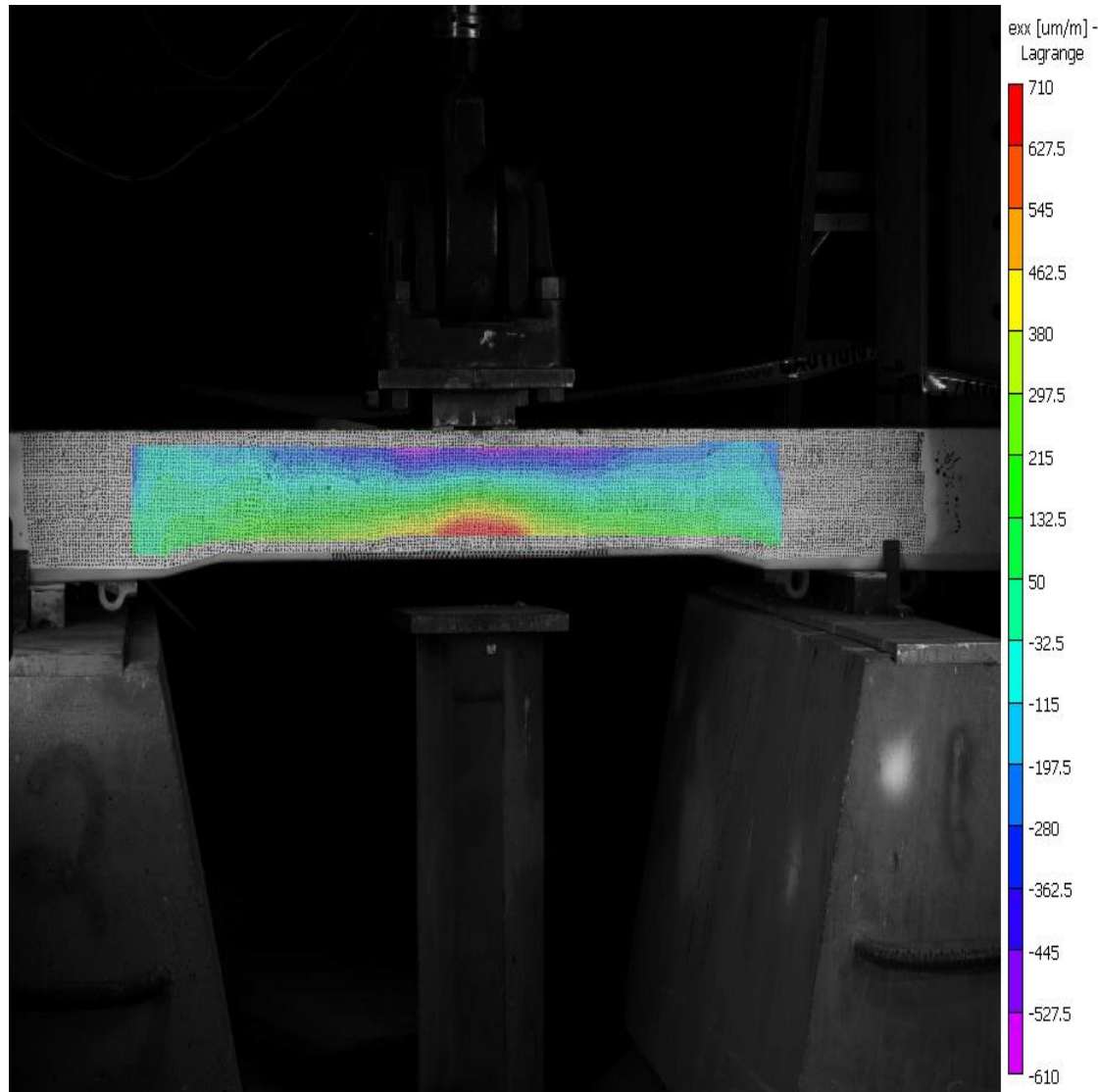
16.5kip , 1848000 cycles



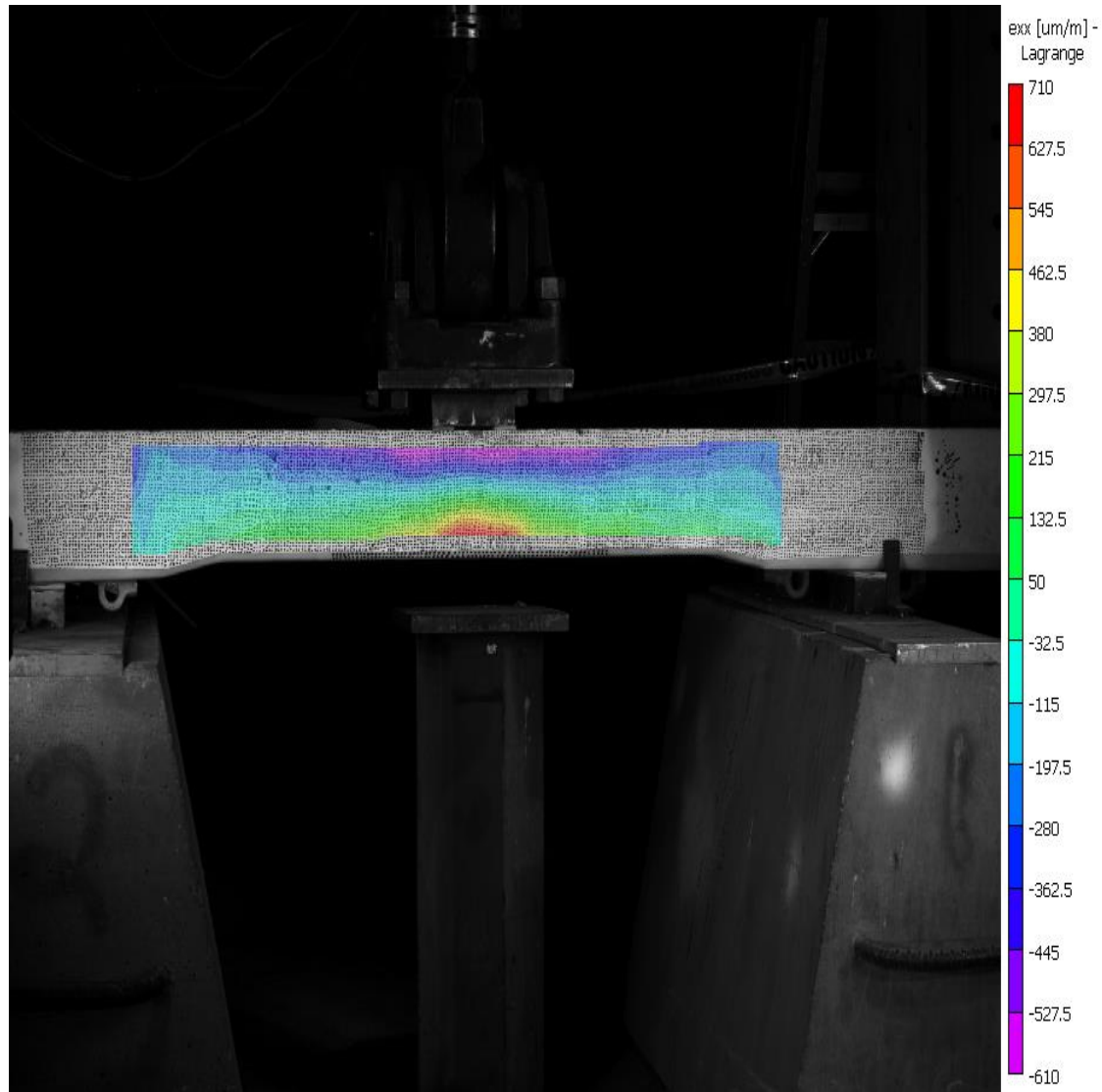
16.5kip , 2174000 cycles



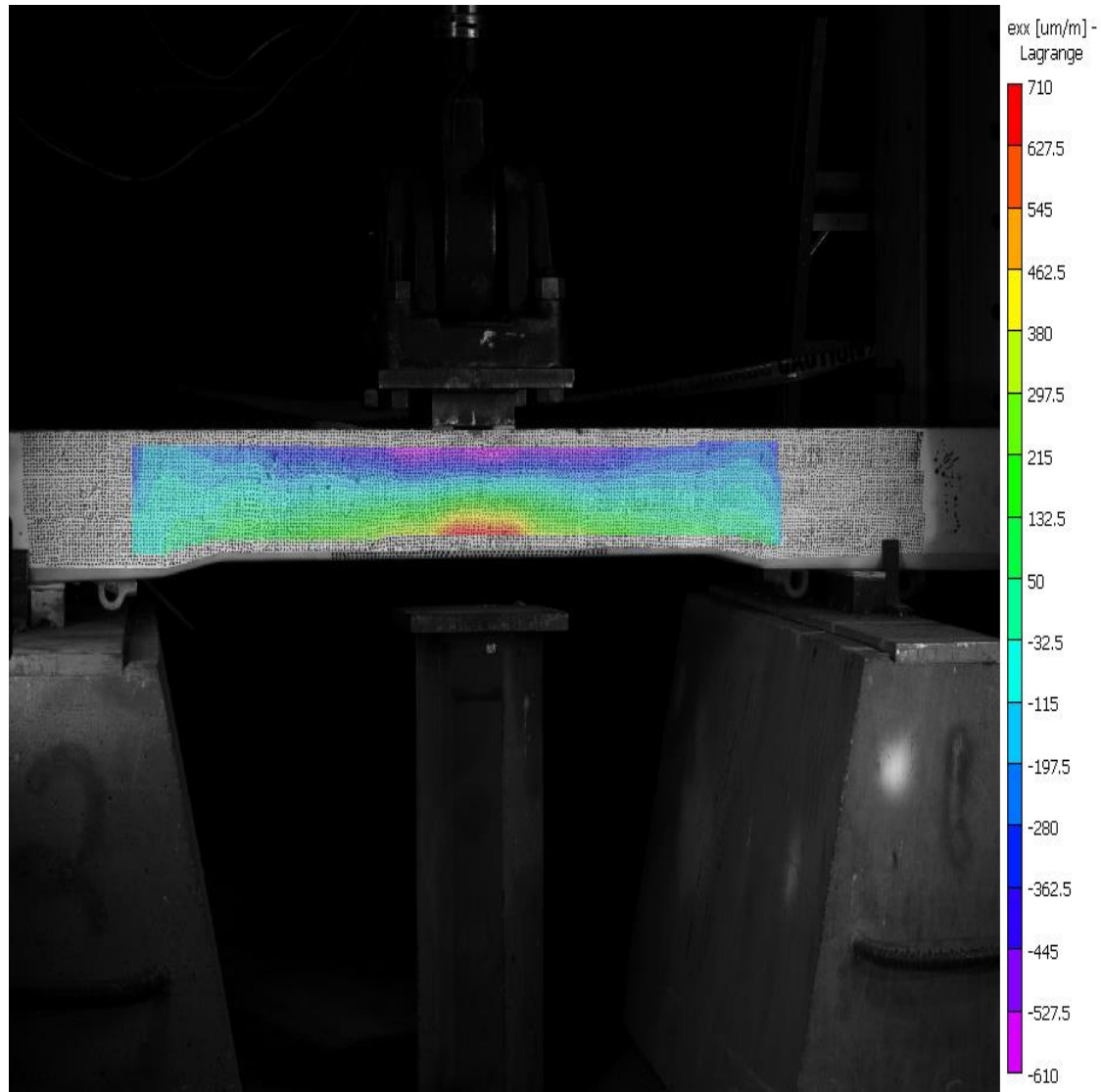
16.5kip , 2520000 cycles



16.5kip , 2852000 cycles

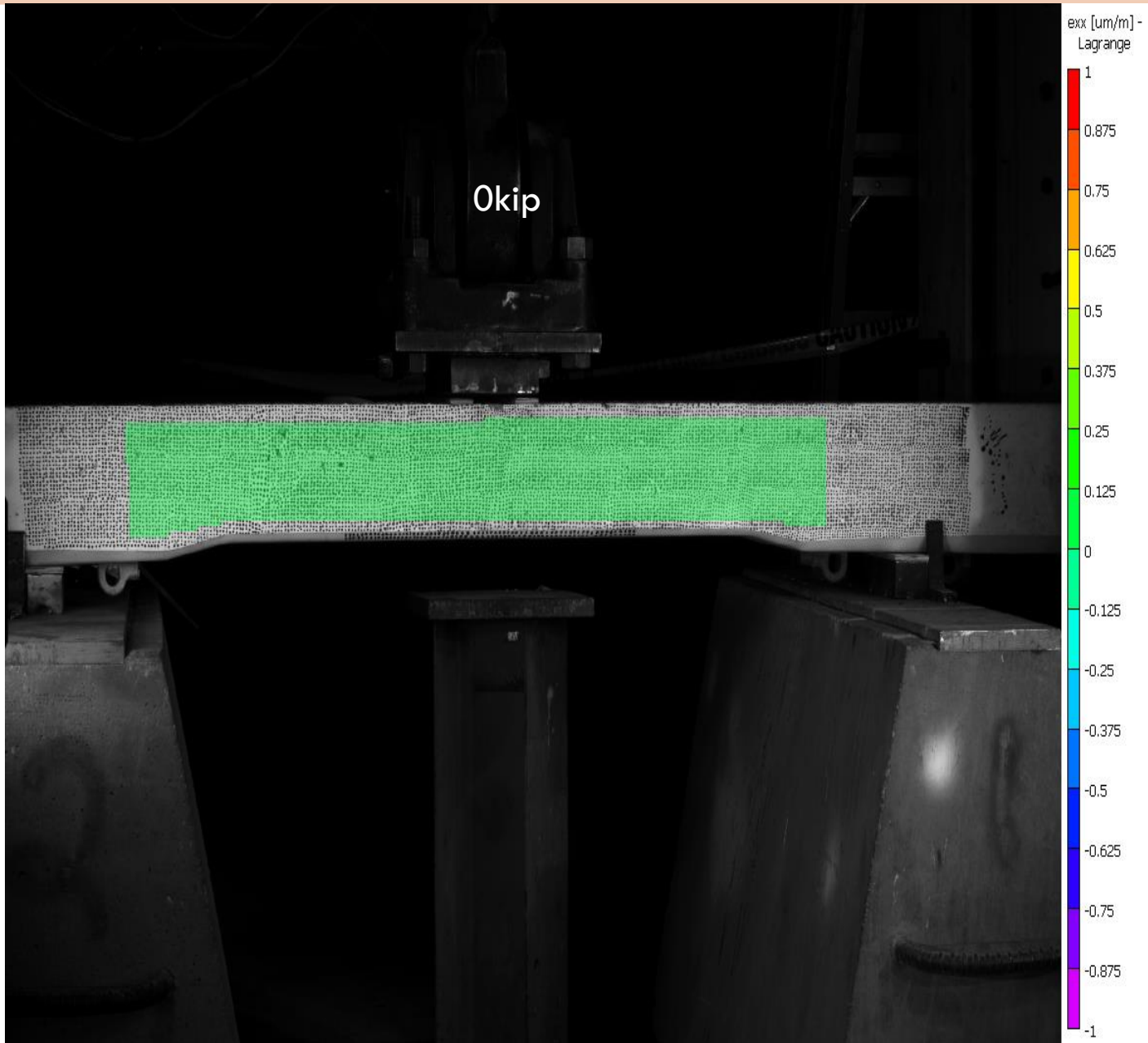


