

Benefits of Adopting High-Strength High-Resilience Concrete in Prestressed Crossties

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On behalf of Dr. Dimitris C. Rizos
University of South Carolina



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Symposium**

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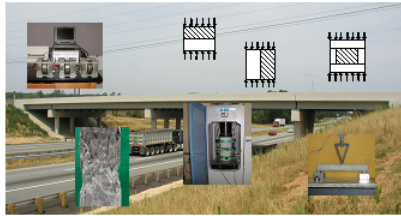
- Historical Background
- Hypothesis
- Material Development and Characterization
- Prototype Tie Design and Fabrication
- Product Qualification
- Conclusions

- **Historical Background**
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Permeability of Portland Cement Concrete (PCC) Structures in South Carolina –Volume II

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and
The Federal Highway Administration
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SCDOT Research Project

- HPC for Highway Bridges
- Local Aggregates
- SCDOT Mixture Designs



Historical Background

Table 2.1 Grades of Performance Characteristics for High Performance Structural Concrete (Goodspeed et al., 1996)

Performance Characteristic	Standard Test Method	FHWA HPC Performance Grade			
		1	2	3	4
Strength (x=compressive strength)	AASHTO T22 ASTM C39	$41 \leq x < 55$ MPa ($6 \leq x < 8$ ksi)	$55 \leq x < 69$ MPa ($8 \leq x < 10$ ksi)	$69 \leq x < 97$ MPa ($10 \leq x < 14$ ksi)	$x \geq 97$ MPa ($x \geq 14$ ksi)
Elasticity (x=modulus of elasticity)	ASTM C469	$28 \leq x < 40$ GPa ($4 \leq x < 6 \cdot 10^6$ psi)	$40 \leq x < 50$ GPa ($6 \leq x < 7.5 \cdot 10^6$ psi)	$x \geq 50$ GPa ($x \geq 7.5 \cdot 10^6$ psi)	
Shrinkage (x=microstrain)	ASTM C157	$800 > x \geq 600$	$600 > x \geq 400$	$400 > x$	
Creep (x=microstrain/pressure unit)	ASTM C512	$75 \geq x \geq 60$ /MPa ($0.52 \geq x \geq 0.41$ /psi)	$60 \geq x > 45$ /MPa ($0.41 \geq x > 0.31$ /psi)	$45 \geq x > 30$ /MPa ($0.31 \geq x > 0.21$ /psi)	$30/\text{MPa} \leq x$ ($0.21/\text{psi} \leq x$)
Freeze-thaw durability (x=relative dynamic modulus of elasticity at 300 cycles)	AASHTO T161 ASTM C666 (Procedure A)	$60\% \leq x < 80\%$	$80\% \leq x$		
Scaling (x= visual rating of the surface after 50 cycles)	ASTM C672	$x=4,5$	$x=2,3$	$x=0,1$	
Abrasion (x= average depth of wear)	ASTM C944	$2.0 > x > 1.0$ mm ($0.08 > x > 0.04$ in.)	$1.0 > x \geq 0.5$ mm ($0.04 > x > 0.02$ in.)	$x < 0.5$ mm ($x < 0.02$ in.)	
Chloride Penetration (x=Coulombs)	AASHTO T277 ASTM C1202	$3000 \geq x > 2000$	$2000 \geq x > 800$	$800 \geq x$	



Historical Background

- Aggregates from specific quarries
- HPC Classified as Grade 1 or 2 based on most properties
- Did not meet Grade based on Elastic Modulus
- HPC Rejected

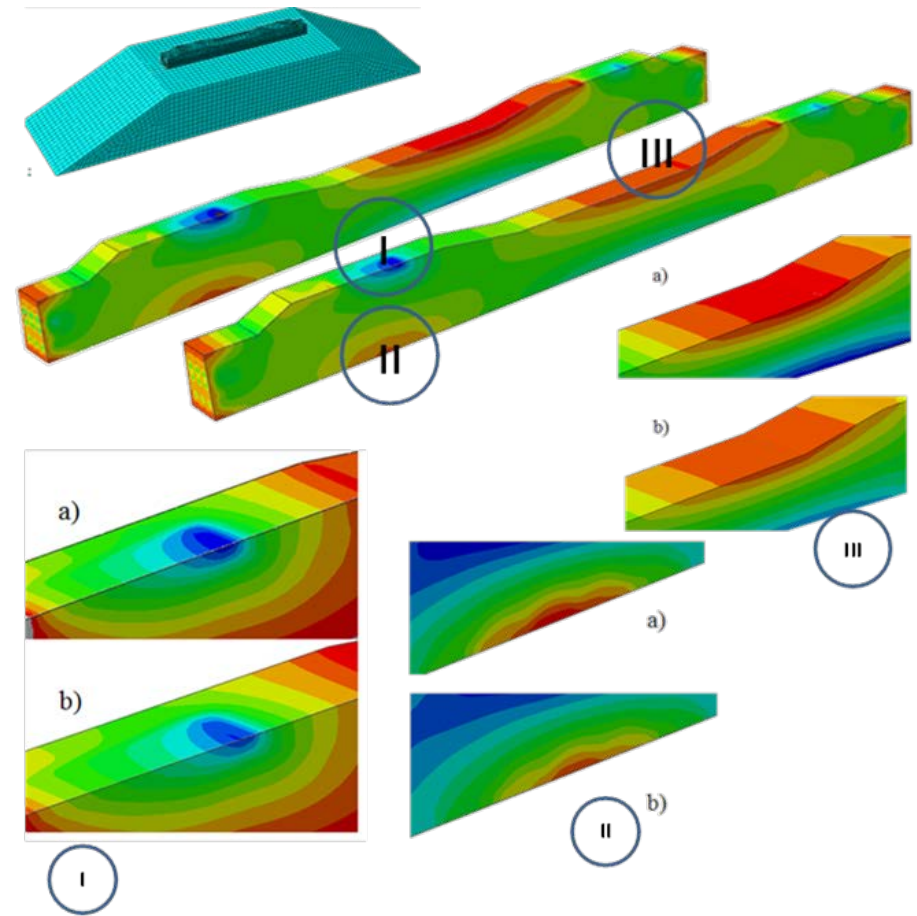
Performance Characteristic	Standard Test Method	Batch No.	Experimental Results	FH\ Perform. Grade
Strength (MPa (psi))	ASTM C39	1	47.5 (6890)	1
		2	51.9 (7525)	1
		3	55.2 (8003)	2
		4	57.6 (8360)	2
Elasticity (GPa (ksi))	ASTM C469	1	21.3 (3089)	< 1
		2	19.4 (2811)	< 1
		3	24.1 (3492)	< 1
		4	24.1 (3501)	< 1
Shrinkage (microstrain)	ASTM C157	Shrinkage tests were not performed		
Creep (microstrain/pressure unit)	ASTM C512	Creep tests were not performed.		
Freeze-thaw durability (relative dynamic modulus of elasticity at 300 cycles, %)	ASTM C666 (Procedure A)	1	---	---
		2	---	---
		3	---	---
		4	>90	2
Scaling (visual rating of the surface after 50 cycles)	ASTM C672	1	4	1
		2	3	2
		3	---	---
		4	---	---
Abrasion (average depth of wear, mm (in.))	ASTM C944	1	1.410 (0.0555)	1
		2	1.711 (0.0674)	1
		3	---	---
		4	---	---
Sulfate Penetration (Coulombs)	ASTM C1202	1	2144	1
		2	2632	1
		3	2683	1
		4	1065	2

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Benefits of Using Higher Resilience Concrete in Prestressed Ties:

- Better load distribution
- Smoother stress gradient
- Lower stress amplitudes
- Delay of onset of damage
- Relative rigidity

Critical Location	Stress Reduction due to HSRM-HPC [%]
I	15%
II	50%
III	48%



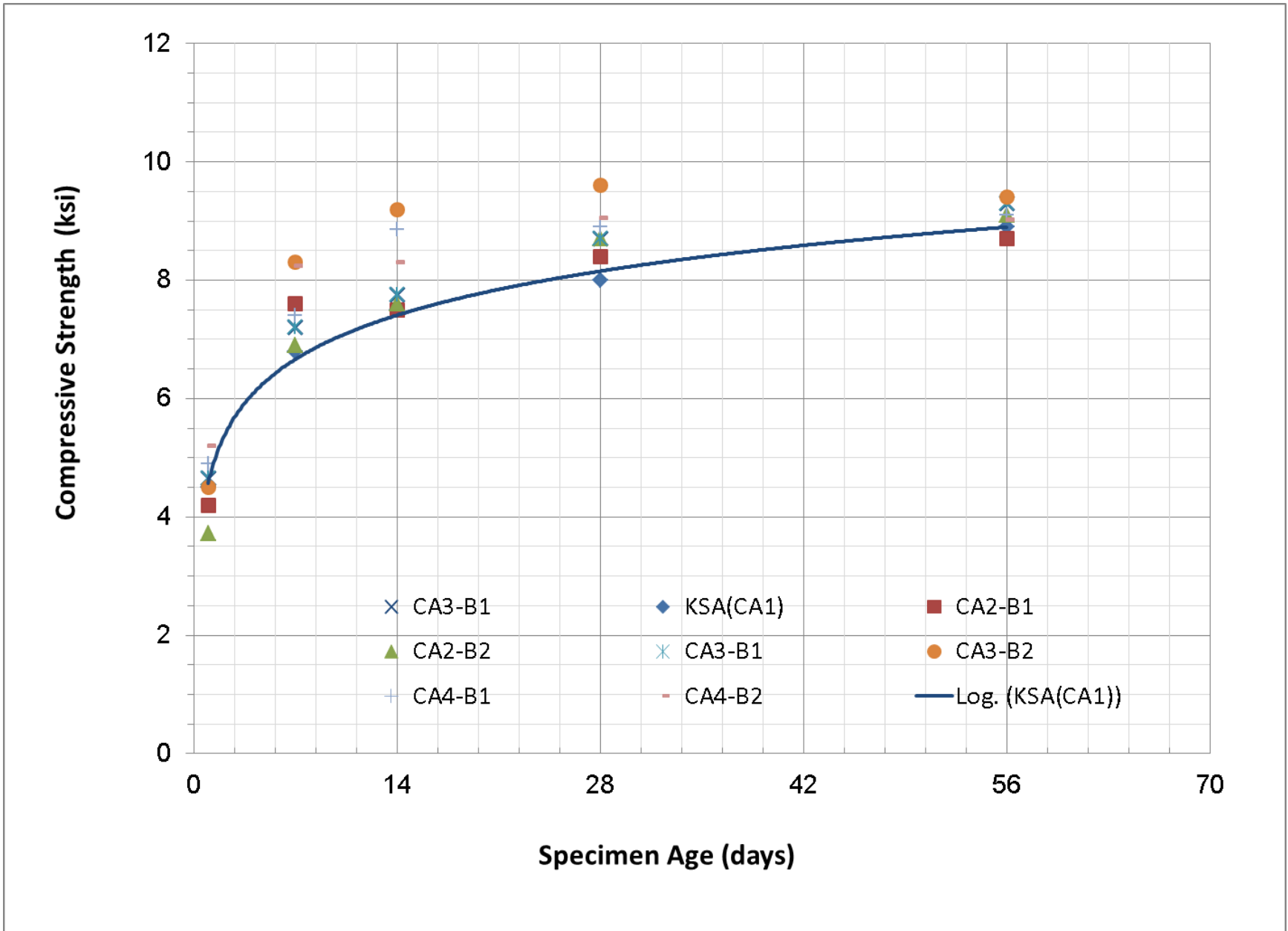
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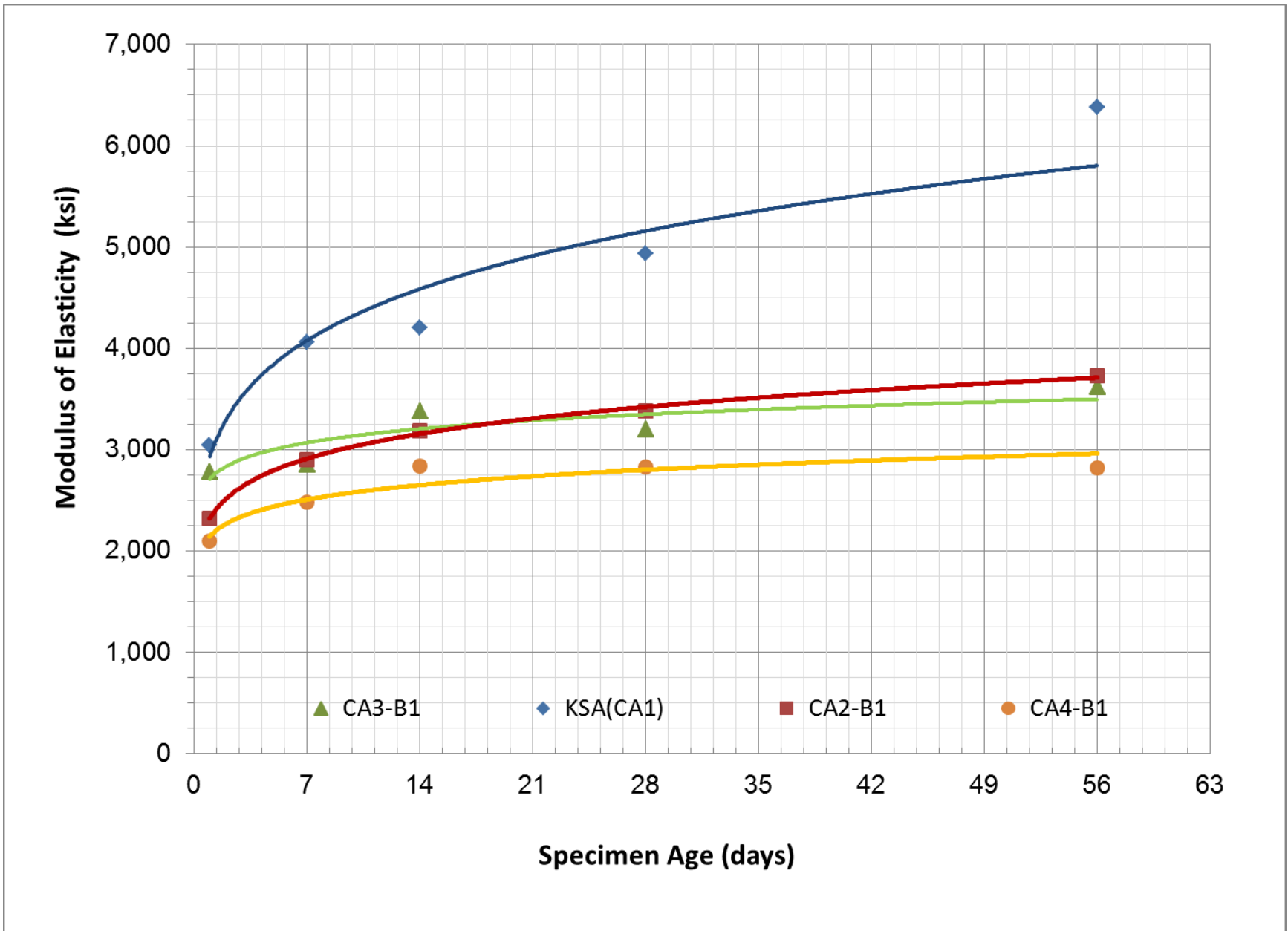
- ▶ **Rocla Design**
 - ▶ Min. 28 Day = 7000psi
 - ▶ Min. Transfer Strength = 4000psi
- ▶ **Direct substitution of aggregates**
- ▶ **4 Aggregate Sources**
 - ▶ CA1: Plum Run Stone (ROCLA)
 - ▶ CA2: Weathered Granite Source A
 - ▶ CA3: Weathered Granite Source B
 - ▶ CA4: Weathered Granite Source C

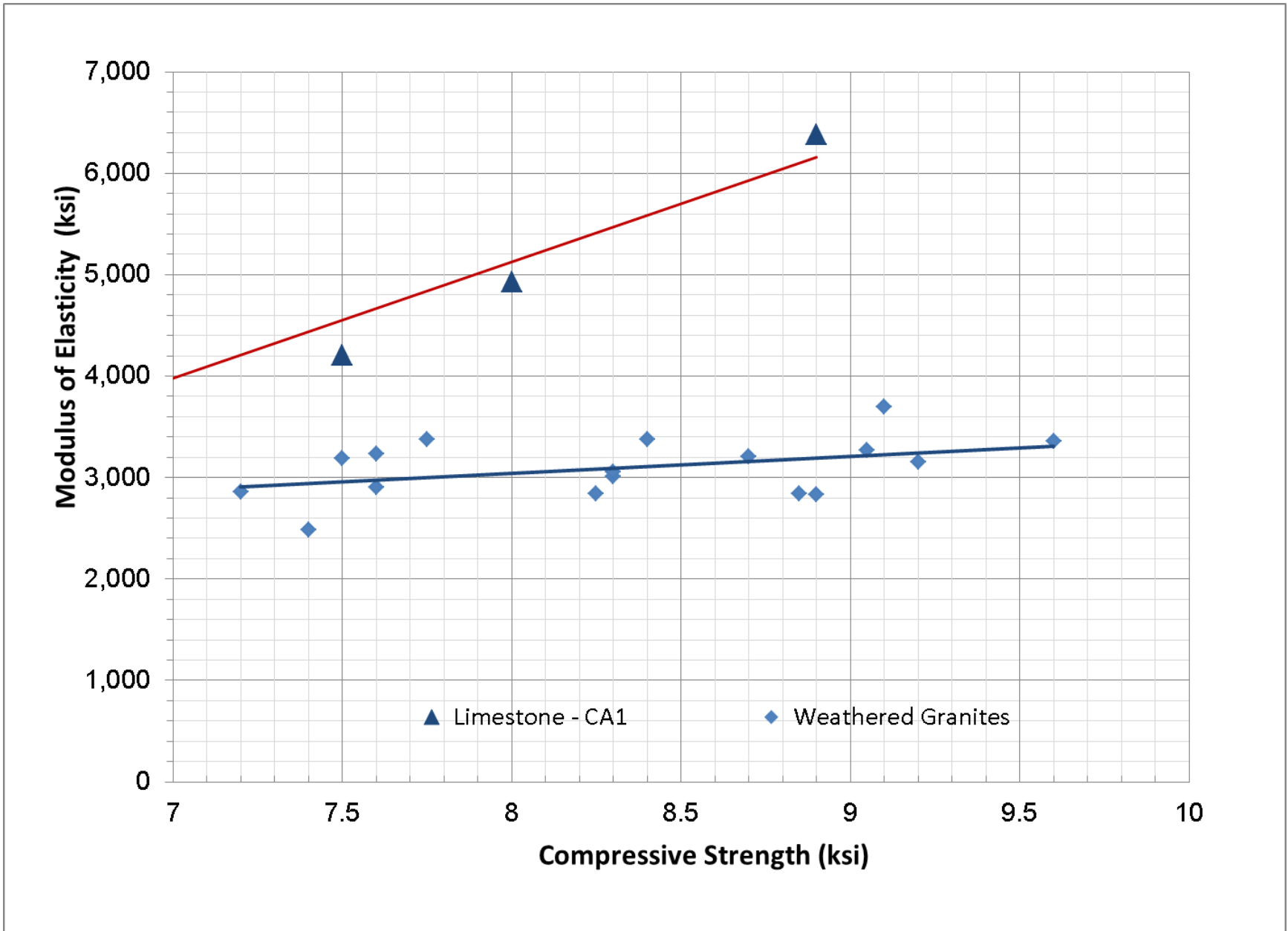




Test		ASTM
Coarse Ag.	Los Angles Abrasion Test	C131
	Sieve Analysis (Particle Size Distribution)	C136
	Bulk Density and Voids	C29
	Density, Specific Gravity and Absorption	C127
Rock	Compressive Strength	D7012 - 14
	Modulus of Elasticity	D7012 - 14
Concrete	Slump	C143
	Density	C138
	Air Content by pressure method	C231
	Compressive Strength of Concrete	C39
	Flexural Strength of Concrete	C78
	Modulus of Elasticity of Concrete	C469
	Shrinkage	C157
Mortar	Compressive Strength	C 109- 13
	Tensile Strength	C 307-12
	Modulus of Elasticity	C 580-02
	Setting Time (Initial and Final)	C191 - 13