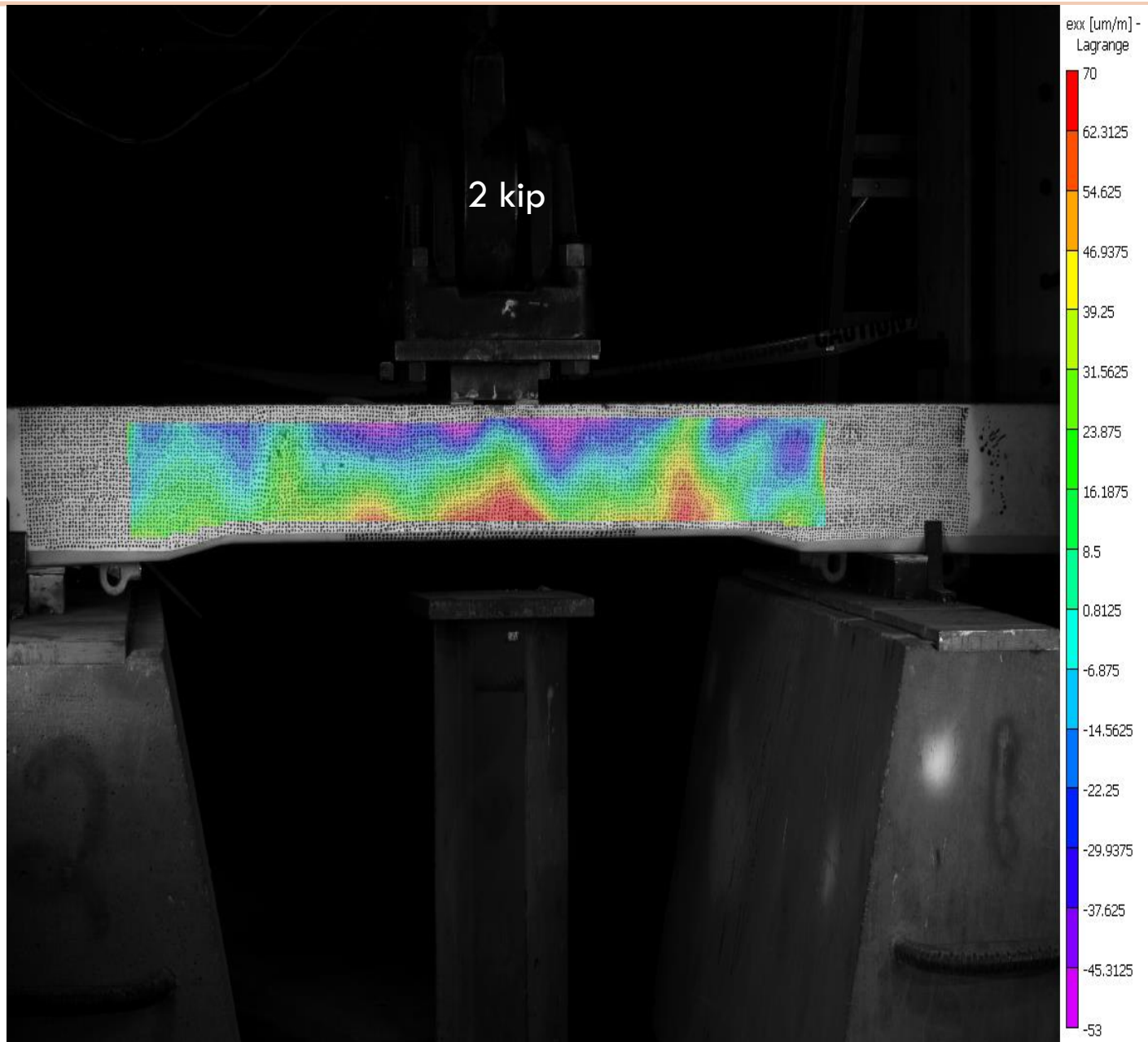
16.5kip , 3000000 cycles

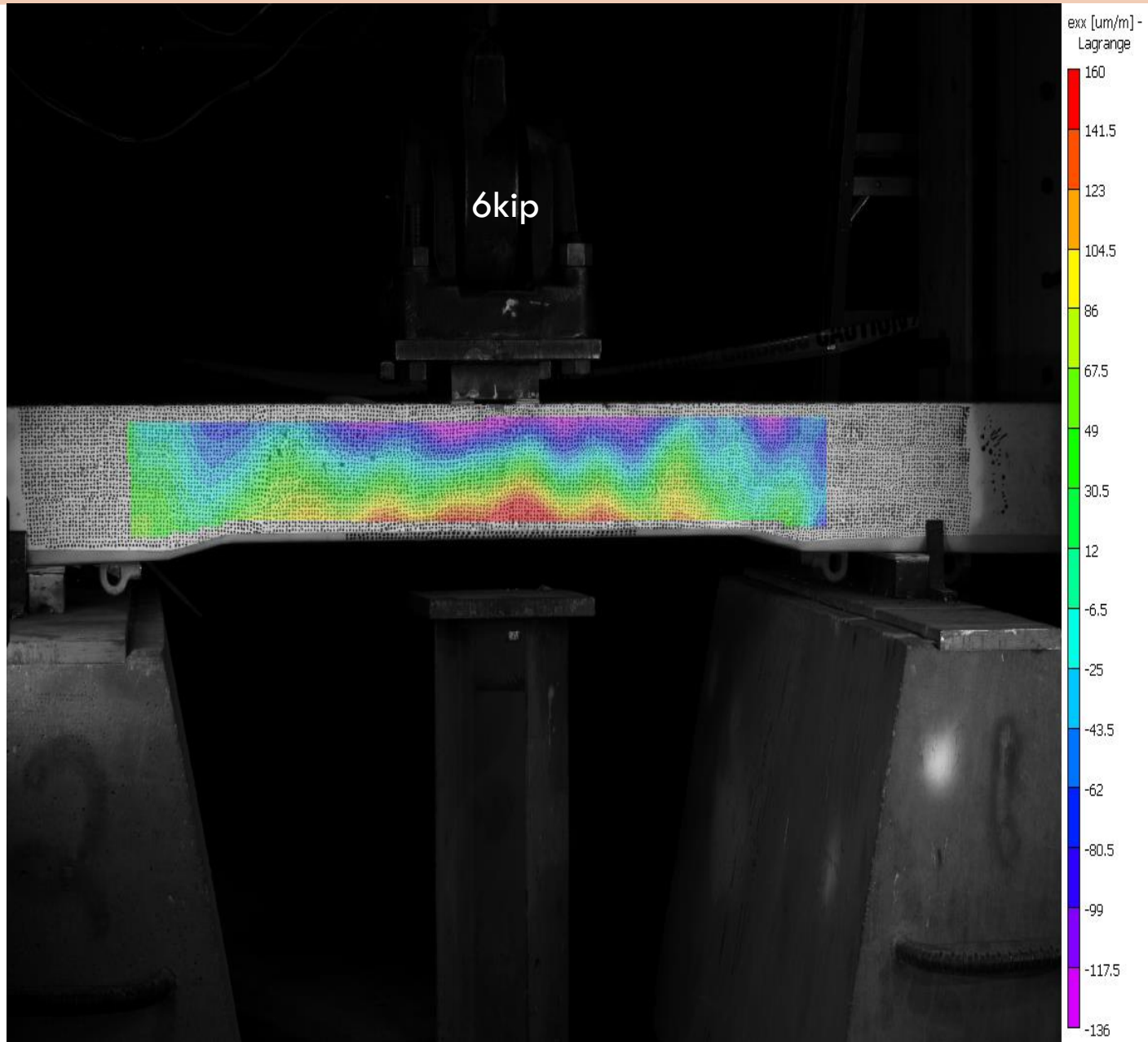


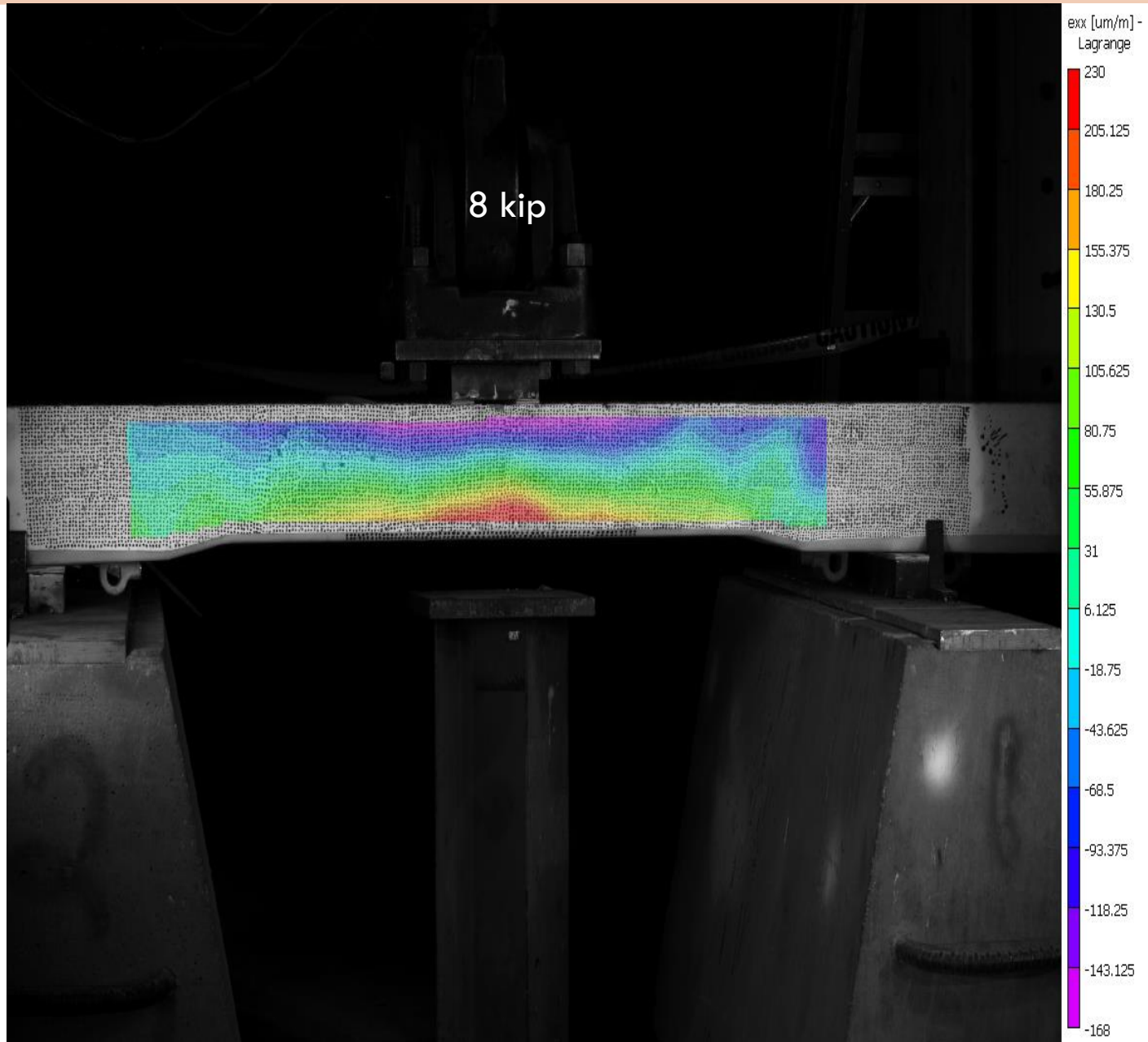
- ❑ Crack location is evident
- ❑ Stress redistribution during first 800,000 cycles