Properties Comparison

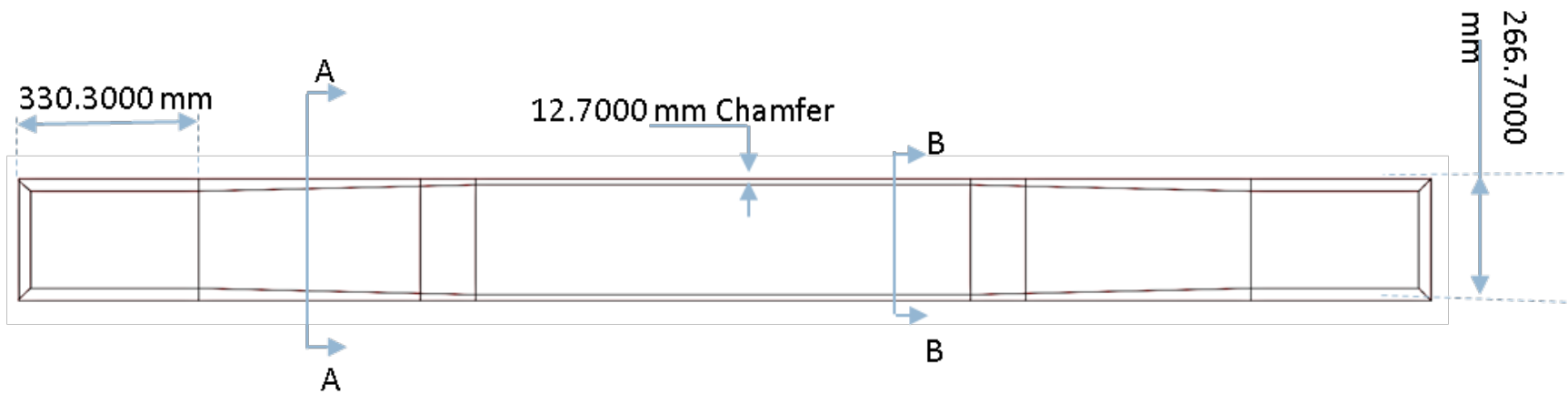
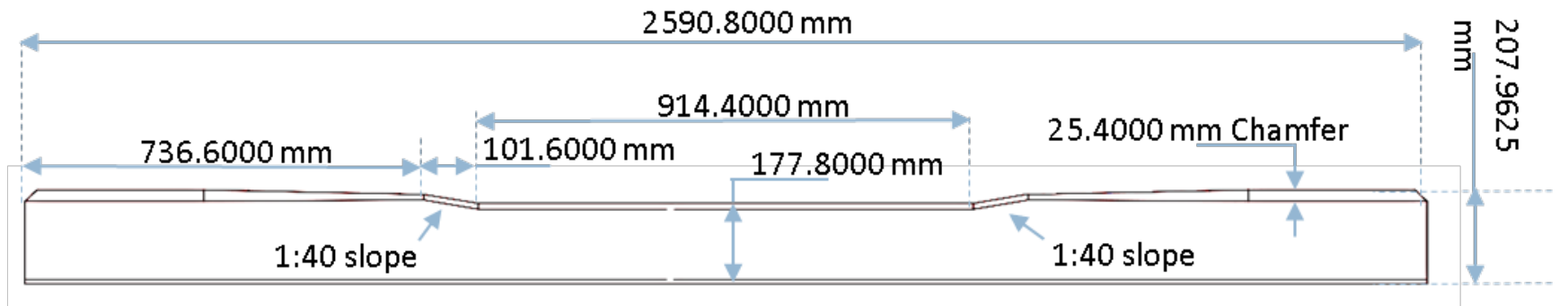
Property		AGGREGATE			
		KSA (CA1)	CA2	CA3	CA4
Aggreg	Voids	42.73	42.51	39.90	39.10
	Density (lb/ft ³)	161.65	164.50	165.00	167.50
	Relative Density	2.58	2.60	2.65	2.69
	LA Abrasion	27.5%	33.9%	44.3%	46.0%
Fresh Concr	Density (lb/ft ³)	152.90	153.73	154.14	158.55
	Yield (yd ³)	0.15	0.15	0.14	0.14
	Cement Content (lb/yd ³)	618.23	621.53	623.21	632.05
	Slump (in)	7.00	6.50	7.50	4.00
	Air Content (%)	5.0%	5.9%	4.8%	4.0%
Concrete	Compressive Strength (psi)	8.8E+03	8.8E+03	9.2E+03	8.7E+03
	<i>Increase/Reduction %</i>	0%	0%	4%	-1%
	Flexural Strength (psi)	0.13fc'	0.125fc'	0.12fc'	-
	Elastic Modulus (psi)	5.6E+06	3.6E+06	3.2+06	2.8E+06
	<i>Elastic Modulus Reduction %</i>	0%	-37%	-43%	-50%
	Lapping Test Abrasion Rate (mm/min)	0.042	0.023	0.029	0.039

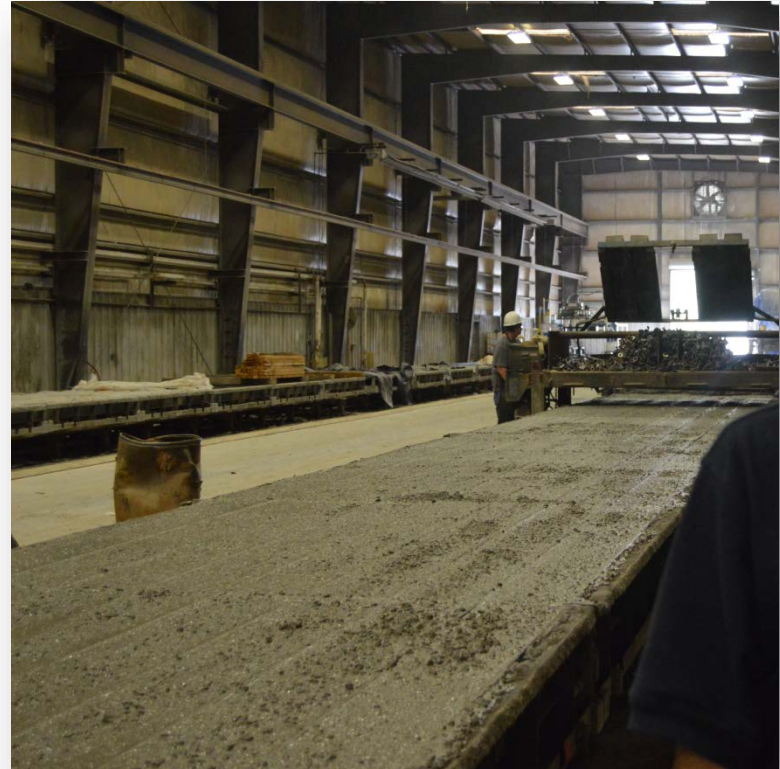


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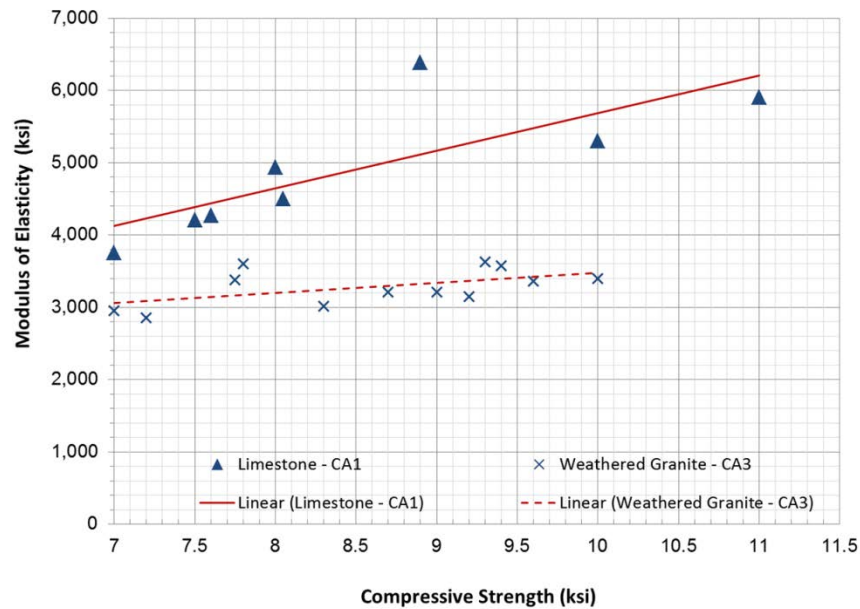
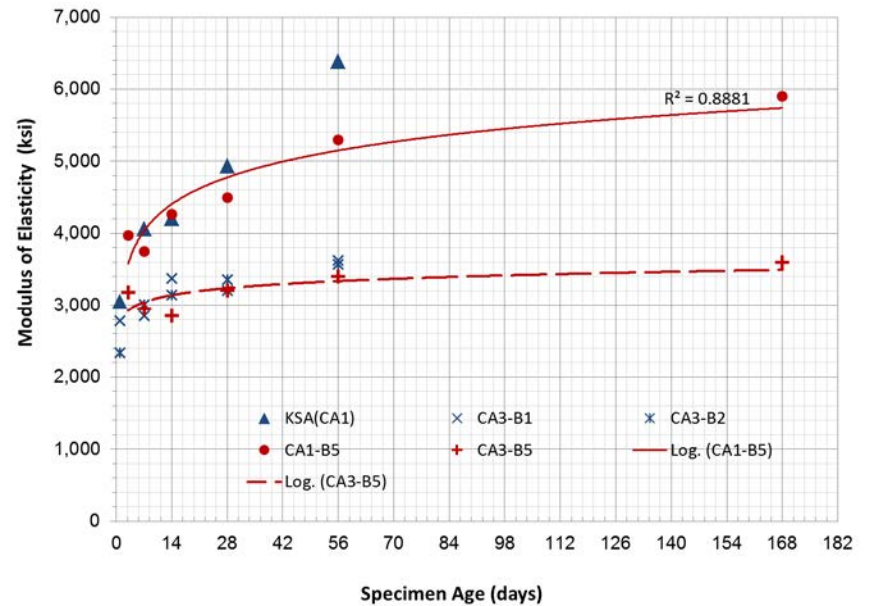
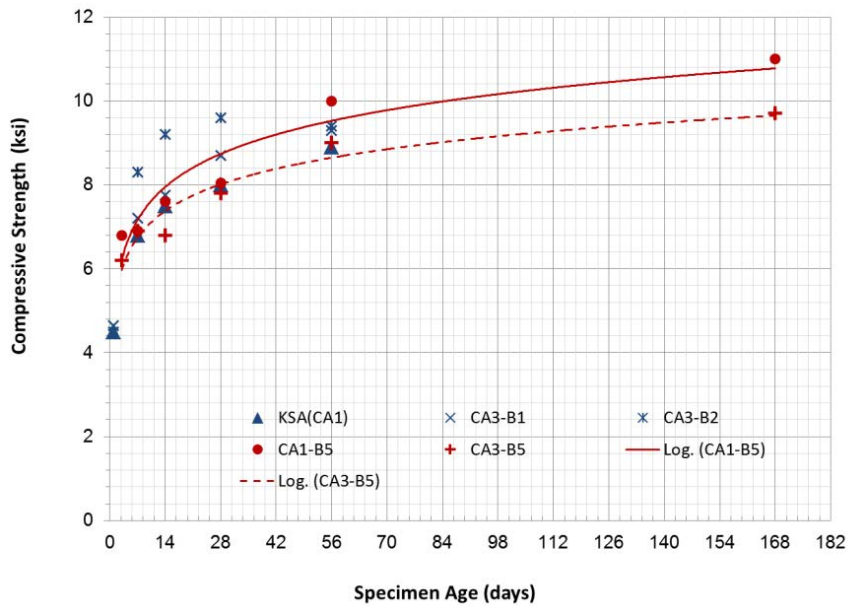








Concrete Properties – Plant Batch

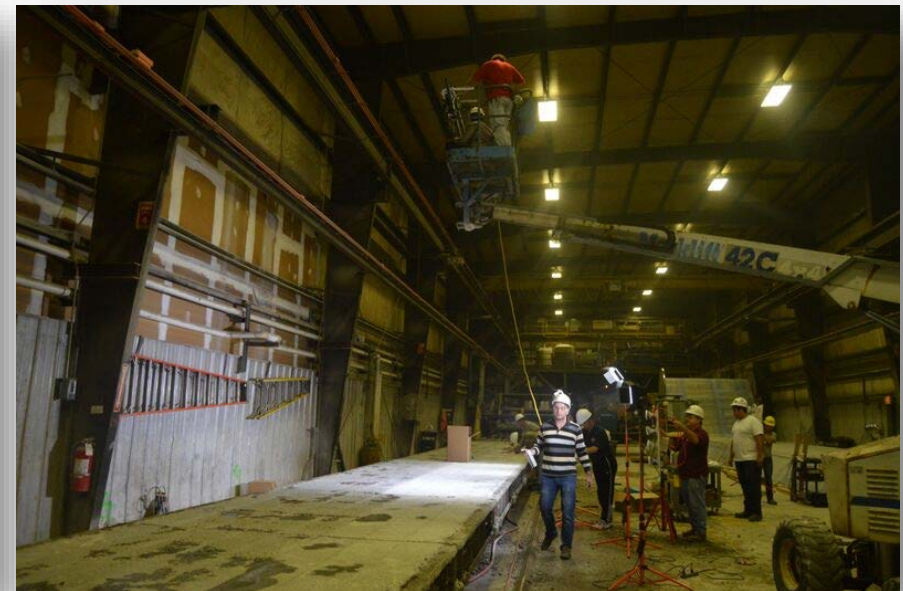




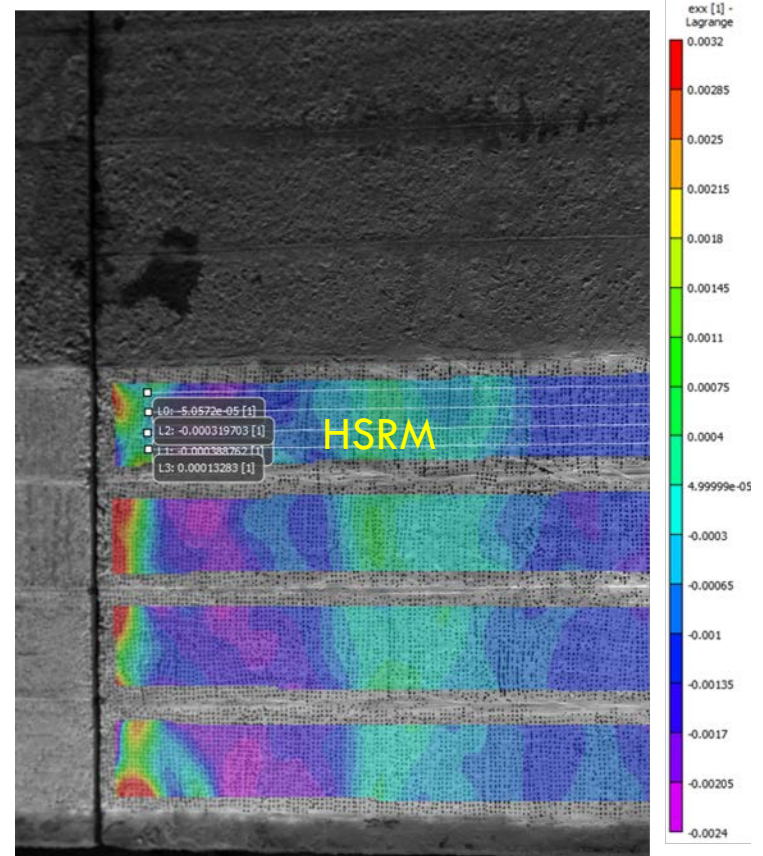
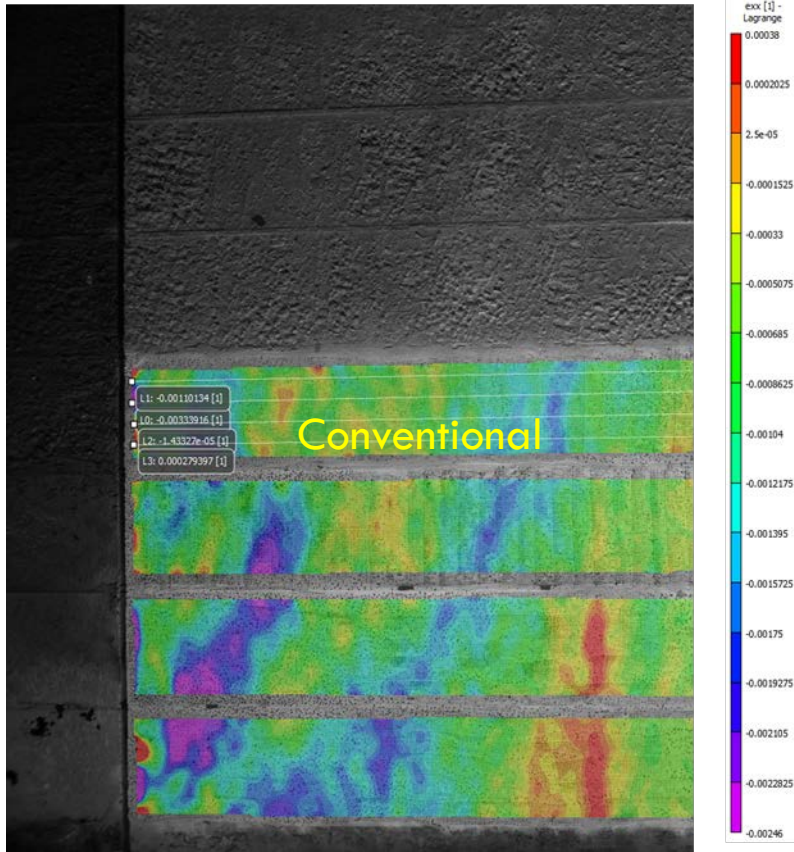
Transfer Length	HSRM-HPC	Standard
Average	11.9 in	16.2 in
Std. Deviation	1.0 in	2.5 in
Coeff. Var.	8.4%	15.4%



Prototype Fabrication: 9/26







- Historical Background
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4.9.1.1 Sequence of Design Tests (Tie “1”)

Completed

- a. Rail Seat Vertical Load Test - Rail seat A (4.9.1.4)
- b. Center Negative Bending Moment Test (4.9.1.6)
- c. Center Positive Bending Moment Test (4.9.1.7)
- d. Rail Seat Vertical Load Test – Rail seat B (4.9.1.4)
- e. Bond Development, Tendon Anchorage, and Ultimate Load Test – Rail seat A (4.9.1.8)

In Progress

- a. Rail Seat Repeated Load Test – Rail seat B(4.9.1.5)

4.9.1.2 Sequence of Design Tests (Tie “2”)

Completed

- a. Fastening Insert Test (4.9.1.9)
- b. Fastening Uplift Test (4.9.1.10)
- c. Electrical Resistance and Impedance Test (4.9.1.14)

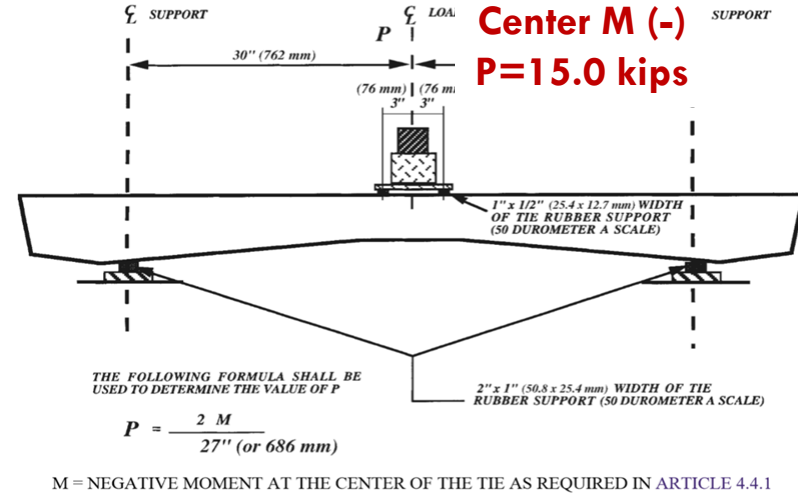
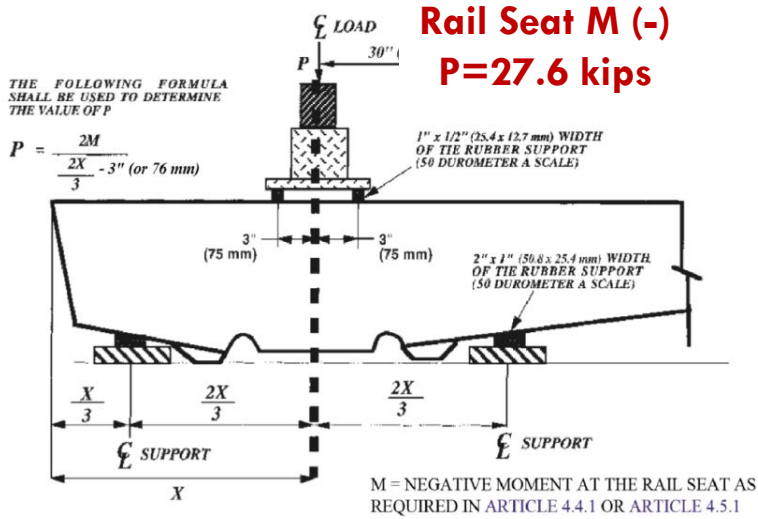