- ❑ No additional cracks observed
 - ❑ visual inspection and DIC measurements
- ❑ Existing crack did not propagate
 - ❑ visual inspection and DIC measurements

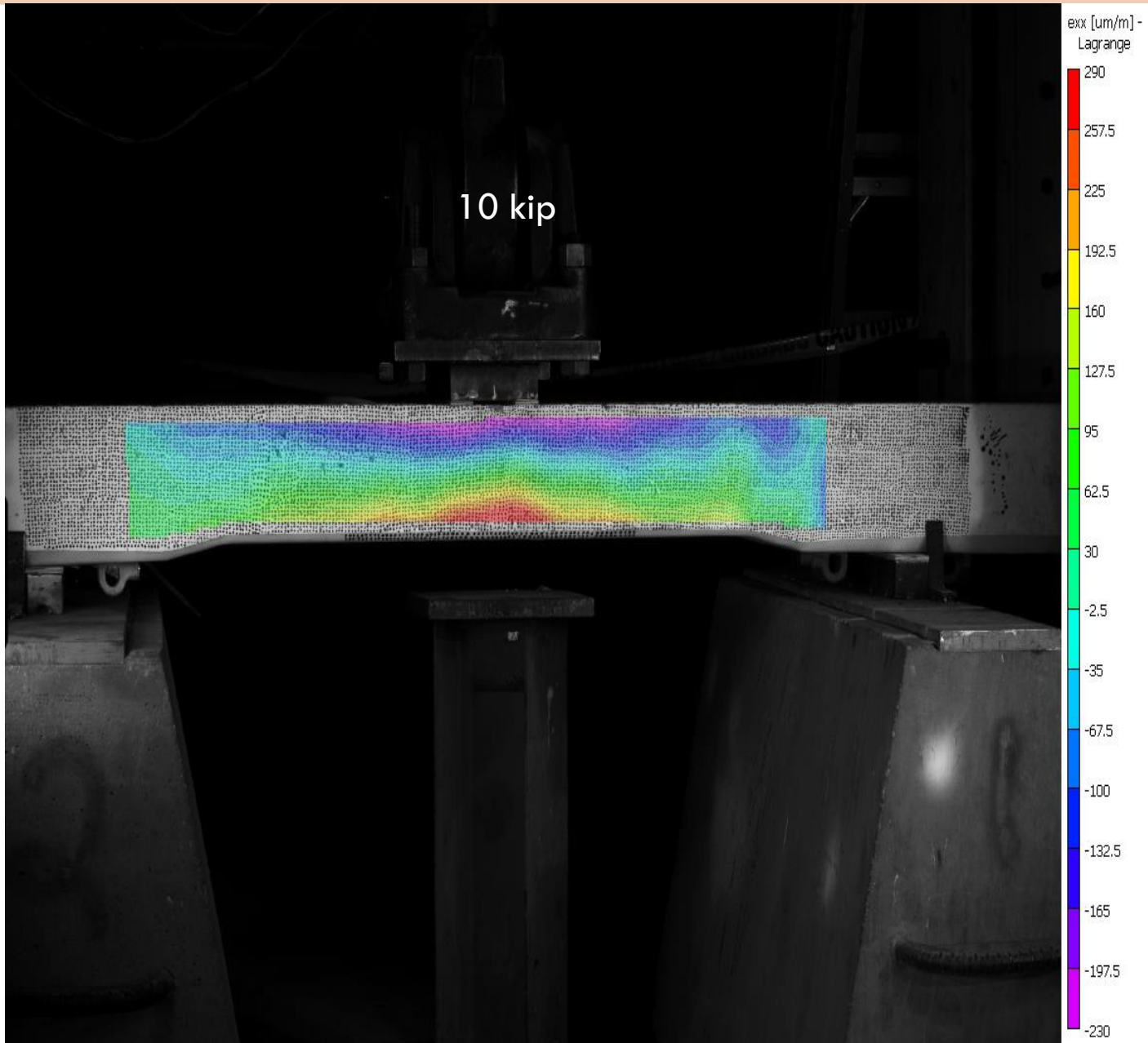
Stage 3 - Loading to Failure
After 6,000,000 total load cycles