Figure 30-4-10. Tie Center Negative Moment Test

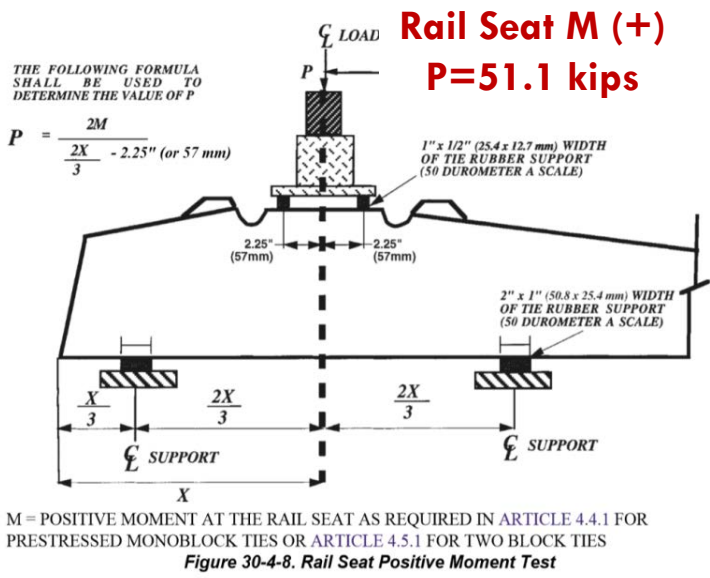


Figure 30-4-8. Rail Seat Positive Moment Test

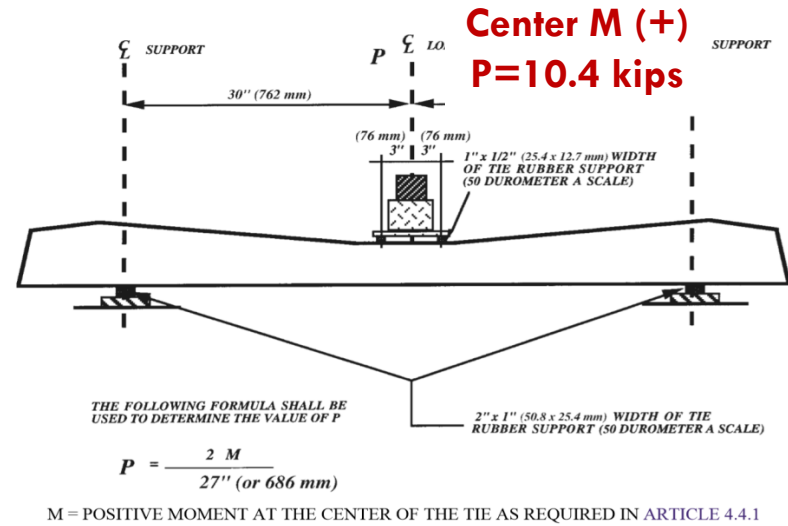
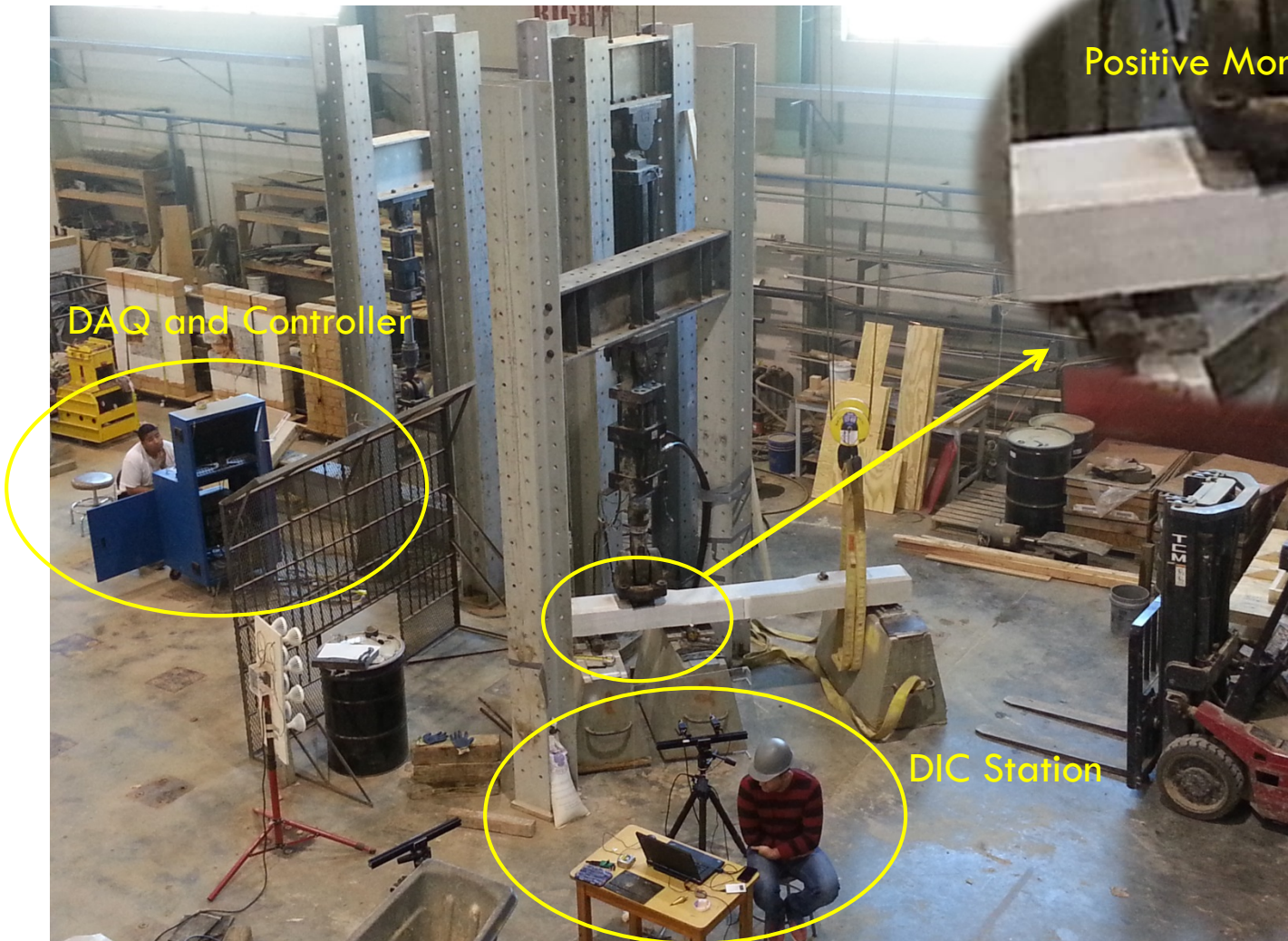


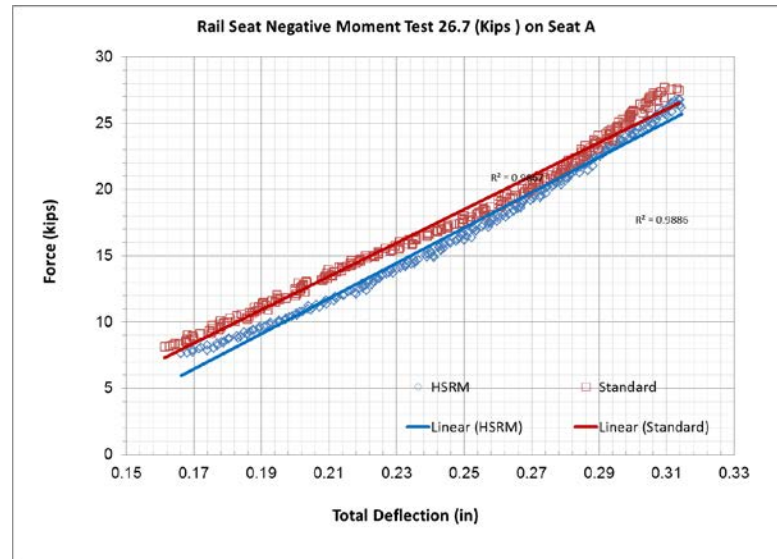
Figure 30-4-11. Tie Center Positive Moment Test



AREMA Sequence of Design Tests (Tie "1")