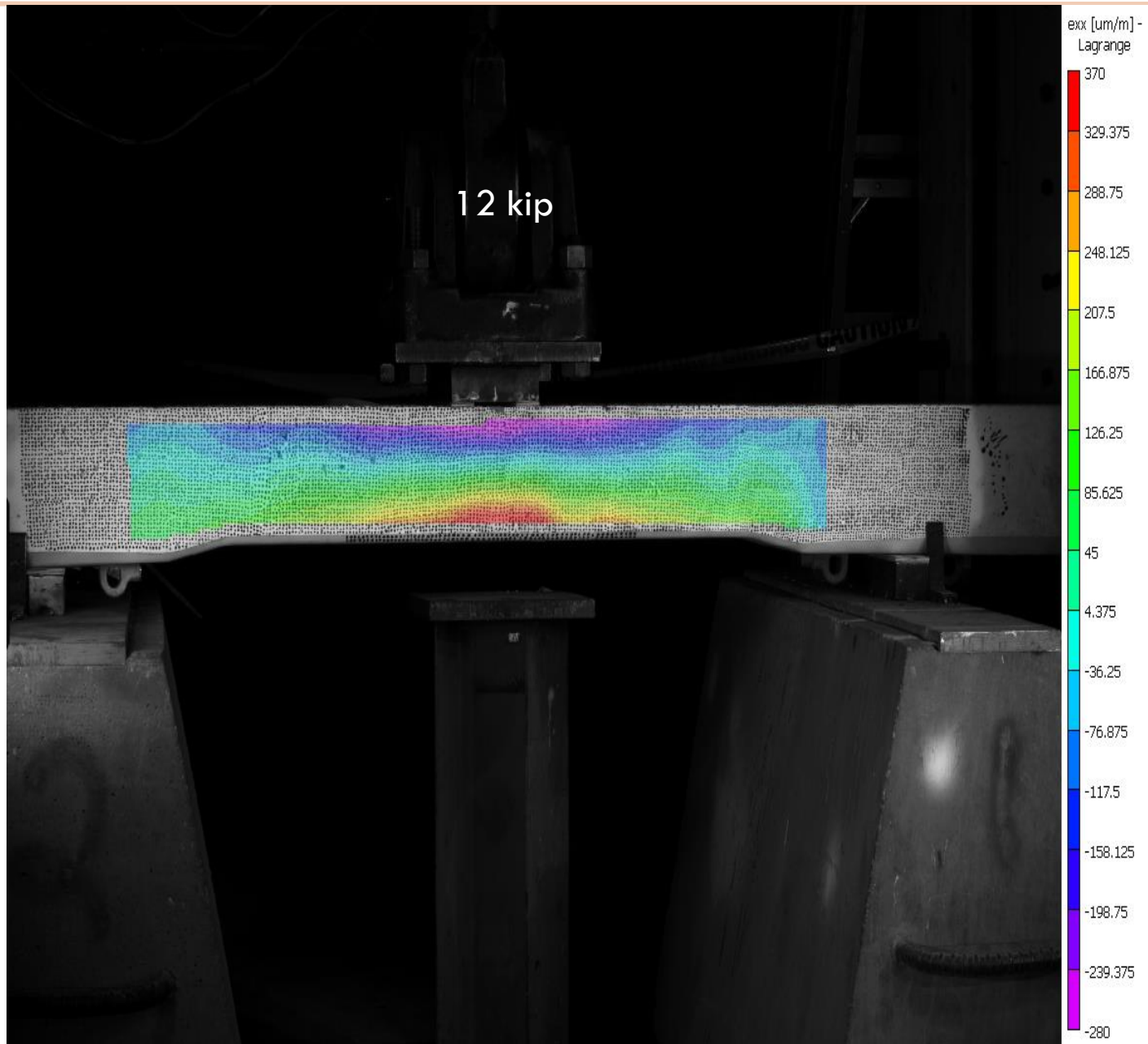


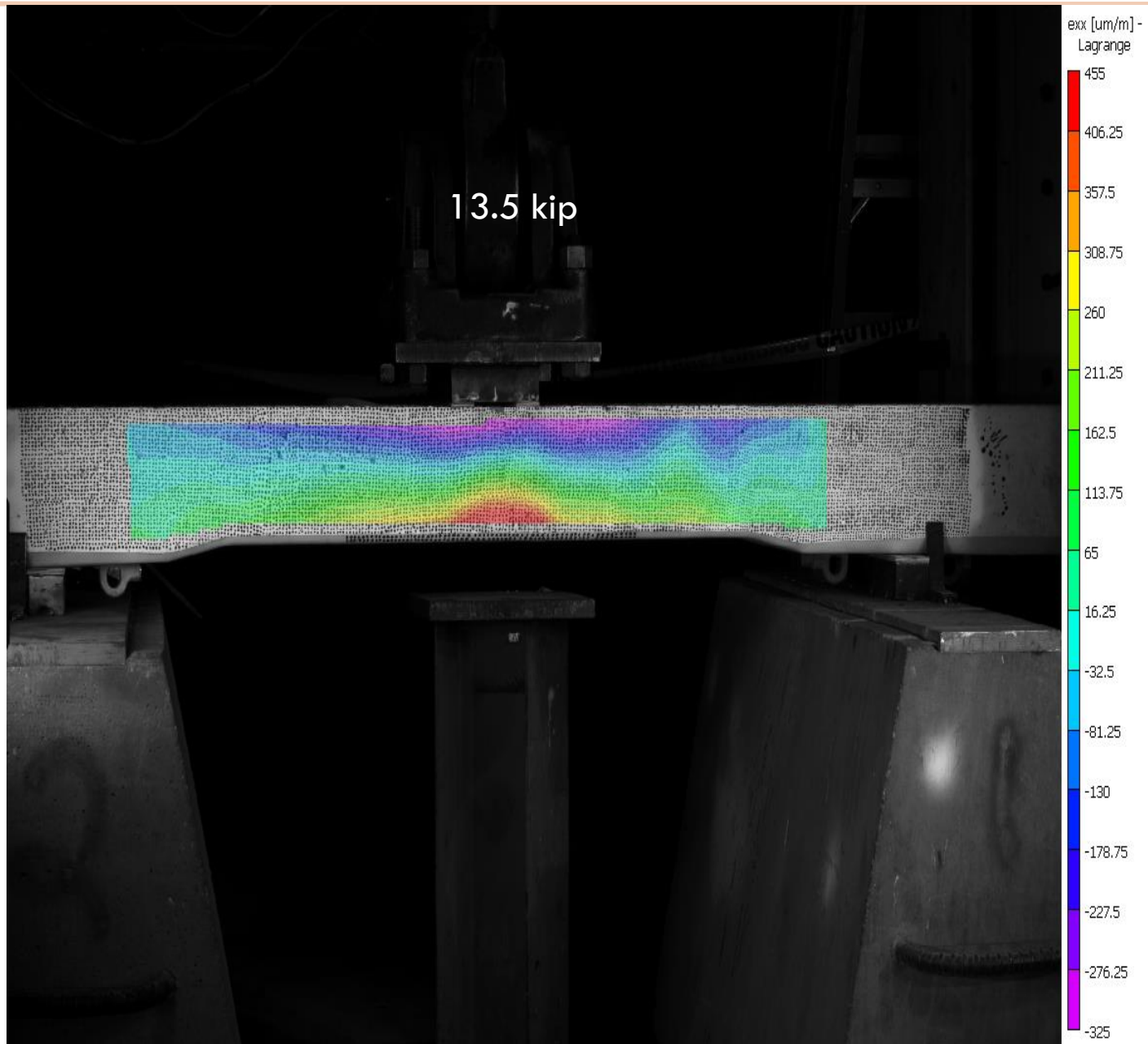


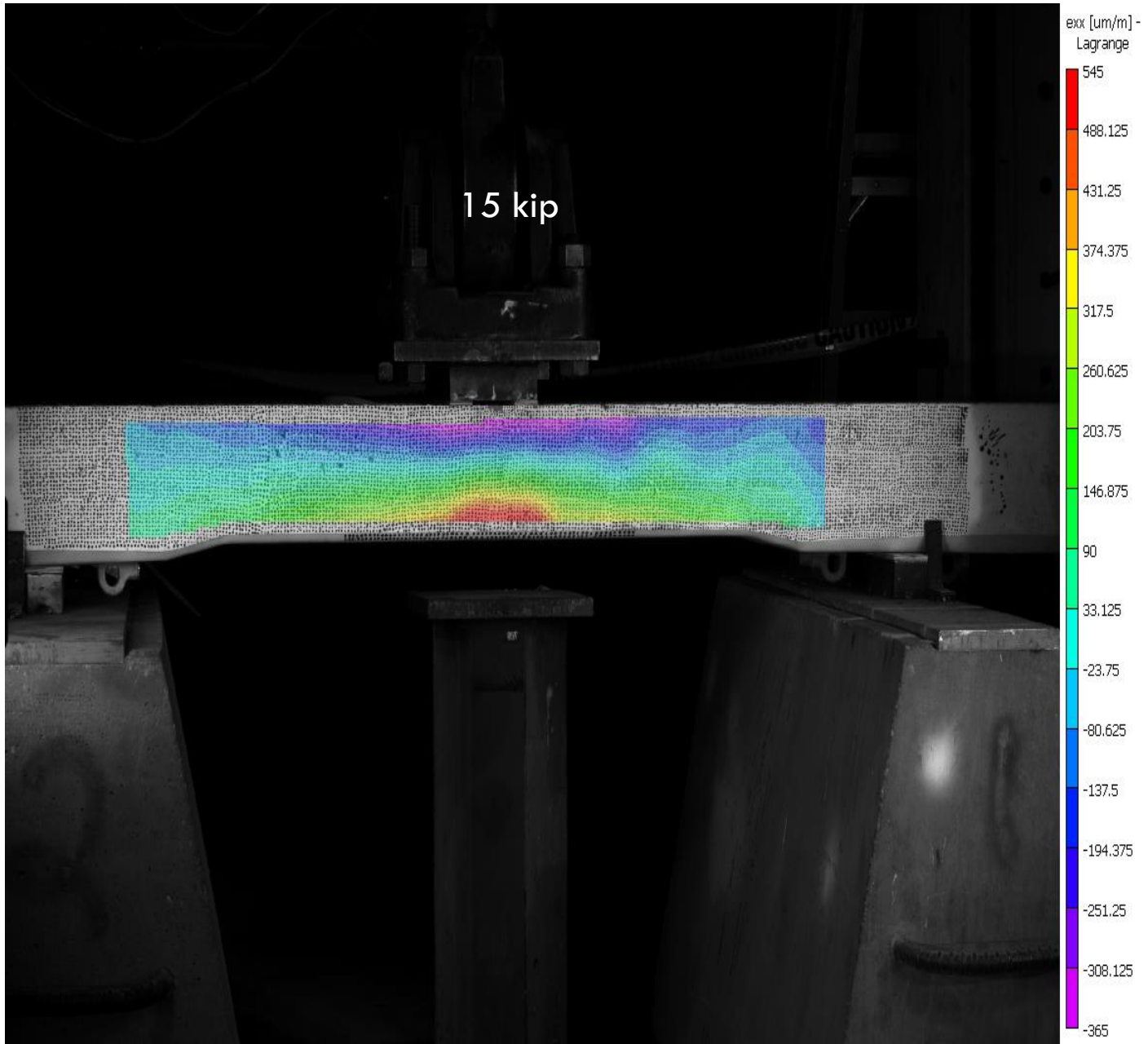


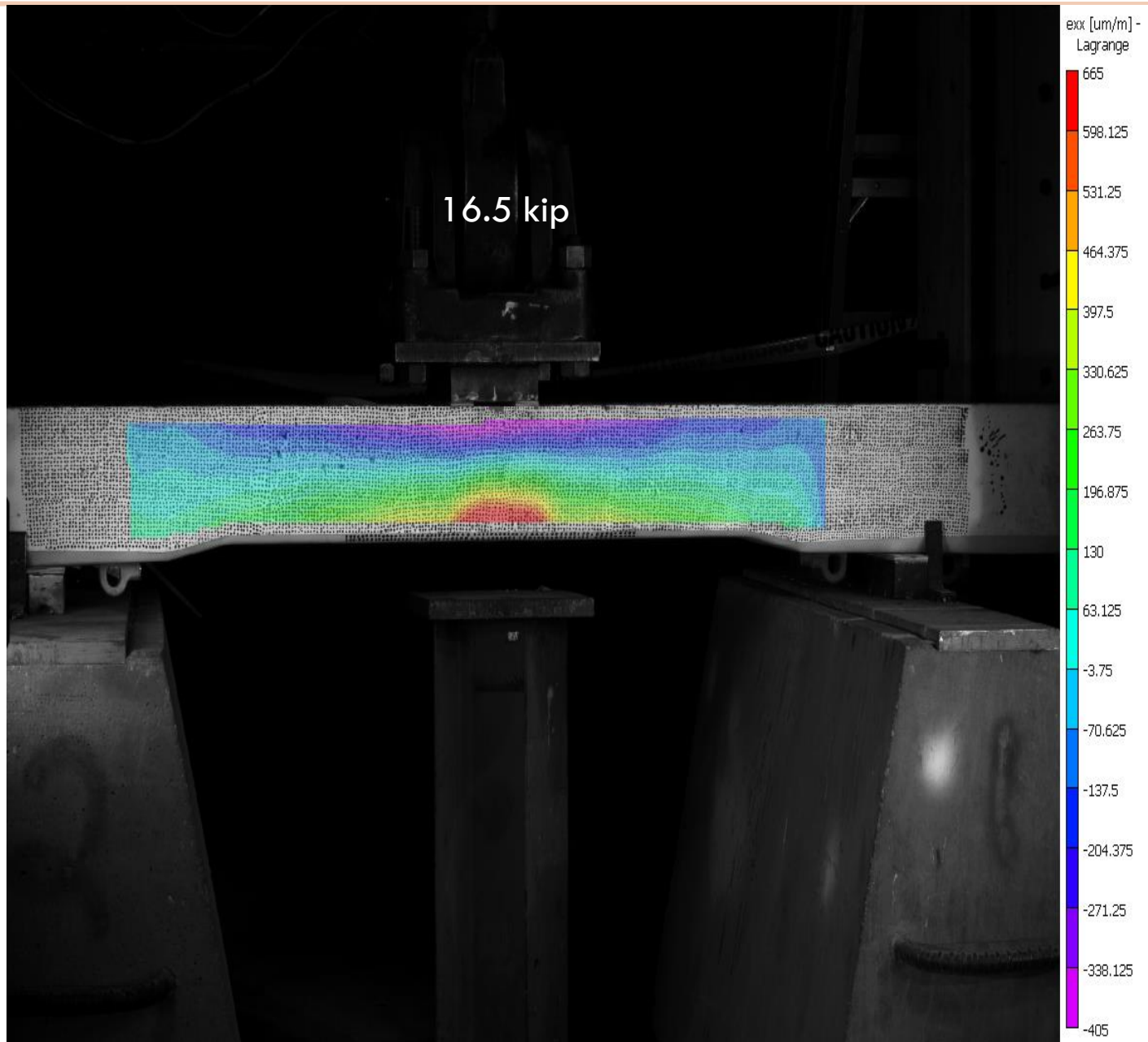


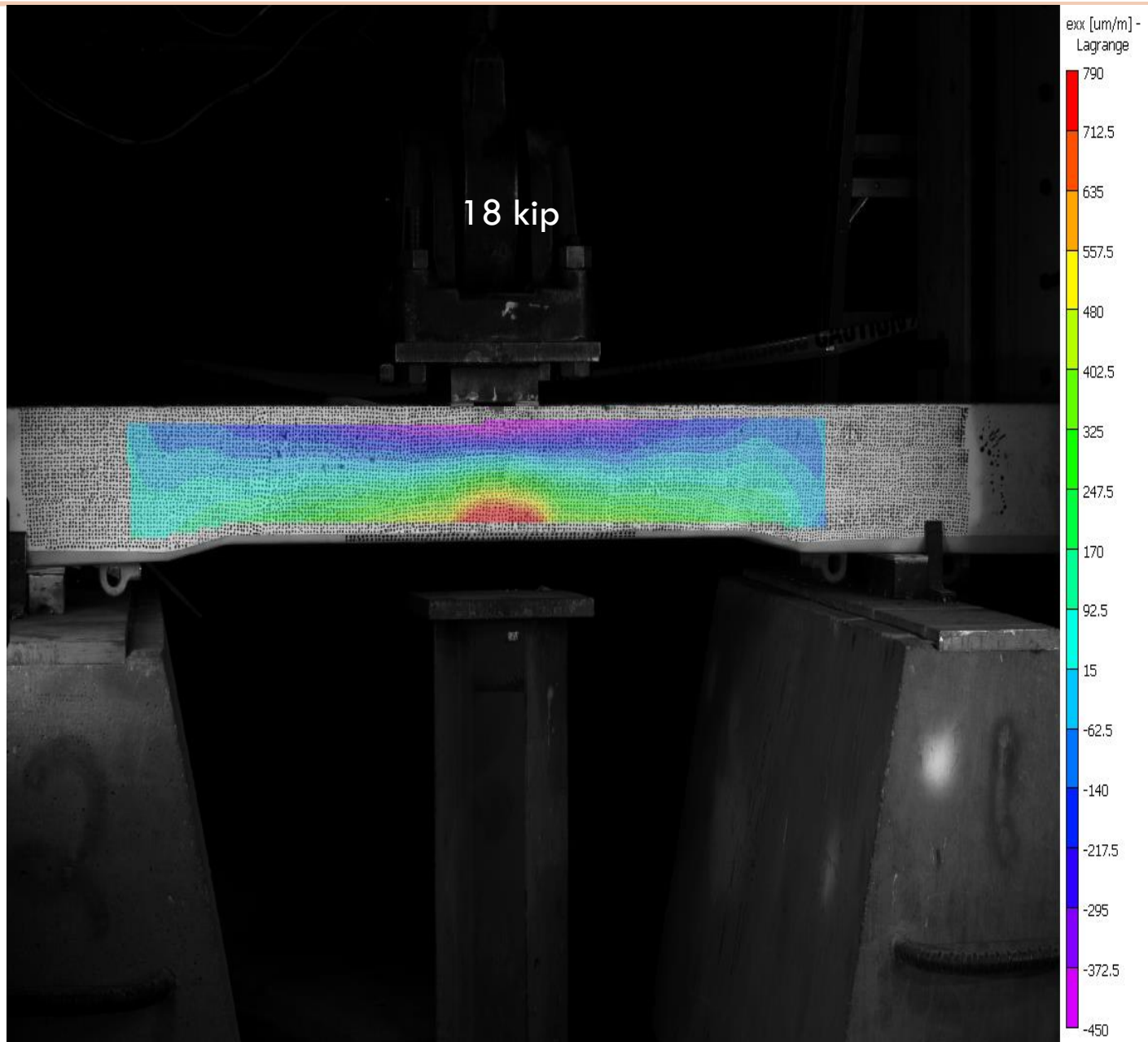


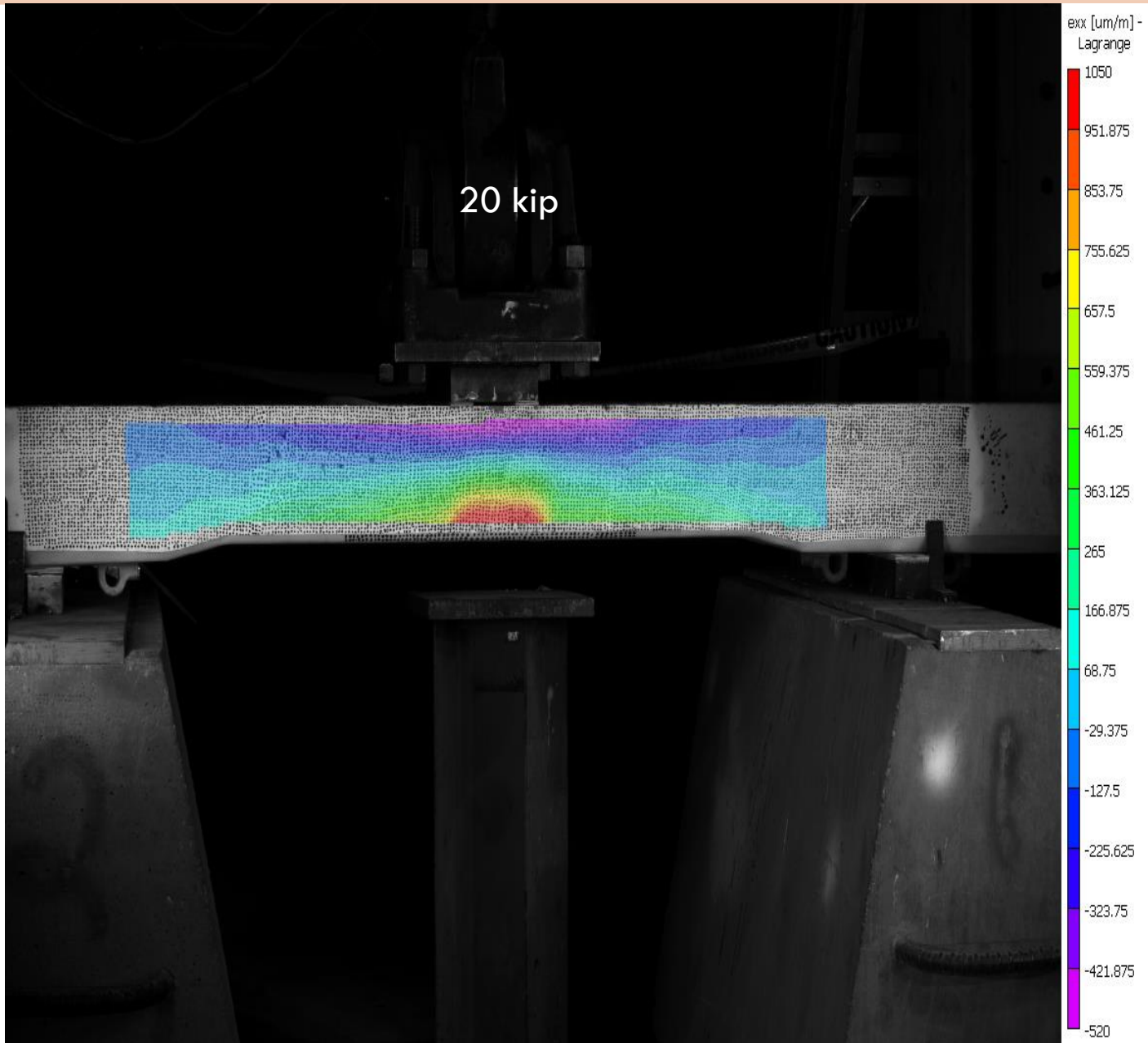


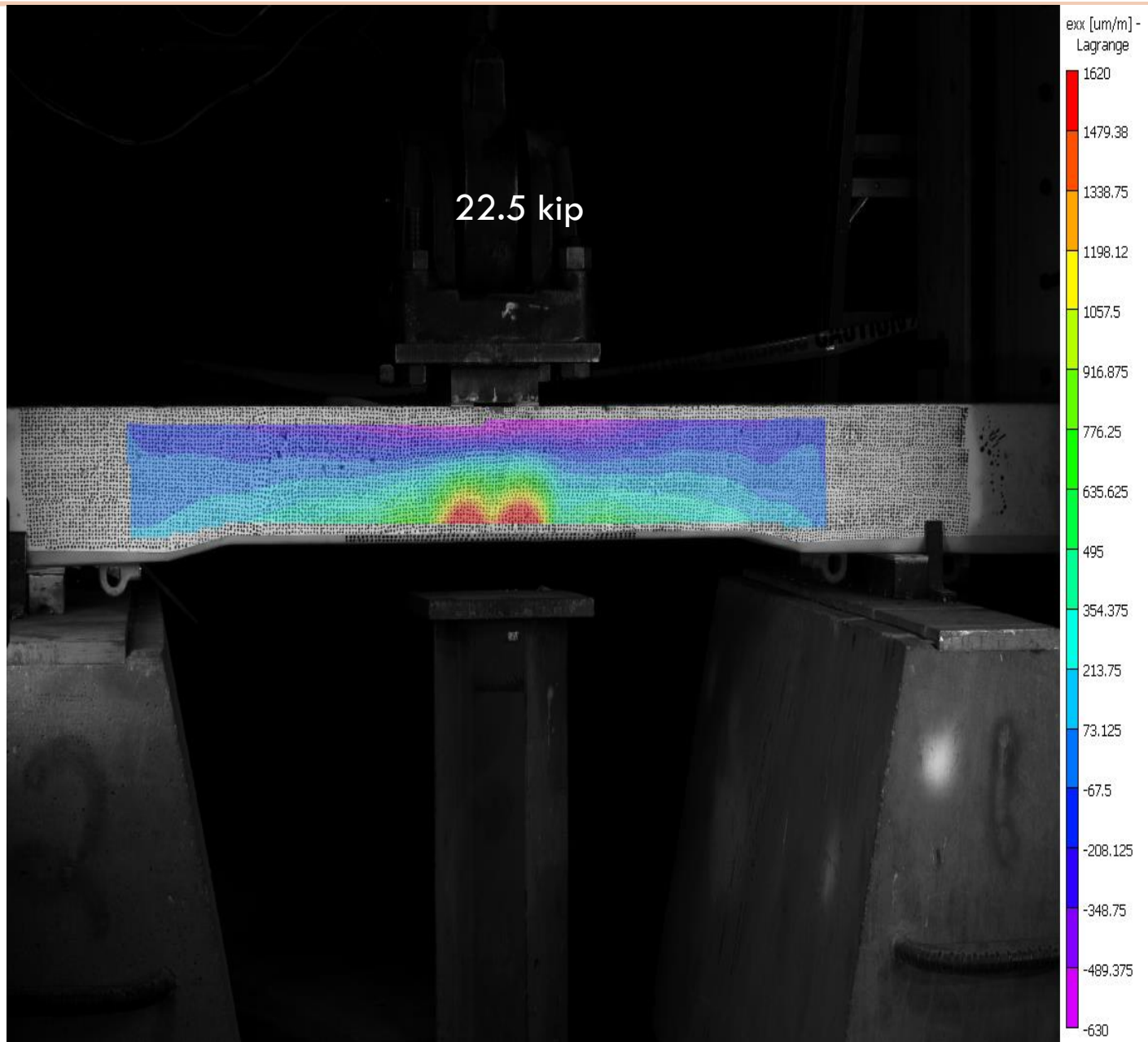


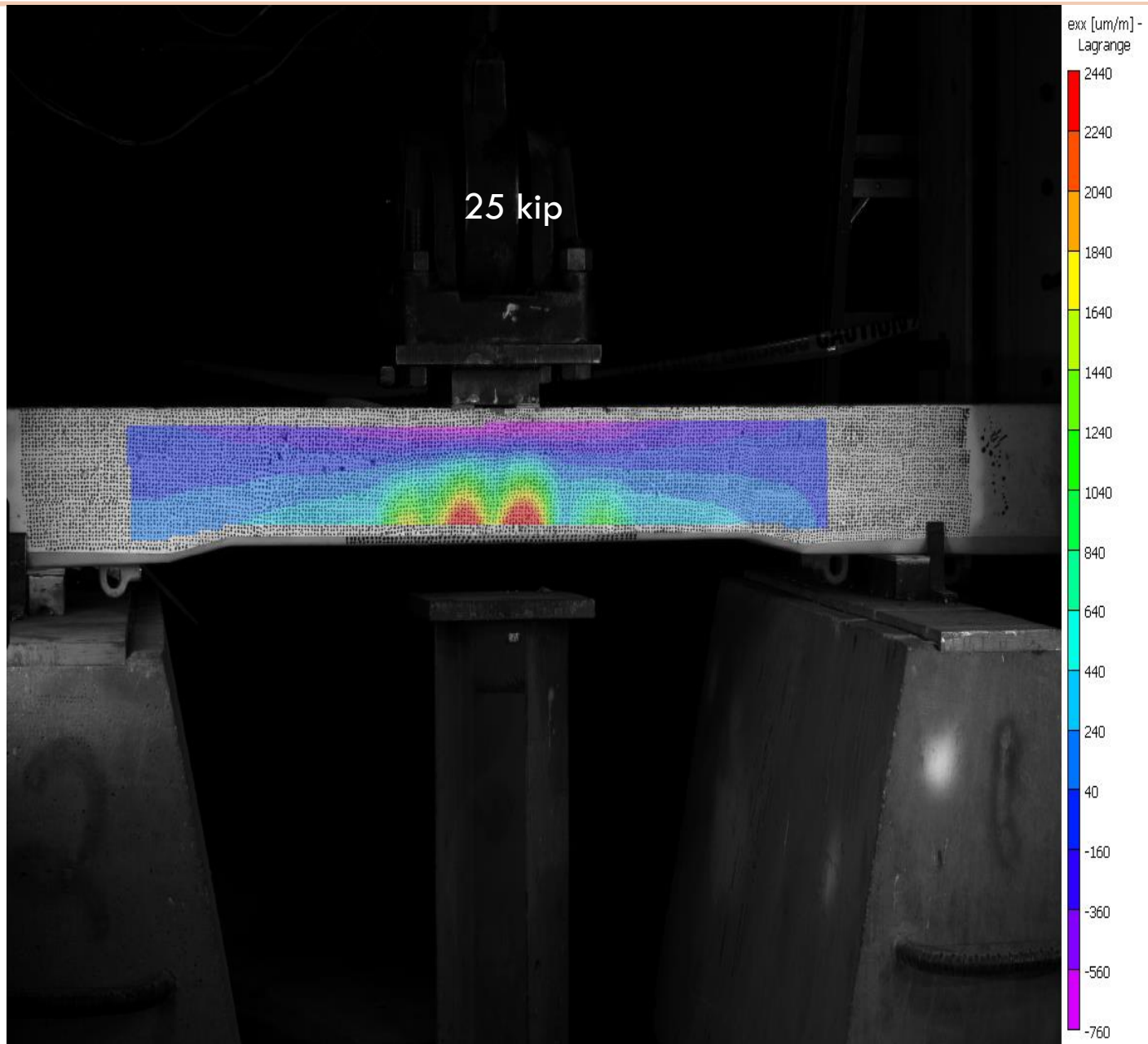


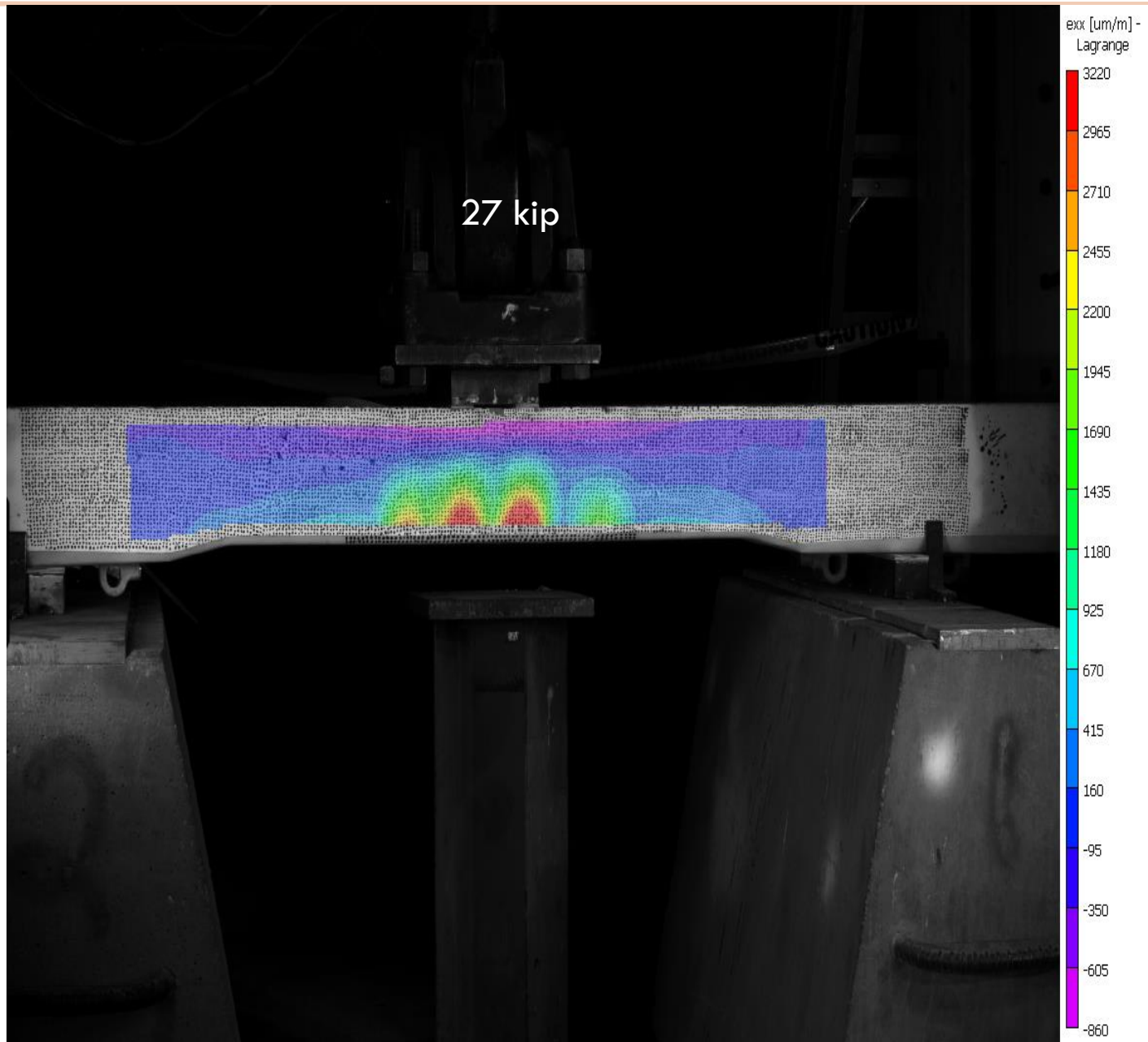


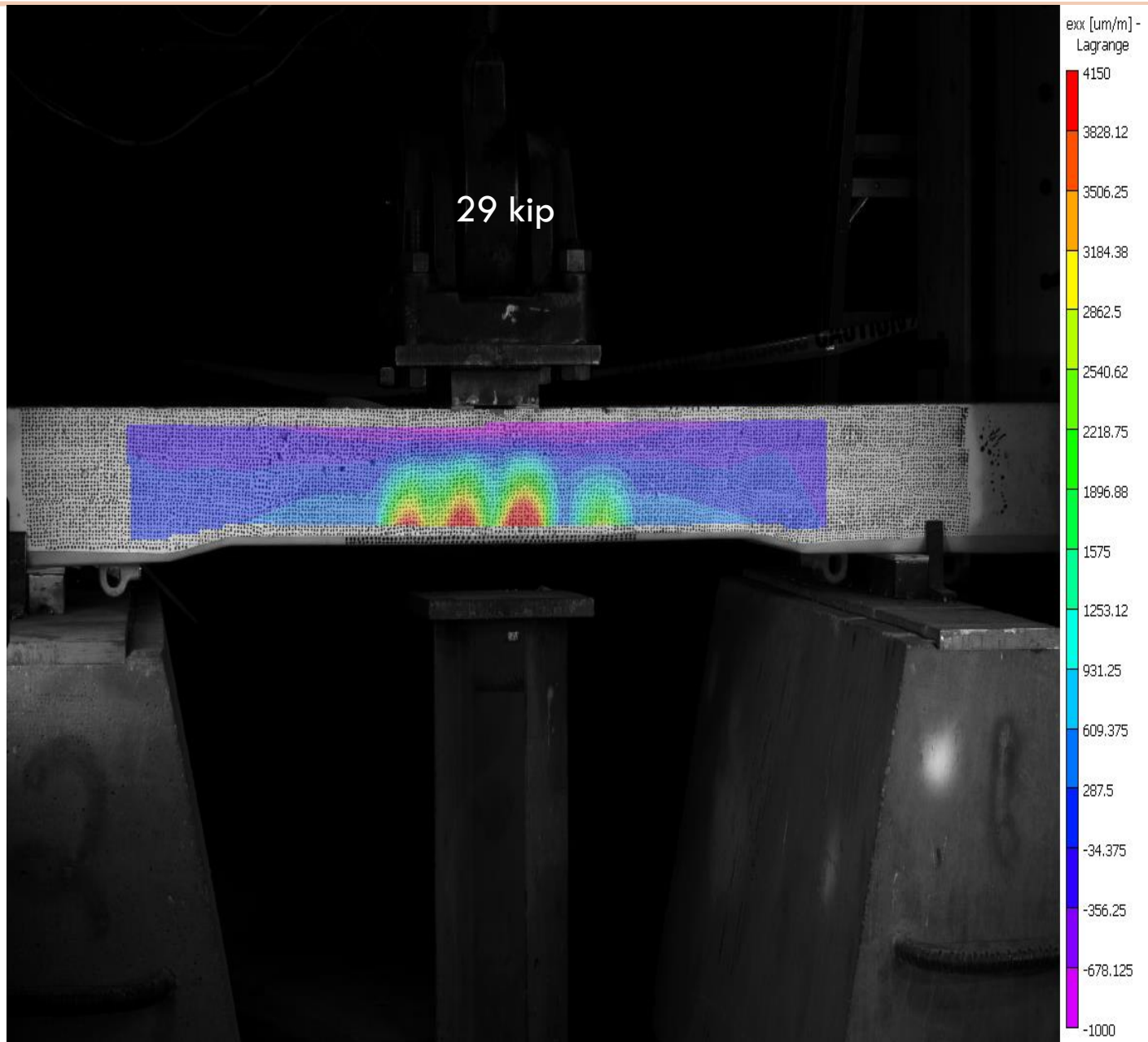


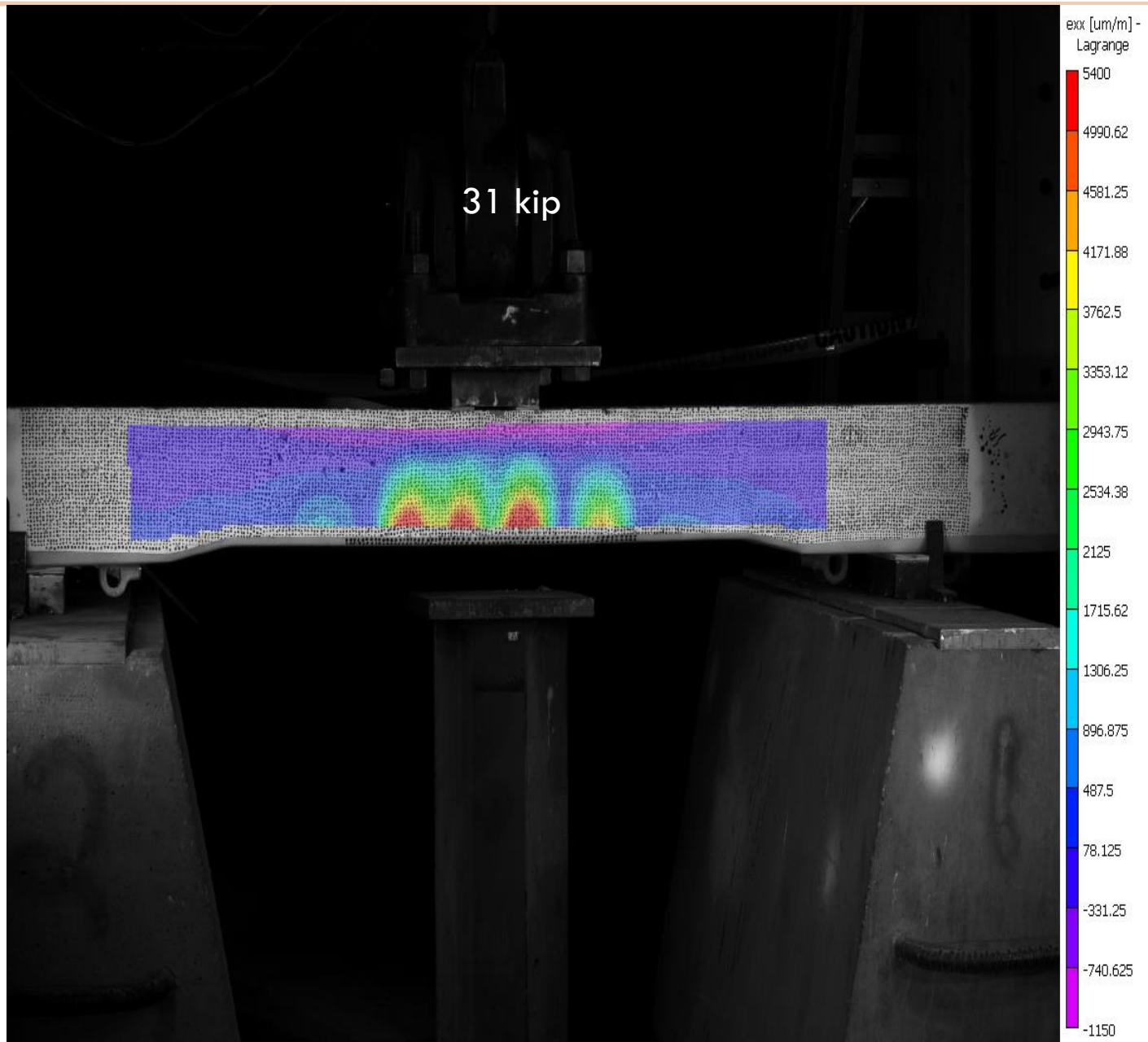


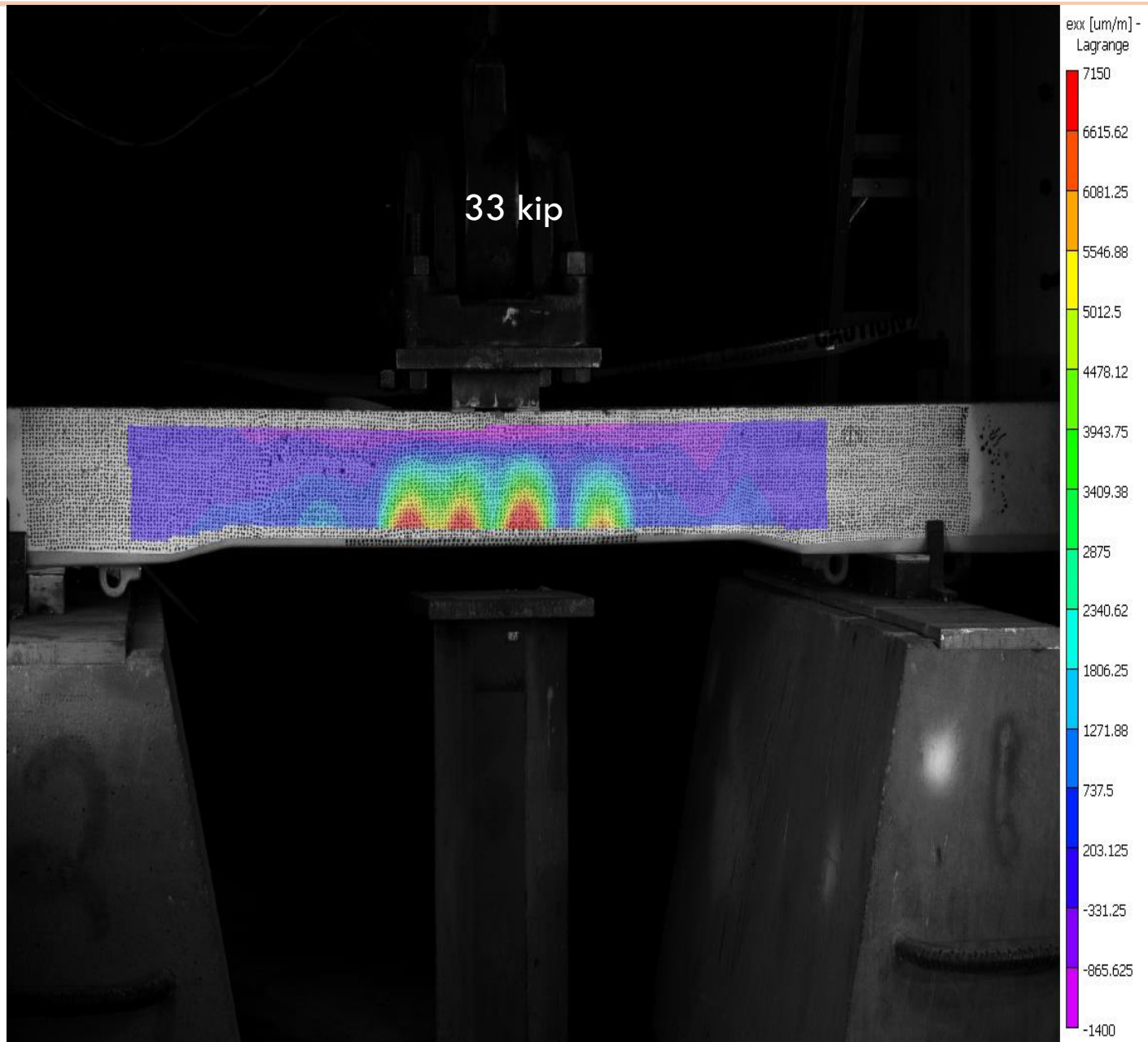


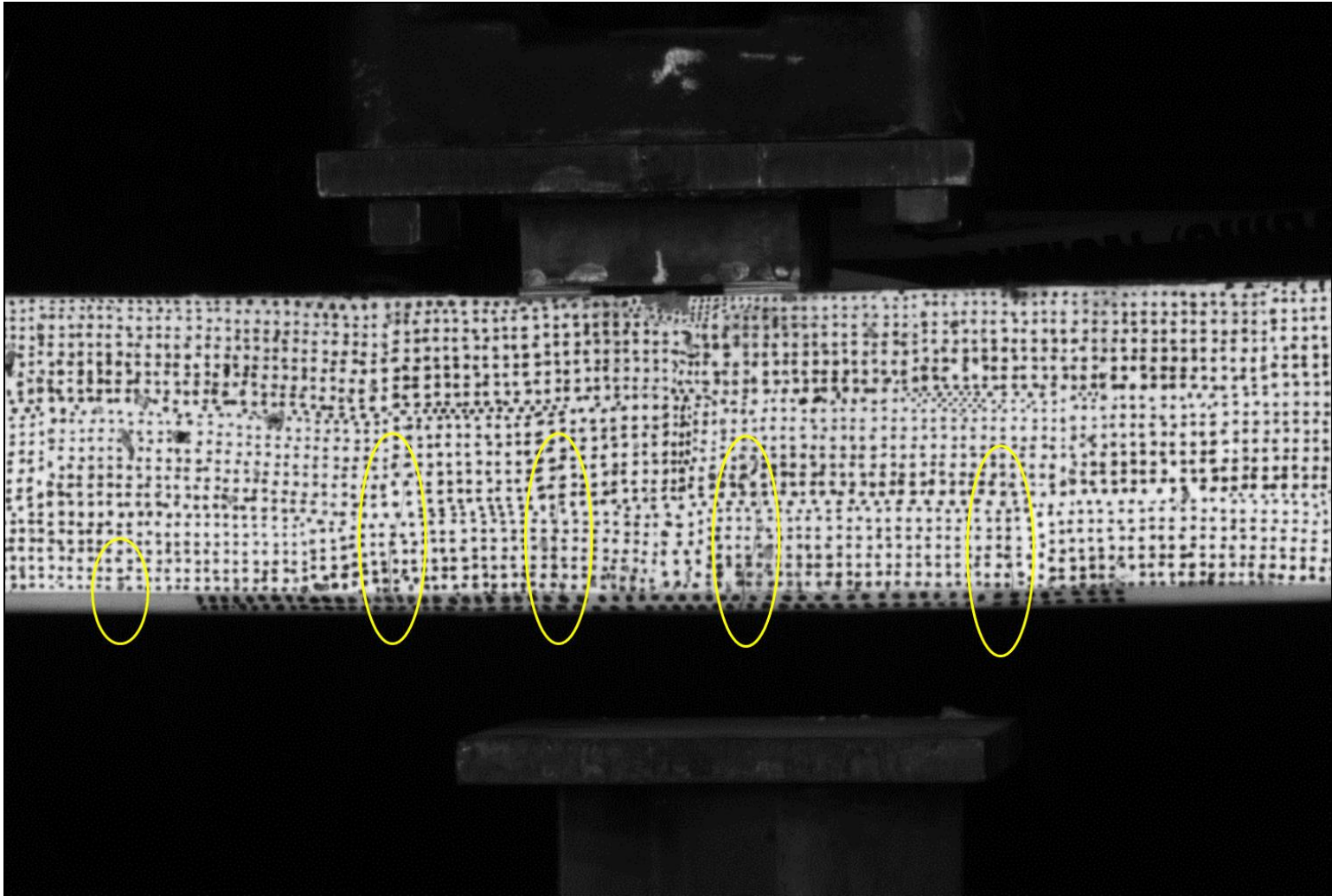






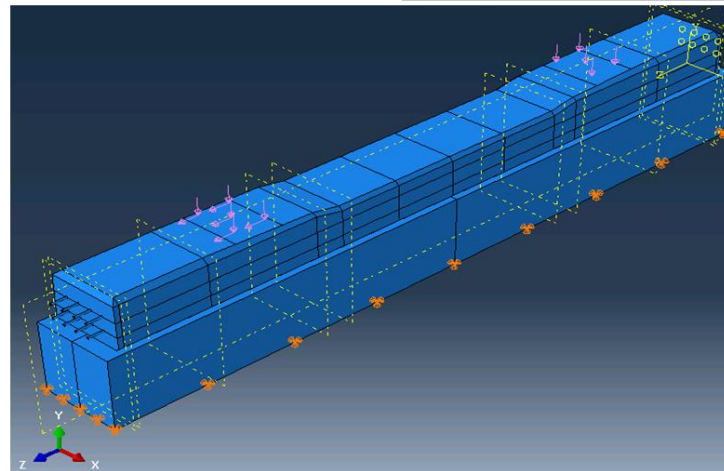
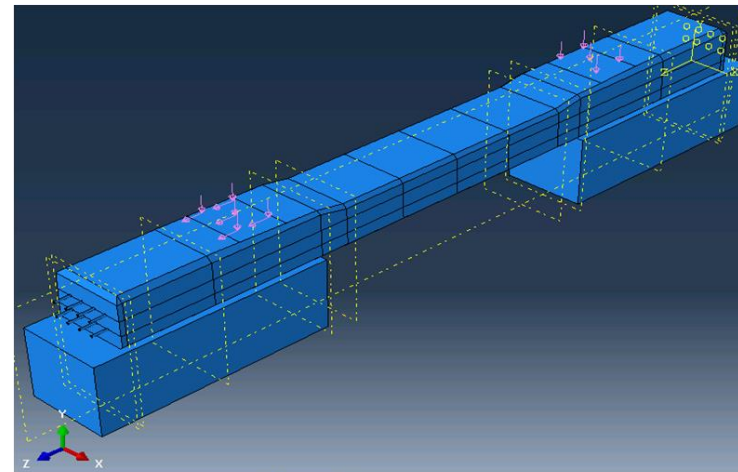
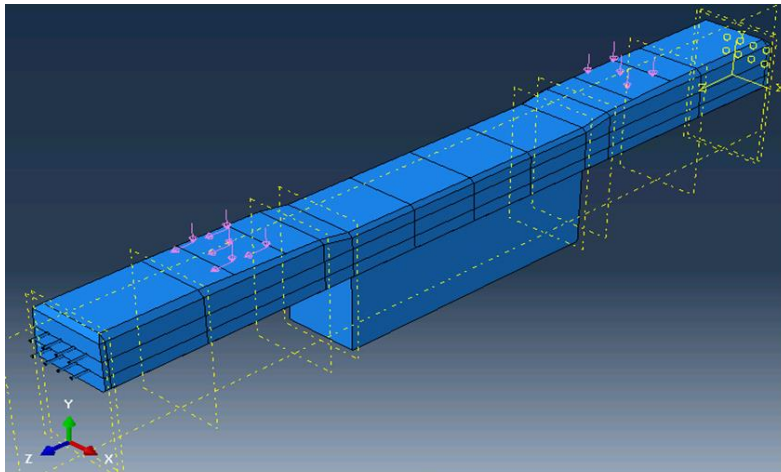






- ❑ HSRM Ultimate load 34kips (standard 30kips)
- ❑ Multiple shallow cracks indicate load redistribution in HSRM (fewer, deeper cracks in standard)

Parametric Studies— FEM Analysis



$L/V = 0.0, 0.2, 0.4$