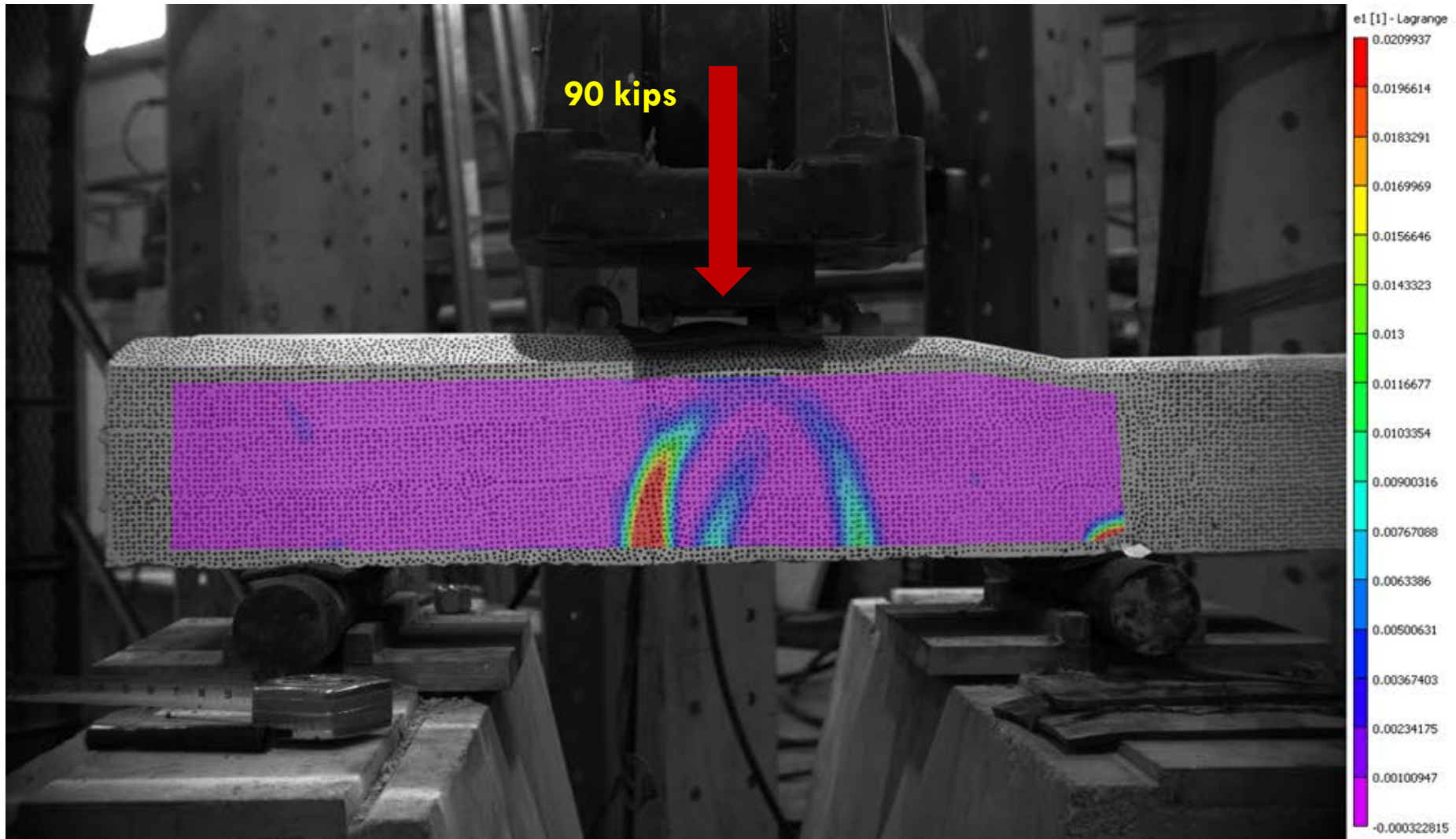


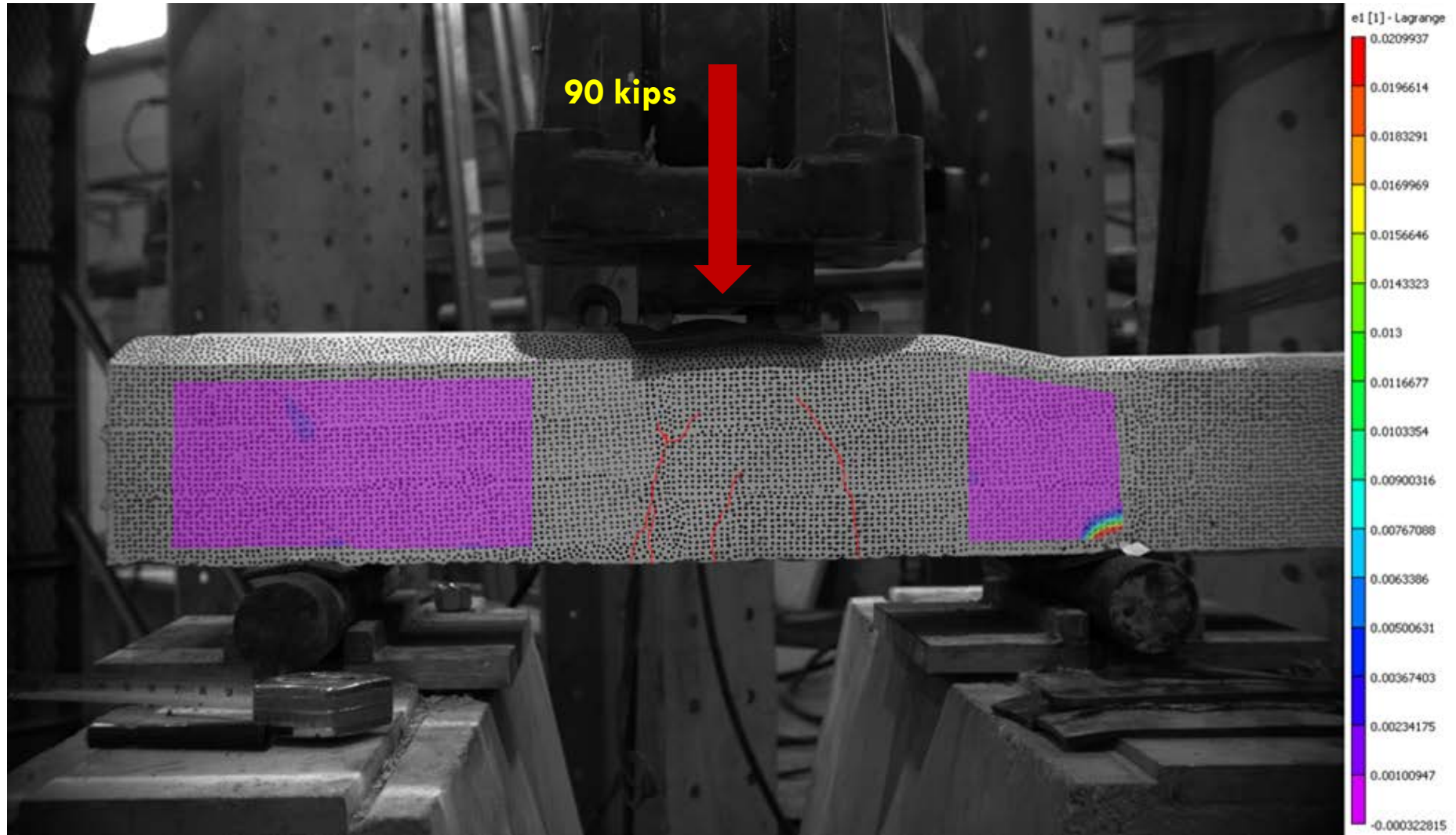






Design Performance – AREMA: Ultimate Load Tests (In Progress)



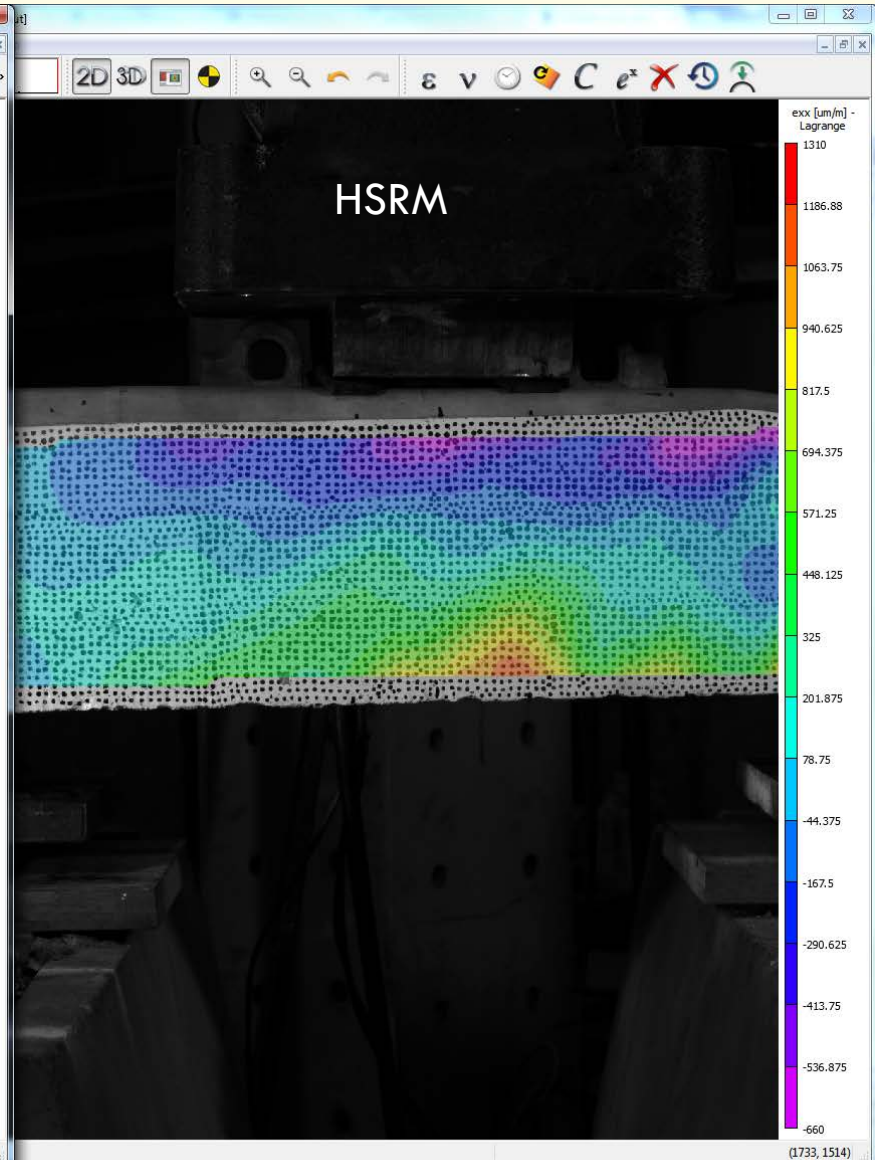
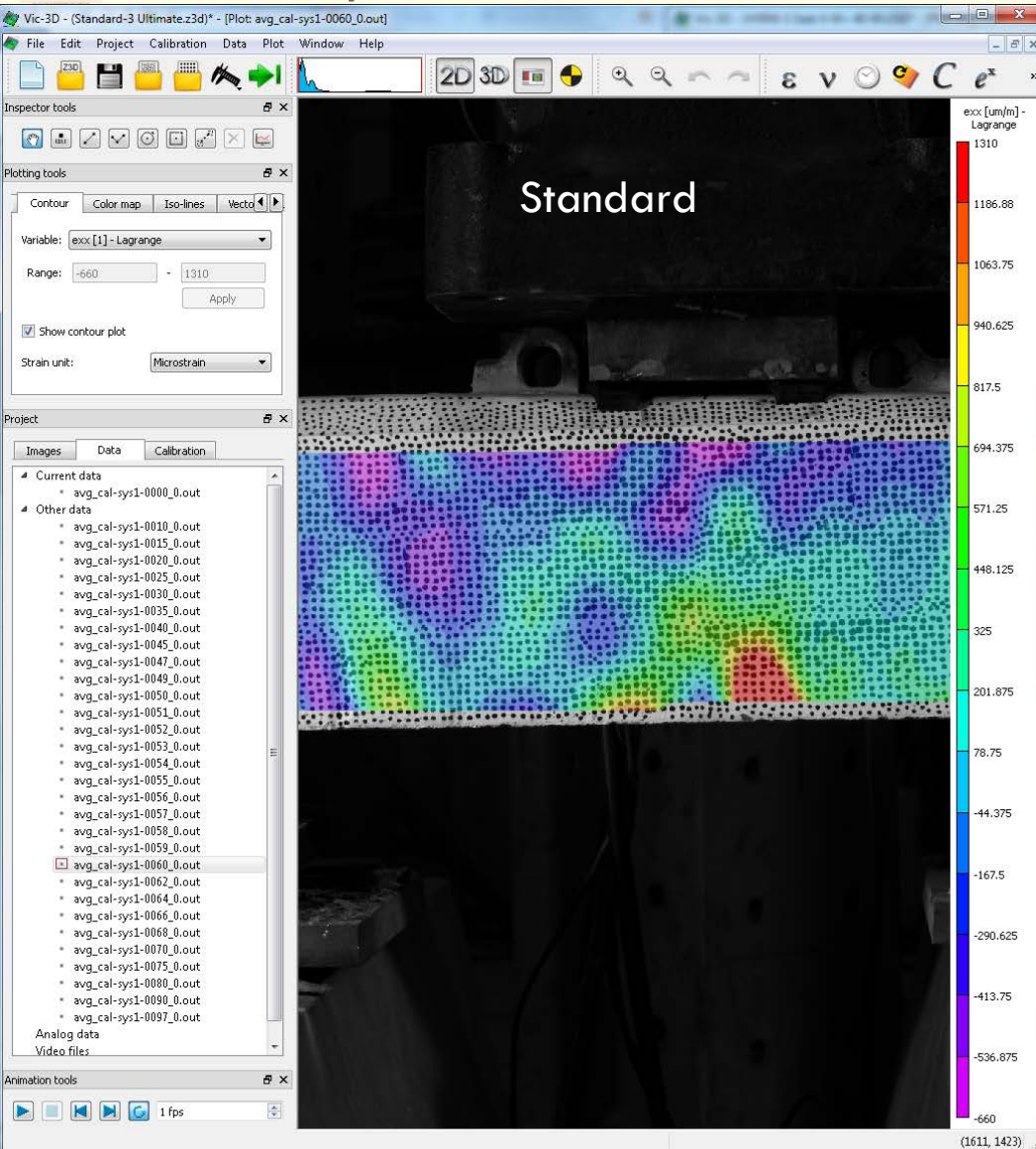




Tie ID		Rail Seat A					Strand Slippage
		$\epsilon_{\text{prestress}}$ (+/- 10%)	ϵ_{crack}	P_{crack}	1.5P	P_u	
Prototype	HSRM-Q1	~800 $\mu\epsilon$	~320 $\mu\epsilon$	56	Pass	>100	No
	HSRM-Q2						
	HSRM-Q3			57	Pass	>100	No
	HSRM-Q4						
	HSRM-Q5			52	Pass	96	No
Baseline	STND-Q1	~500 $\mu\epsilon$	~220 $\mu\epsilon$				
	STND-Q2						
	STND-Q3 (9-1)			57.9	Pass	88.9	No
	STND-Q4 (11-3)			52.1	Pass	105.3	No
	STND-Q7			49	Pass	97	No
Other	STND-Q5-A						
	STND-Q6-A						

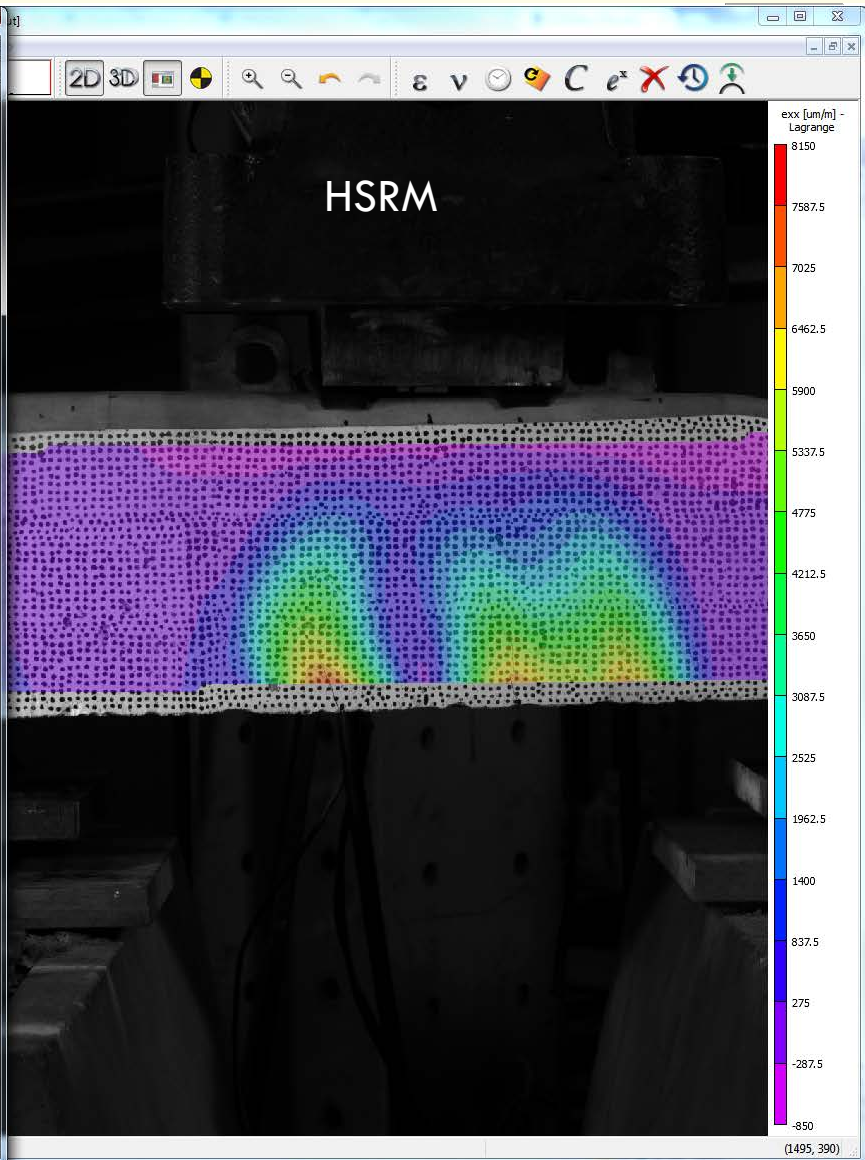
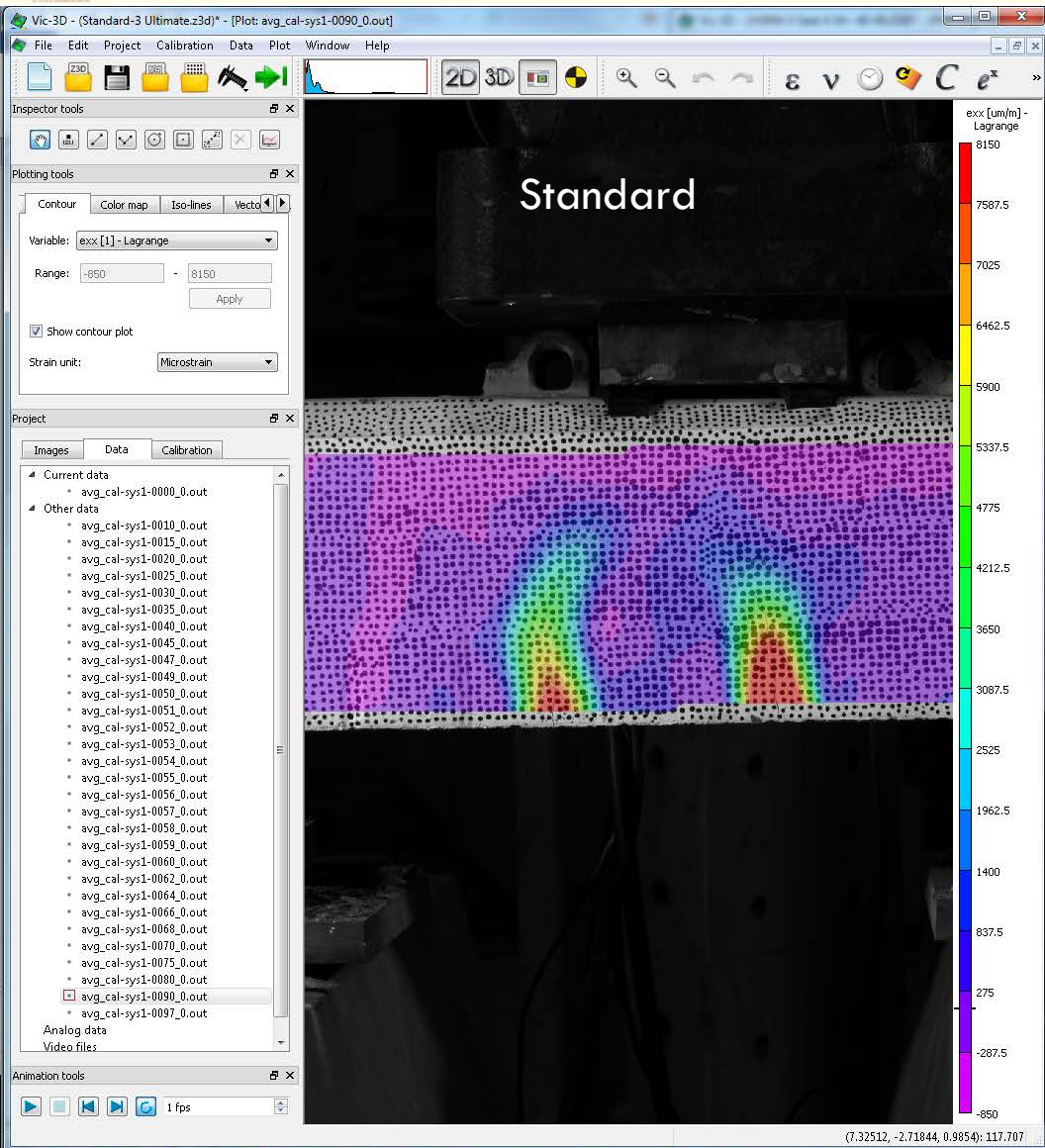