Elastic Modulus Values Mpa (ksi)	
Standard	HSRM
31,918 (4,629)	23,018 (3,338)

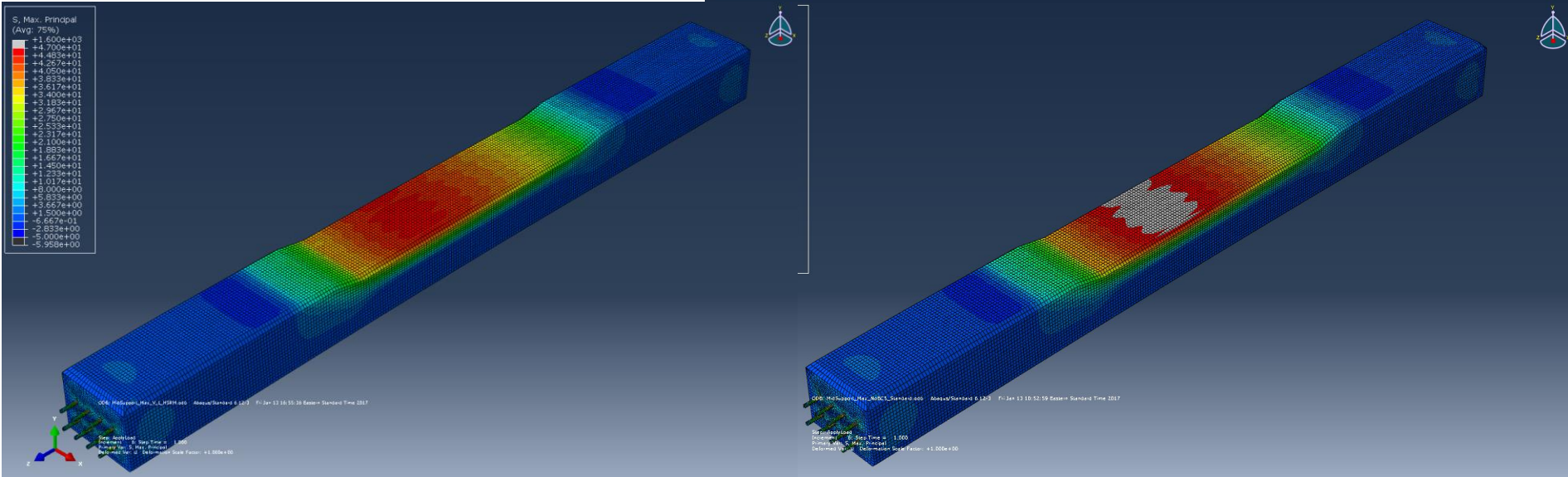
~27% reduction

Ballast: $E = 200 (29)$

Max Principle Stress – Example In Progress

HSRM

Standard



3%-12% stress reduction

- Maintains high strength**

- Smoother stress gradients in tie and stress redistribution after cracking**

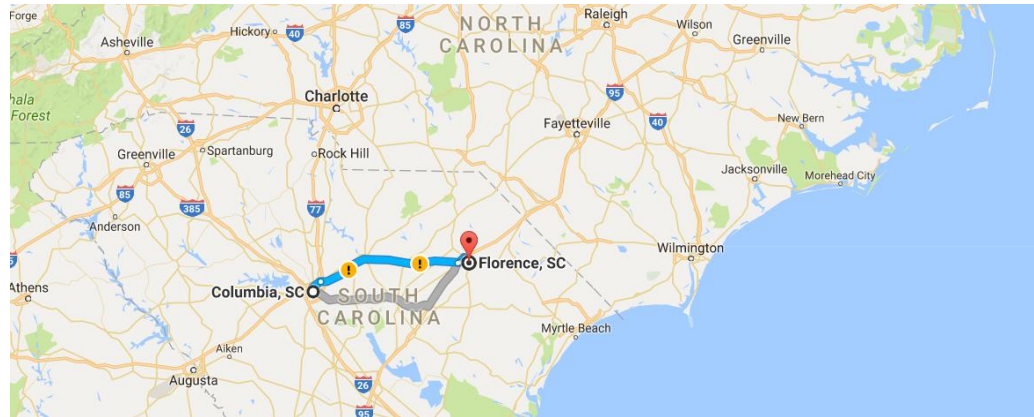
- Stress amplitude reduction**

- Onset of damage delayed**

- Better load distribution on track ?**

- ❑ Historical Background
- ❑ Hypothesis
- ❑ Material Development and Characterization
- ❑ Prototype Tie Design and Fabrication
- ❑ Product Qualification
- ❑ Benefits
- ❑ **Conclusions & Future Work**

- ❑ Residual Strength (Post Damage)
- ❑ Dynamic DIC measurements
- ❑ Effects on load distribution on track
- ❑ In situ testing and monitoring



- ❑ HSRM-HPC similar properties as Limestone HPC except Elastic Modulus (up to 50% reduction)
- ❑ HSRM Ties Passed all AREMA Qualification Tests and meets or exceeds standard tie performance
- ❑ A technology based modification in concrete tie technology that improves the safety of rail service and maintenance operations without impacting fabrication cost and process



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Thank You!



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