P=60 kips Same Scale





P=90 kips – Same Scale

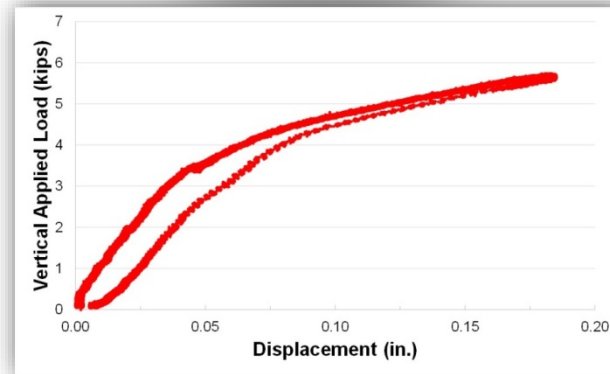




Fastener Pullout and Torque Tests



Crosstie	Rail Seat	Location	Pull-out (12kips)	Torque (250lb-ft)
Rocla	A	Field	PASS	PASS
		Gauge	PASS	PASS
	B	Field	PASS	PASS
		Gauge	PASS	PASS
USC Prototype	A	Field	PASS	PASS
		Gauge	PASS	PASS
	B	Field	PASS	PASS
		Gauge	PASS	PASS



Crosstie	Rail Seat	Result
Standard Crosstie	A	PASS
	B	PASS
USC Prototype Crosstie	A	PASS
	B	PASS

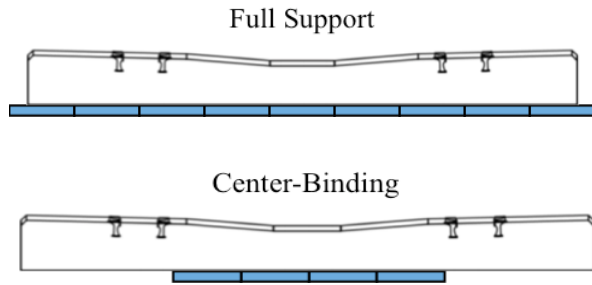
Crosstie	Level of Distress	Load (kips)
Standard	Crack Initiation at	31.6
	Insert Pulled out	34.6
HSRM	Crack Initiation	33.2
	Insert Pulled out	35.1

Standard

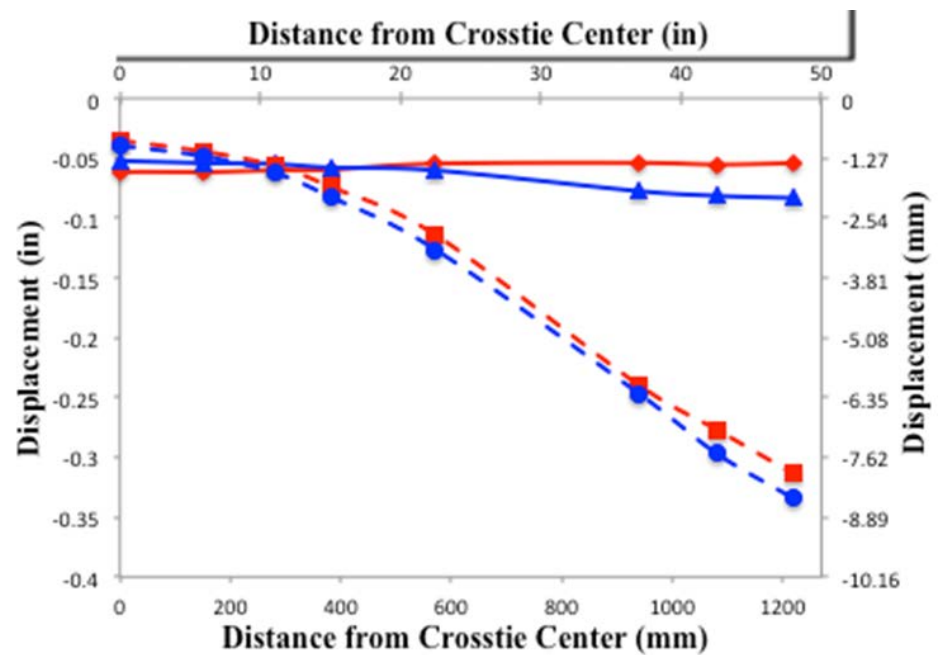
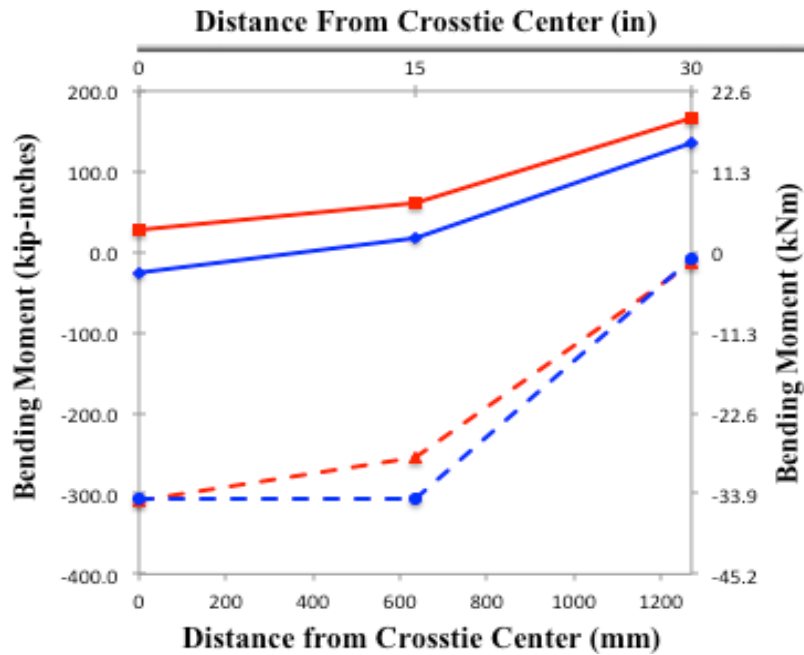


HSRM

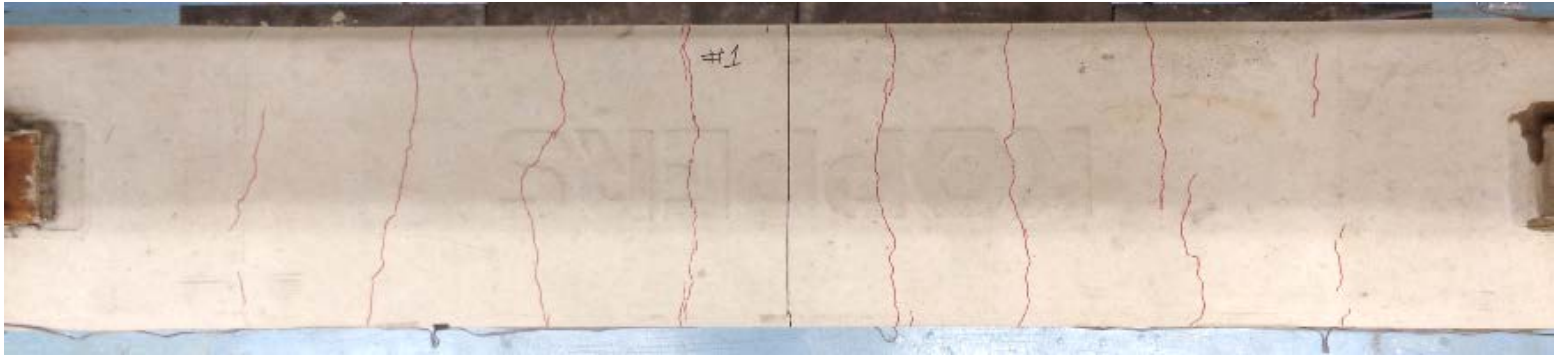




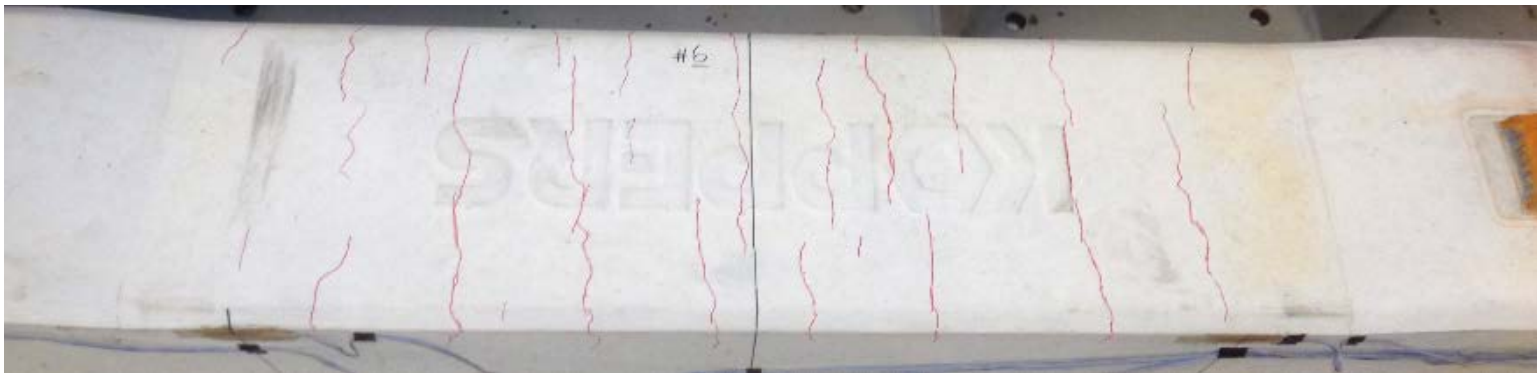
- Standard- Full Support
- Standard- Center Bound
- HSRM- Full Support
- HSRM- Center Bound



Standard Tie



HSRM Tie



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- **Conclusions and Current and Future Work**

- HSRM-HPC similar properties as Limestone HPC except Elastic Modulus (up to 50% reduction)
- HSRM Ties Passed all AREMA Qualification Tests and meets or exceeds standard tie performance
- HSRM Tie provides
 - ▣ Better load distribution
 - ▣ Stress reduction
 - ▣ Delay onset of damage
- A technology based modification in concrete tie technology that will improve the safety of rail service and maintenance operations without impacting fabrication cost and process



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Dr. Robert Peterman

Dr. Juan Caicedo
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Dr. Robert Mullen

Ali Abdulqader
Sally Bartelmo
Albert Ortiz
Adam Zeitouni
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